

RED FLAT NICKEL CORP.

Evaluation of the Red Flat Ni/Co Property Mining Potential, Curry County, Oregon, U.S.A.

NI 43-101 Technical Report

TECHNICAL SPECIFICATIONS

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1. EXECUTIVE SUMMARY

Red Flat Nickel Corp. (hereinafter: RFN) owns a 100% interests in the Red Flat property. The property consists of 93 claims of 600 ft by 1,500 ft and 7 claims of 600 ft by 965 ft, covering a total area of 2,015 acres. It lies in south-western Oregon, some 300 miles south of Portland, Oregon, in the coastal range north-west of Curry County. It is in a mountainous forest area that can be accessed from Gold Beach by taking the US 101 for 10 miles towards the east, via the Hunter Creek road and then connecting to local prospect roads. The property location is shown on Map 1 in Appendix A.

The Red Flat property was discovered in 1939 and was investigated by Hundhausen et al. in 1954 (USBM) and later by Ramp in 1978 (DOGAMI). This early work consisted of 39 drill holes, approximately 9,000 ft of trenches and geological mapping of the ultramafic rock. The regional geology was described and mapped (geological map of Curry County) by Ramp et al. (1977) and it is presented on Map 2. Two key findings from these early investigations are that the average laterite thickness was 12.5 ft and possibly extended down to 50 ft (Hundhausen et al., 1954) and that the nickel accumulation area covers approximately 1,100 acres (Ramp, 1978).

The nickel deposits on the property is the result of the surface alteration of olivine rich ultramafic rocks, often called nickel laterites. They are formed by the weathering of the serpentinized peridotite generally in humid savannas climates with poor drainage and associated with dry climates and semi-arid environments. During weathering, nickel is concentrated in place while more soluble elements such as magnesium, calcium and silica are dissolved and leached rapidly. Nickel accumulates in the form of nickel-silicate veins or becomes enriched in the insoluble residue of silica, nickel hydrosilicates, and oxides of magnesium and iron.

Between 2007 and 2009 RFN conducted extensive auger drilling, sonic drilling and mechanical trenching on the property. Between 2007 and 2008, 676 auger holes were drilled on a 300 x 300 ft grid. The depth of the holes varied from 3 to 24 ft and when combined, totalled 5,638 ft drilling. The 2008 drilling campaign also included 11 sonic drill holes for a total length of 930 ft and 9 seismic refraction geophysics lines for a total length of 13,570 ft.

In 2009, four trenches were mechanically excavated to conduct soil and rock sampling, chemical assays, corestone content estimation, density measurements,

and large sample metallurgical analysis. Mineralogical and metallurgical tests were ongoing at the time of writing this report.

The drilling and trenching work located and accurately defined the mineralized zone, discovered garnierite and confirmed the presence of economic Ni and Co grades in two resource fractions, the soil fraction and the rock fraction. The results show a strong horizontal continuity and that the nickel concentration in the soil fraction increases with depth. The measured resources category is limited to the area where the sampling techniques used allowed for corestone sampling and analysis (sonic drilling and trenching). Based on the results, the measured, indicated and inferred resources were evaluated using 0.7% and 0.8% Ni cut-offs. Resource estimate are presented as follows:

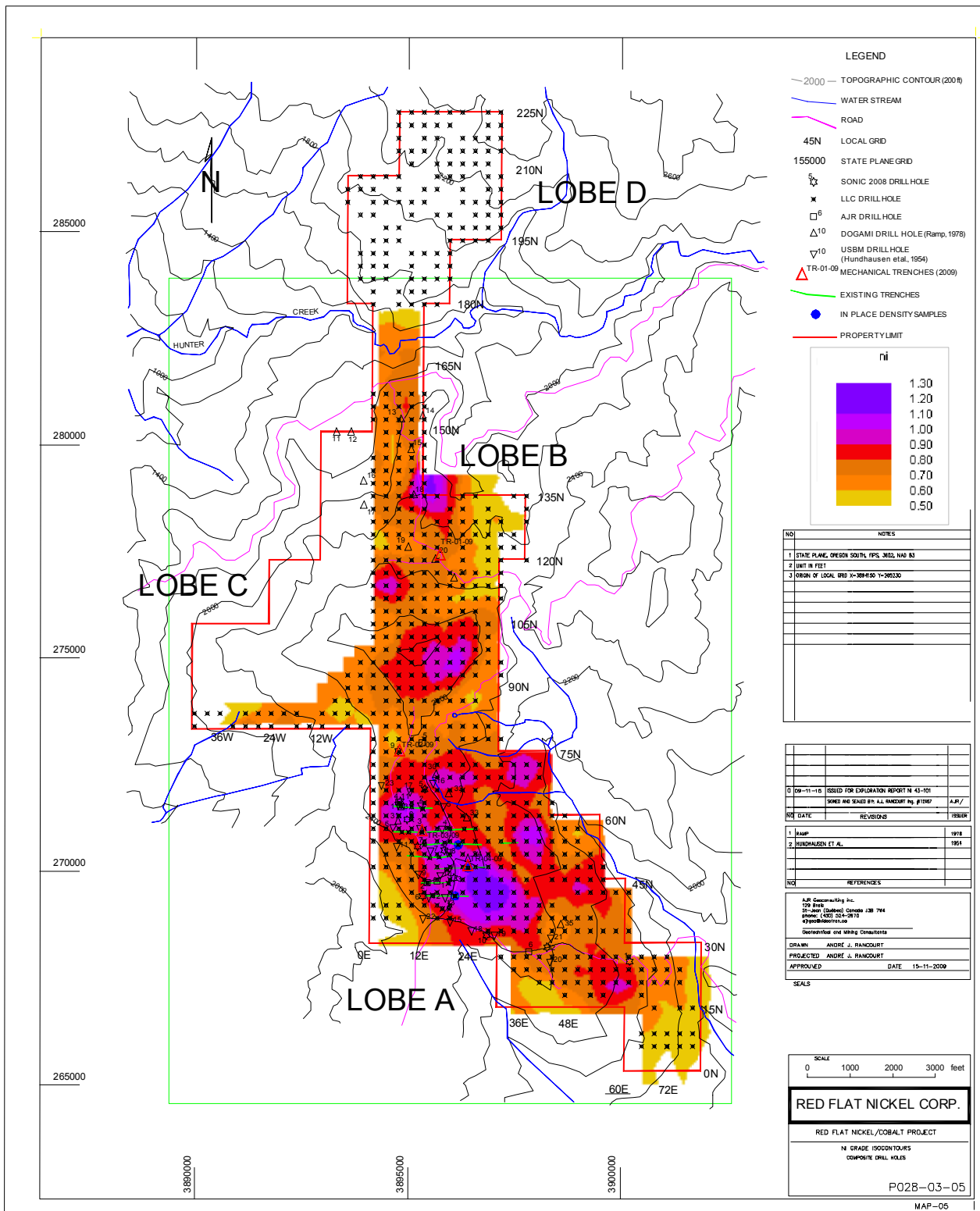
Cut-off Ni (%)	Type	Measured Tons (*1000) Ni (%)		Indicated Tons (*1000) Ni (%)		Inferred Tons (*1000) Ni (%)		Total Inferred Tons (*1000) Ni (%)	
0.7	Soil	1,710	0.91	3,218	0.81	4,169	0.80	9,097	0.82
	Rock	2,277	1.05	3,218	0.81	4,169	0.80	9,664	0.89
	Total	3,987	0.99	6,436	0.81	8,338	0.80	18,761	0.84
0.8	Soil	1,700	0.91	1,684	0.88	1,728	0.88	5,112	0.89
	Rock	2,007	1.10	1,684	0.88	1,728	0.88	5,419	1.00
	Total	3,707	1.01	3,368	0.88	3,686	0.88	10,531	0.92

Given the excellent results of the 2007, 2008 drilling program and the 2009 trenching program, which found garnierite-group minerals grading up to 4.3 % Ni and concentrations of up to 1.53 % Ni in the corestones, additional work is recommended on the property, to upgrade the resource.

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Evaluation of the Red Flat Ni/Co Property Mining Potential,
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NI 43-101 TECHNICAL REPORT

1. Executive Summary



2. INTRODUCTION

2.1 CLIENT AND MANDATE

At the request of the President of Red Flat Nickel Corp. (RFN), AJR Geoconsulting Inc. (AJR) was assigned the mandate to update the resource estimate on the Red Flat lateritic nickel/cobalt property in Curry County, Oregon and to prepare an independent, NI 43-101 compliant technical report. This is the third report, reflecting three years of extensive field investigation by RFN.

André J. Rancourt, Eng, M.A.Sc. President of AJR Geoconsulting Inc. was appointed Project Manager. This report was produced by André J. Rancourt. The site supervision was sub-contracted to LithoLogic Resources (LLR), with Mike D. Strickler, R.G. as the lead geologist, Oregon qualified geologists, as field geologists.

2.2 REPORT OBJECTIVE

The goal of the 2009 summer field work was to upgrade the resource category. To achieve this, trenches, bulk sampling and petrographic characterization of the ore were completed. Preliminary metallurgical testing is also ongoing but the results were not yet available at the time of writing this report. RFN also wishes to perform pre-feasibility and feasibility studies that will facilitate the environmental and mineral permitting needed to put the project into production.

The 2009 trenching, drilling and sampling program resulted in the estimation of measured, indicated and inferred resources.

The NI 43-101 report informs potential investors on the specific characteristics of the Red Flat property, as defined by the instrument.

2.3 ABBREVIATIONS USED

RFN:	Red Flat Nickel Corp.
AJR:	AJR Geoconsulting, consulting engineer
LLR:	Lithologic Resources, a professional geological firm in Selma, Oregon.
CIM:	Canadian Institute of Mining and Metallurgy
ATV:	All terrain vehicles
BLM:	Bureau of Land Management, www.blm.gov
USBM:	United States Bureau of Mines

USGS: United States Geological Survey

DOGAMI: Oregon Department of Geology and Mineral Industries,
egov.oregon.gov/DOGAMI

MLRR: Mineral Land Regulation and Reclamation Program

DEQ: Department of Environmental Quality

NSR: Net Smelter Return

2.4 FIELD VISIT

Field work was carried out during 2007, 2008 and 2009 on the Red Flat deposit and consisted of mechanical shovel trenches (2009), sonic drilling on lobe A, refractive seismology on lobes A and B, and auger testing on lobe C (2008), and drilling on lobe A and lobe B (2007).

The excavation of 4 trenches and sampling was done on August 13, 2009. In 2008, a total of 930 ft of sonic drilling was completed in eleven (11) separate holes.

Sonic drilling began on September 10th, 2008, and was completed on September 25th, 2008. Shallow auger testing continued at Red Flat with a total of 395 holes with an aggregate depth of 3,117 ft.

In 2007, field work consisted essentially in an auger drilling program that took place between September 13th, 2007 and January 4th, 2008. Some 275 holes were drilled for a total of 2,483 ft.

All the sampling and drilling was carried out under the direct supervision of LLR.

The author has visited the property twice, the first visit was on December 1st, 2007, and the second visit was on August 13th, 2009. Both visits were done in the presence of LLR geologists and crew. In 2007, AJR sampled six (6) additional verification holes and in 2009, AJR performed complementary sampling in the trenches. Tables 2.1 and 2.2 present the characteristics of the verification drill holes and the samples. Chapter 14 presents the interpretation of the verification holes results performed during the author's visit. Appendix B shows the complete list of the trench and drill hole assay results for the 2007, 2008 and 2009 sampling and drilling programs under LLR field supervision.

Table 2. 1 - Characteristics of the verification drill holes and samples taken by AJR

Hole No.	Sample	Coordinates ¹		Length
	(ft)	East (ft)	North (ft)	(ft)
AJR-01	0 - 6	3895685	269765	7
	6 - 7			
AJR-02	0 - 6	3895468	269733	6
AJR-03	0 - 6	3894836	271528	9
	6 - 9			
AJR-04	0 - 6	3894790	271625	6
AJR-05	0 - 4	3895334	273020	4
AJR-06	0 - 6	3897849	268108	6

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

Table 2. 2 - Characteristics of the trench samples taken by AJR in 2009

Trench No.	Sample no.	Coordinates ¹		Trench depth	Description
	Depth (ft)	East (ft)	North (ft)	(ft)	
1	6	3895685	269765	7	Altered corestone
	8				Altered corestone
	15				Fresh corestone
2	4	3895468	269733	6	Corestone
	6				Fresh corestone
	10				Corestone
3	2	3894836	271528	9	Rind
	15				Fresh corestone
	15A				Rind
	GAR				Garnierite grab sample
4	3	3894790	271625	6	Saprolite loose and porous
	5				Altered corestone
	6				Fresh corestone
	9				Altered corestone
	9A				Altered corestone

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

3. RELIANCE ON OTHER EXPERTS

AJR has reviewed all the property titles and technical data provided by RFN and its representatives. AJR has compiled and interpreted the data from trenches, drill holes and geochemical assays for the 2007, 2008 and 2009 investigation programs supervised by LLR. AJR has also interpreted the historical data to include them in the resource calculations. A review of the publicly available information at the USBM, the USGS and the DOGAMI completed the technical information used in the preparation of this report. AJR believes that the information used to prepare this report is valid and appropriate.

AJR is not qualified to express a legal opinion with regard to property title or its validity, and cannot be held responsible for potential issues caused by irregularities. However, appendix E includes a deed that confirms the property titles.

4. PROPERTY DESCRIPTION AND LOCATION

4.1 PROPERTY AREA

The project includes 93 claims of 600 ft by 1,500 ft and 7 claims of 600 ft by 965 ft, covering a total area of 2,015 acres. Map 1, in Appendix A, presents the property location and the claim layout. The Red Flat claims were reviewed using the notice of location presented, received and duly recorded in the official records of Curry County, Oregon. The list of claims is presented in Appendix E.

4.2 LOCATION

The property is located on the top of Red Flat Mountain, 9 miles east of the town of Gold Beach, Oregon, in the north-west of Curry County, about 300 miles south of Portland, Oregon. It is in a mountainous forest area that can be accessed from Gold Beach by taking the US 101 via the Hunter Creek road and then connecting to local prospect roads. Table 4.1 presents the northern, southern, eastern and western property limits.

Table 4. 1 - Geographic coordinates of the Red Flat property limits

Claim	Map	Limit	Coordinates ¹	
			East	North
Red Flat	Signal Butte 7.5" Quad, and Sundown Mountain 7.5" Quad, OR	West	3890000	
		East	3901800	
		North		287800
		South		265200

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

4.3 TYPE OF MINING TITLE

RFN holds lode mining claims for its Red Flat property. The MLRR and the BLM covers in details the rights, obligations and definitions regarding lode mining claims.

4.4 ISSUERS RIGHTS AND OBLIGATIONS

4.4.1 Surface Rights

The Red Flat property covers 2,015 acres. The claims are renewed yearly after payment of the Annual Maintenance Fees (see attached certified documents in Appendix E).

4.4.2 Mining Royalties

RFN has a 100% interest in the Red Flat property. According to the documents provided by RFN, the Red Flat property is not subject to any royalties or NSR payable to a third party other than those provided for by law.

4.4.3 Agreements

No information on acquisition privileges has been found in the documents provided to AJR by RFN.

4.4.4 Claims Delimitation

The Red Flat property was staked and claimed by LLR during the spring of 2007. AJR has checked that all the drill holes and the entire mineralized deposits included in the resource estimations were within the limits of the Red Flat property. AJR has observed and documented actual claim monuments staked by LLR. Figure 4.1 and 4.2 shows photographs of some monuments taken during the 2007 field visit.

4.4.5 Location of Mineralized Zones

The lateritic surface layer containing the nickel/cobalt, lies at the surface; it is a lateritic surface horizon covering ultramafic rocks. The mineralized layer follows the ground surface and was mapped by Ramp (1978). It has been traced by drilling to a maximum depth of 40 ft and might reach a depth of 50 ft (Hundhausen et al., 1954). The nickel grade is correlated with depth. The ore body is highly continuous in the horizontal plane.

4.4.6 Environmental Obligations

Exploration work conducted by/or on behalf of RFN must comply with the DEQ and applicable legislation. Forest management permits were issued in 2007, 2008 and 2009. The 2009 valid forest management permit is attached as Appendix F.

**5. ACCESS, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND
PHYSICAL GEOGRAPHY**

5.1 ACCESS ROADS AND INFRASTRUCTURE

The property can be accessed from Gold Beach by taking the US 101 via the Hunter Creek road and the connecting prospect road for approximately 9 miles. The Coos Bay/North Bend airport is located about 60 miles north of the property.

5.2 CLIMATE

The climate that prevails on a regional scale is temperate and of the coastal range type. The property lies in the mountains and reaches approximately 4,000 ft in elevation, abutting the coastal strip. The average day temperature on the property ranges from 32° F in the winter to 70° F in the summer. The area has morning valley fog in the summer and tends to keep marine influences out of the intermountain valleys. It has mild winters and mild summers with high precipitation (up to 75 in. per year). In the winter, snow covers the ground from November to April, at elevations above 4,000 ft.

The Red Flat property is located on a mountain side, in the west part of the Coastal Range at around 2,600 ft. Most of the property experiences colder temperatures than the surrounding valleys. Very few people live in the coastal range itself.

5.3 SERVICES AND LOCAL RESOURCES

Gold Beach is situated on the coast and is the closest city with services. The nearest airport is at Coos Bay/North Bend, located 70 miles north of the property. Working materials can be easily brought in from Coos Bay or Gold Beach to the property. The local economy is largely based on the logging industry and the coast has tourist vocations in the summer. There is a gravel operation in the Hunter Creek and several borrow pits along the road.

5.4 TOPOGRAPHY, ALTITUDE AND VEGETATION

The topography of the property was shaped by the coastal mountain range. The maximum difference in altitude on the property is 1,200 ft, and the average altitude of the property is around 2,600 ft. The property lies on the east side of a mountain ridge, reaching a maximum altitude of around 2,800 ft. The mountain ridge is composed of three topographic structures, the south-east ridge (lobe A), the center ridge (lobe B) and the north ridge (lobe C).

Because of the rock lithology and altitude, the vegetation is less abundant and less prolific than in the valley bottoms. The property is mostly covered by fir, spruce, pine and cedar trees and manzanita, salal, rhododendron and other brushy varieties (see figure 5.1).

6. HISTORICAL EXPLORATION AND EXPLOITATION WORKS

6.1 EXPLORATION WORKS

6.1.1 General

Nickel-bearing laterites of south-western Oregon are known since the discovery of the Nickel Mountain Mine near Riddle, Oregon in 1881. This mine was in operation from 1954 until 1976 and provided 39 million tons of ore at nickel grades between 1 and 1.5 %. Regional investigations were carried out by the DOGAMI beginning in 1943. DOGAMI's work on the laterites followed the publication of a study of the Nickel Mountain deposit by the USGS (Pecora and Hobbs, 1942). The following history briefly outlines a number of activities on the Red Flat property:

- 1939 - The Red Flat nickel/cobalt horizon was discovered by Harry Hefferley.
- 1947 - Libbey and others completed reconnaissance mapping and hand-auger sampling.
- 1954 - Extensive drilling, trenching and metallurgical tests were carried out by the USBM (Hundhausen et al.)
- 1978 - Drilling and mapping completed by the DOGAMI (Ramp, 1978).

6.1.2 Type and Quantity

Hundhausen et al. (1954) and the USBM drilled 22 holes using a Star churn drill mounted on a 6-wheel-drive truck. In total, they drilled 1,032 ft. Holes were 6" diameter and ranged in depth from 20 to 117 ft. They were located approximately 500 ft apart and were concentrated in lobe A. They also completed approximately 9,000 ft of trenches and performed metallurgical smelting tests on over 14 tons of dry material collected from drill holes and trenches.

Ramp (1978) and DOGAMI completed geological mapping of the area and collected 35 samples from holes and channel/grab/chip samples taken by the DOGAMI and others. The map and sampling partly cover three lobes of the property. The regional geology was described by Ramp et al. (1977) and culminated in a geological map of Curry County. Ramp et al. (1978) augered 9 holes for a total length of 71 ft. They also drilled 6 holes for a total length of 110 ft. Holes range in depth from 5 to 25 ft.

6.1.3 Results

The work from Hundhausen et al. (1954) demonstrated the horizontal continuity of the laterite and they recovered 94.5 % of the nickel processed by the smelting furnace. Drill holes and sample sites from both Hundhausen et al. (1954) and Ramp

(1978) are located on map 3 in Appendix A. Table 6.1 summarizes the assay results from Hundhausen et al. (1954), and table 6.2 presents the work from Ramp (1978), as used in this report for the resources estimation. Appendix G includes an extract of the report from Ramp (1978), and the complete report from Hundhausen et al. (1954).

Table 6. 1 – Assay 5 ft composite results modified from Hundhausen et al. (1954)

Coordinates ¹		USBM Drill hole no.	Sample composite thickness (from surface) using 0.5% Ni cut-off	Ni
X	Y			
(ft)	(ft)		(ft)	(%)
3894779.8	271563.859	1	30	0.58
3895314.14	271547.79	2	35	0.54
3895287.15	271014.027	3	60	0.71
3895812.61	270994.823	4	50	0.73
3895838.82	271527.408	5	30	0.52
3894659.08	271038.292	6	30	0.57
3895540.65	270482.939	7	45	0.88
3895943.35	270446.087	8	0	0.41
3895255.87	269929.359	9	20	1.04
3895767.58	269910.375	10	30	0.96
3894742.95	270585.397	11	50	0.76
3895498.12	269384.289	12	15	0.81
3895882.77	269390.019	13	35	0.75
3895994.63	268821.297	15	15	1.15
3895603.65	272072.747	16	5	0.92
3895061.05	271880.496	17	30	0.79
3896501.19	268607.897	18	10	0.51
3897037.61	268504.138	19	0	0.41
3898344.19	267880.991	20	25	0.95
3898373.1	268435.448	21	20	0.51
3895363.03	268899.699	22	0	0.25
3894387.89	272025.6	23	30	1.22

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

Table 6. 2 - Sample assay results modified from Ramp (1978)

Coordinates ¹		Auger hole no.	Drill hole no.	Sample interval	Ni
X	Y				
(ft)	(ft)			(ft)	(%)
3893334.61	280296.239	11		6	0.96
3893672.91	280292.131	12		6	0.90
3895358.61	280685.046	14		14	0.86
3893969.51	279153.129	16		7	0.34
3893973.88	278587.46	17		9	0.69
3895149.38	278817.985	18		5	0.90
3895017.31	277597.61	19		6	0.78
3895655.93	277315.034	20		8	1.11
3896093.81	276865.376	21		10	1.54
3895669	272271.845		30	10	0.65
3894772.2	271176.182		31	25	0.78
3895961.98	271812.472		32	15	0.57
3896384.55	271249.213		33	25	0.83
3896414.57	270292.036		34	15	0.66
3898599.48	268737.27		35	20	0.55

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

These holes and samples have been included in the geological interpretation along with the 2007 and 2008 drilling program.

6.2 PREVIOUS MINERAL RESOURCES AND MINERAL RESERVE ESTIMATIONS

There were two previous resource estimations done for the Red Flat property. Those estimations are dated April 2008 and March 2009, and were also prepared by AJR. It is also important to refer to the work of Hundhausen et al. (1954) on lobe A and the work done by Ramp (1978) on lobes A, B and C.

The following historical characterization from Ramp should be noted. On lobe A, the mineralized zone shows an average thickness of 28.3 ft with an average of 0.77 % Ni. The average grade for the first 10.7 ft of laterite is 1.2 % Ni. The deepest borehole reached 60 ft with a grade of 0.7 % Ni. On lobe B and C, the mineralized zone reached a depths ranging from 3.3 ft to 13 ft, with an average grade of 0.71 % Ni and 0.09 % Co.

6.3 PREVIOUS PRODUCTION

There has been no prior Ni, Co production from the Red Flat property.

7. GEOLOGICAL CONTEXT

The regional geology of the area was described by Walker and King (1969), Ramp et al. (1977) and on a larger scale by Irwin (1997) and Johnson and Raines (2001). The property is located on the Northern Coast Range mountains physiographic terrane, composed mostly of sedimentary rocks of Mesozoic Age from the Dothan Point Formation and some ultramafic and gabbroic intrusions of Jurassic age. The ultramafic rocks and the Colebrook schist form thrust plates in unconformity with the younger Dothan Point volcano-sedimentary rocks. To the east, the Northern Coastal Range contacts the older volcanics of the Pre-Nevadan Klamath Mountains and to the north, it contacts the younger sedimentary rocks of the Oregon Coast Range.

7.1 REGIONAL GEOLOGY

The regional geology has been described in detail by Hotz (1964) and by Ramp (1978). The area is mostly covered by Jurassic ultramafic bedrock and some volcano-sedimentary of the Dothan Point Formation and Colebrook schists. Also, a few of the youngest Cretaceous sedimentary rocks are present in the area. The ultramafic rocks found on the property are forming a thin erosional remnant of a thrust sheet together with a thin sheet of Colebrook schist overlying unconformably on the Dothan Point Formation (Ramp, 1978). The area is intruded with diabase dykes and faulted with high angle fault zones. Map 2, in Appendix A, illustrates the regional geology.

7.2 PROPERTY GEOLOGY

The property is covered by ultramafic rocks and the Colebrook schist formations. They form a thrust plate lying in unconformity on the younger Dothan Point volcano-sedimentary Formation. The ultramafic rocks which comprise the Red Flat deposits are mainly composed of serpentinized peridotite (harzburgite and dunite) and pyroxenite. The rocks are mainly made of a typical olivine alteration called bowlingite, serpentine, quartz, chlorite and talc. Magnetite, hematite, zircon and rutile were also observed. Some quartz is present in small veins associated with fibrous talc.

The mineralized horizon is a lateritic weathering profile formed by the prolonged weathering of the ultramafic rocks in sub-tropical climates. The laterite zones are divided in four distinct area, the lobe A of 500 acres located to the south-east, the lobe B covers 250 acres to the north, lobe C extends another 200 acres to the west and lobe D is located some 2,500 ft north of lobe B and covers 154 acres.

Mineralogical and petrographic analyses were made on the limonite and saprolite and also two polished rock sections and the reports are presented in Appendix D.

8. TYPE OF MINERAL DEPOSITS

The type of deposits in the Red Flat area consists of a concentration of nickel and cobalt from the surface alteration of olivine rich ultramafic rocks often called nickel laterites. Ultramafic rocks average 0.2 – 0.4 % Ni. Laterites are formed by weathering of the serpentinized peridotites generally in humid savanna climates with poor drainage and associated with dry climates and semi-arid environments. During weathering, nickel is concentrated in place while more soluble elements such as magnesium, calcium and silica are dissolved and leached rapidly. Nickel accumulates in the form of nickel-silicate veins or becomes enriched in the insoluble residue of silica, nickel hydrosilicates, and oxides of magnesium and iron. Similar Oregon laterite nickel deposits have been described by Pecora and Hobbs, (1942) and by Hotz, (1964).

The laterites found on the property are remnants of an old upland surface and according to Irwin (1997), the weathering has taken place during the Pleistocene and/or the Pliocene. Typical laterite profile is presented on table 8.1.

Table 8. 1 - Typical lateritic profile (adapted from Golightly, 2005)

Unit	Mineralogy	Structure
Landslide	Mixed of cover, corestones, limonite and saprolite	Slide and slumping accumulation of mixed structures
Cover	Goethite + Kaolinite ± Hematite ± Gibbsite + Quartz	Granular iron pebbles (kanga) with peridotite boulders (30 – 60 %) at surface, limonitic matrix
Limonite	Goethite ± Mn, Co oxides ± Gibbsite ± Quartz	Porous clayed limonite, some sand, some relict bedrock corestones
Upper Saprolite	Ni in serpentine + Mn, Co oxides + Quartz	Fe rich Mg poor Saprolite crusts surround Ni enriched saprolite corestones
Lower Saprolite	Ni in serpentine + Goethite	Fe poor Mg rich Saprolite crusts surround peridotite corestones
Bedrock	Forsteritic Olivine and Serpentine (± pyroxenes ± talc)	Joint blocks, serpentinite breccia

Figures 8.1, 8.2, 8.3 and 8.4 respectively illustrate examples of corestone cover, bedrock outcrop and trenches made by Hundhausen et al. (1954). The variation of Ni, Co and Fe grade with depth is shown in figures 8.5, 8.6 and 8.7, respectively. Apart from the apparent vertical sampling spacing effects (horizontal lines), figure 8.5 shows that the Ni grade seems to increase with depth. Figure 8.6 is less instructive

due to the lab accuracy detection of Co. However, higher Co values appear to be located around 5 ft to 15 ft. Finally, figure 8.7 shows that the Fe values decrease with in depth.

9. MINERALIZATION

The nickel laterites of the project can be classified on the basis of ore mineralogy as clay silicate deposits and potentially oxide deposits. The mineralization is found in two fractions, the soil fraction and the rock fraction. For the soil fraction, the mineralized zone is usually composed of residual goethitic limonites covering altered peridotite layers (saprolite) with iron oxide veins. The mineralogy of the laterites at Nickel Mountain (Oregon) was studied by Pecora and Hobbs (1942) and Hotz (1964). They concluded that montmorillonite, chlorite and talc constitute the clay fraction. Also, nickel occurs in nontronite, a ferric iron member of the montmorillonite (Hotz, 1964; Ramp, 1978). For the rock part, nickel is also concentrated in thin fracture fillings of garnierite saprolite corestones blocks. In support of these conclusions, one chip sample of garnierite from the 2009 field work assayed at 4.3 % Ni.

Garnierite was found in the serpentinized bedrock on the property by Hundhausen et al. (1954) and in two of the four trenches excavated in 2009 by RFN. Garnierite appears to be present when the concentration of nickel in the soil exceeds 1 %. Figure 9.1 illustrates some of the Garnierite group mineral found during the 2009 trenching program.

Map 4, in Appendix A, presents the nickel concentration distribution in the soil. Figure 9.2 shows the cumulative frequency of nickel grades, from the figure, three types of mineralization can be identified using straight lines. The first type is from 0 to 0.4 Ni% and represents the non mineralized zone, the second is the first mineralization zone from 0.4 Ni% to around 1 Ni%, and the third type high grade mineralization zone above 1 Ni%.

The limonite and saprolite from Red Flat deposit were submitted for preliminary mineralogical analysis to the SGS laboratory with the objective of identifying the mineralogical phases in the lateritic profile. Also, in 2007 some preliminary petrographical characterizations of corestone were conducted by the petrograph S. Caderon, P.Geo. Ph. D. The samples sent from AJR to S. Caderon were used to produce two polished thin sections from altered ultramafic rock. This work did not find any sulphide nickel mineral and clarified that nickel from Red Flat deposit will be found as a substitution element in different clay minerals or silicate and/or hydroxide minerals. A petrographical study is presented in Appendix D.

10. EXPLORATION WORK

10.1 GENERAL

Since RFN started exploration work on the Red Flat property in 2007 the following was completed: 670 auger holes covering 770 acres and 4 mechanically excavated trenches were completed; 1,564 samples were taken to the laboratory for chemical assay; 4 large samples (> 100 lbs) were sent for mineralogical and metallurgical analysis; 9 in-place density measurements were performed on 1 ft³ soil samples; and 12 rock density measurements were performed on fist grab samples. Map 3 presents the locations of the exploration work.

10.2 MAPPING

Geological mapping of the property was completed based on the drilling results and the nickel concentration. Map 5 presents the nickel concentration indicative of the laterite location.

10.3 GEOPHYSICS

The 2008 exploration program conducted by RFN included 9 seismic refraction geophysics lines for a total length of 13,570 ft. Data acquisition was performed between October 13th and November 24th, 2008. The objective of the seismic refraction program was primarily to validate the use of the method on this type of deposit and furthermore and to identify the depth of the mineralization. Geophysics were used because seismic acoustic wave velocity can be correlated to the rock nature and the rock quality. The wave velocity is well correlated with the bedrock quality. For to the Red Flat deposit, the clay fraction on the top shows a lower acoustic wave velocity and the bedrock underneath presents a greater acoustic wave velocity.

The sonic drill hole logs were also plotted on the seismic lines to see if a correlation could be interpreted for the limonite/saprolite interface and the interpreted interface saprolite/bedrock with a seismic velocity. It was concluded that a correlation exists between the thickness of the soil layer and the wave velocity interpreted from the testing. AJR also tried to correlate the interface corresponding to a 0.6% Ni cut-off with the seismic velocity, but in this case, there was no correlation. Appendix H summarizes the geophysical results.

10.4 DRILLING

See section 11.

10.5 TRENCHING

See section 12.

11. DRILLING

In 2008 the drilling program consisted of sonic drilling on lobe A, and auger testing on lobe C. A total of 930 ft of sonic drilling was completed in 11 separate holes achieving depths of 27 to 118 ft with an average depth of 77.5 ft. Sonic drilling began on September 10th, 2008, and was completed on September 25th, 2008. The 2008 shallow auger drilling was a continuation of the 2007 program and it completed 395 auger holes with an aggregate depth of 3,117 ft.

In 2007, the field work consisted of a vertical auger drilling program that took place between September 13th, 2007 and January 4th, 2008. Some 275 holes were drilled for a total of 2,483 ft. LLR directly supervised all of the drilling and sampling in 2007 and 2008.

11.1 SONIC DRILLING

Sonic drilling allows for a continuous sample of all material—the soils, the corestones and the bedrock. Eleven sonic drill holes were located on lobe A in the more prospective zone. Map 3 shows the location of these sonic drill holes. Figures 11.1 and 11.2 illustrate typical drilling and sampling operations. Drill hole results are summarized in table 11.1, along with the estimated percentage of rock and soil. The sonic hole drill logs are presented in appendix B.

The drill hole locations did not follow a defined grid. The locations were selected based on available access. Analysis of the corestone from the sonic drill holes confirms the presence of mineralization in the rocks (corestones) in the form of nickel-rich silicates (Garnierite Group) and validates data from USBM (Hundhausen et al., 1954). In some cases, the corestone is mineralized with a grade similar to that of the soil and in other cases the corestone shows only background nickel grades. It was possible to identify the base of the deposit in all eleven holes.

The average depth of the mineralized zone found in the holes (cut-off of 0.7 % Ni) was 16 ft and the deepest mineralization was found at 46 ft deep in hole 8.

Table 11. 1 – Summary of Sonic Drill Holes Results

Hole no.	From (ft)	To (ft)	Length (ft)	Ni (%)	Type ¹	Composition	
						soil (%)	rock (%)
1	0	4	4	0.6	S	100	0
1	4	8.5	4.5	0.12	R	0	100
1	8.5	15	6.5	0.7	S	75	25
1	15	17	2	0.36	S	75	25
1	17	23	6	0.47	S	75	25
1	23	25	2	0.34	S	100	0
1	25	27	2	0.12	R	0	100
2	0	5	5	0.76	S	100	0
2	5	10.5	5.5	0.65	R	0	100
2	10.5	27	16.5	0.26	R	0	100
3	0	1.5	1.5	0.71	S	100	0
3	1.5	8	6.5	0.65	S	75	25
3	8	10	2	0.28	S	100	0
3	10	11	1	0.26	R	0	100
3	11	11.5	0.5	0.23	R	0	100
3	11.5	12.5	1	0.44	S	100	0
4	0	6	6	1.07	S	80	20
4	6	14	8	0.98	S	75	25
4	14	16	2	0.69	R	15	85
4	16	17.5	1.5	0.94	S	85	15
4	17.5	19.5	2	0.23	R	40	60
4	19.5	26	6.5	0.23	R	0	100
5	0	2.5	2.5	0.77	S	100	0
5	2.5	7	4.5	0.57	R	20	80
5	7	12	5	0.89	S	80	20
5	12	17	5	0.34	R	0	100
5	17	18	1	0.5	S	80	20
5	18	18.5	0.5	0.19	R	0	100
5	18.5	20.5	2	0.22	S	50	50
6	0	2	2	0.78	S	100	0
6	2	7	5	0.97	S	75	25
6	7	11	4	1.16	S	100	0
6	11	12	1	0.65	S	100	0
6	12	12.5	0.5	0.7	R	0	100
6	12.5	14.5	2	0.93	S	75	25
6	14.5	16.5	2	0.72	R	10	90
6	16.5	18	1.5	0.61	S	50	50
6	18	20.5	2.5	0.4	R	10	90
6	20.5	21.5	1	0.81	S	75	25
6	21.5	22	0.5	0.71	R	0	100
6	22	22.5	0.5	0.64	S	75	25
6	22.5	24	1.5	0.52	R	0	100
6	24	24.5	0.5	0.43	R	0	100
6	24.5	25.5	1	0.7	S	90	10
6	25.5	27	1.5	0.32	S	50	50
6	27	30	3	0.32	S	50	50
7	0	0.5	0.5	0.97	S	100	0
7	0.5	8	7.5	1.26	R	0	100
7	8	13	5	0.78	S	75	25
7	13	17	4	1.14	S	65	35
7	17	17.5	0.5	0.28	R	0	100
7	17.5	27	9.5	0.26	S	50	50
8	0	1.5	1.5	0.23	S	100	0
8	1.5	5	3.5	0.77	R	0	100
8	5	8	3	0.28	S	75	25
8	8	11	3	0.4	S	100	0
8	11	17	6	0.65	R	85	15

Hole no.	From (ft)	To (ft)	Length (ft)	Ni (%)	Type ¹	Composition	
						soil (%)	rock (%)
8	17	22	5	0.44	S	50	50
8	22	22.5	0.5	1.45	R	0	100
8	22.5	27	4.5	0.62	S	90	10
8	27	33	6	0.42	R	50	50
8	33	40	7	1.31	S	50	50
8	40	43	3	1.02	R	10	90
8	43	44.5	1.5	0.94	R	0	100
8	44.5	46	1.5	0.78	S	80	20
8	46	47	1	0.44	R	0	100
8	47	49	2	0.33	R	20	80
9	0	1	1	1.01	S	100	0
9	1	7	6	0.63	S	75	25
9	7	9	2	0.25	R	0	100
9	9	15	6	0.44	S	75	25
9	15	16.5	1.5	0.25	R	0	100
10	0	4	4	0.38	S	100	0
10	4	12	8	0.25	R	0	100
10	12	17	5	0.21	R	0	100
10	17	22	5	0.21	R	30	70
11	0	2	2	-	S	100	0
11	2	9	7	-	R	0	100
11	9	10	1	-	S	100	0
11	10	27	17	-	R	0	100

¹ S: Soil, R: Rock

11.2 AUGER TESTING

Holes were drilled with two drills. The first was a 1.6 HP hand held auger drill that average 6.4 ft in depth and reached a maximum depth of approximately 15 ft. The second was a 5.5 HP two-man auger drill that reaching a maximum depth of 24 ft. All holes were logged and carefully sampled by professional Oregon geologists. All drill holes were surveyed using a Trimble GeoExplorer XT which has a ± 3 ft accuracy. Figures 11.3 and 11.4 are showing typical drilling operations. Drill hole results are provided in appendix B. Hole locations, drilling results, kriging and interpretation are also provided on maps 3, 4, 5 and 6 in Appendix A.

Data from the 2007 and 2008 auger testing were used to define the limits of the deposit, quantify the grade and determine a minimum depth extension of the deposit. While auger testing is the most economical way to sample laterites as a first step, its sampling capacity is limited and it should be used in conjunction with other sampling techniques to allow a complete ore characterization. For example, augers do not sample or drill through corestones. Hence, the grade of the corestones is unknown and a refusal can result from contacting a corestone instead of bedrock, in which case, the cause of the refusal is unknown.

A total of 676 auger tests were completed in 2007 and 2008 by LLR and the drilling generally followed a 300 x 300 ft grid. Hole depth varied from 3 to 24 ft and totalled

5,638 ft of drilling. The average hole depth, using a 0.5% nickel cut-off is 9.3 ft. LLR directly supervised all of the auger drilling.

12. TRENCHING

In 2009, 4 four trenches were mechanically excavated using a Hitachi 160LC excavator. Trench depths ranged from 8 to 21 ft and the work was completed between August 10th, 2009 and August 15th, 2009.

The objective of large mechanically excavated trenches was to obtain information about the proportion of corestones within the property and the mineralogy of the corestones. The trenching was also used to acquire large samples for mineralogical and metallurgical testing.

A total of 54 samples taken from the trenches, from which numerous chemical assays were conducted, 8 samples were taken for soils density analysis and four large samples (> 100 lbs) were taken for mineralogical and metallurgical testing. The trenching and sampling were carried out under the direct supervision of LLR.

12.1 MECHANICAL TRENCHING

The mechanical trenching allows for the visualisation of the deposit, the evaluation of the corestone content and the sampling of the clay and corestone fractions. Of the 4 trenches, 3 were located on lobe A and one was located on lobe B. Map 3 shows the location of the mechanical trenches and table 12.1 lists the results for the 4 trenches. Figures 12.1 to 12.4 depict the trenching and sampling. Assay results from the trenches and additional photographs are presented in appendix B.

The trenches do not follow a defined grid, they were located using available access. In some trenches, the corestone is mineralized with grades similar to those of the soil and in other cases the corestone shows only background nickel grades. Mineralized corestone was sampled from all 4 trenches and samples were also taken from the corestone rind, the rusty coating surrounding the rock. Figure 12.5 illustrates corestone and figure 12.6 shows the rind. As shown in table 12.1, the nickel grade of rind sample varies from 0.4 to 1.65 % Ni.

Table 12. 1 – Trenching Results for Soil, Corestone and Rind Sample

	Trench no.																								
	1				2				3				4												
Sample Type	Depth (ft)	Ni (%)	Fe/Mg	Soil type ¹	Depth (ft)	Ni (%)	Fe/Mg	Soil type ¹	Depth (ft)	Ni (%)	Fe/Mg	Soil type ¹	Depth (ft)	Ni (%)	Fe/Mg	Soil type ¹									
Soil	1	0.795	10.91	L	1	0.95	3.84	S	1	0.27	9.57	S	1	1.03	78.13	L									
	2	1.26	20.10	L	2	0.78	0.73	S	2	0.745	42.57	L	2	1.25	8.81	S									
	3	1.23	7.52	S	3	0.85	0.71	S	3	0.815	52.07	L	3	1.57	3.97	S									
	4	1.15	2.52	S	4	0.46	1.15	S	4	0.821	41.40	L	4	1.75	4.18	S									
	5	1.06	2.08	S	5	0.61	0.61	S	5	0.71	19.28	L	5	1.32	1.76	S									
	6	1.08	2.60	S	6	0.52	0.54	S	6	0.782	18.43	L	6	1.66	4.10	S									
	7	1.14	1.95	S	7	0.29	0.52	S	7	1.01	21.17	L	7	1.48	1.82	S									
	8	0.917	0.86	S	8	0.28	0.51	S	8	0.765	6.90	S	11	0.39	0.23	S									
	12	0.629	0.62	S					9	0.736	5.64	S													
									10	0.882	7.14	S													
									11	0.919	7.24	S													
									12	1.02	6.28	S													
									13	1.01	6.40177	S													
									14	0.979	4.32432	S													
									15	1.02	3.54286	S													
									21	1.44	7.06215	S													
Average Soil Ni (%)	1.029				0.69				0.87				1.44												
Corestone																									
Corestone percentage	55%				80%				35%				30%												
	0.276				0.29				0.821				1.38												
6	0.2				4	0.69			15	1.01			3	0.89											
8	0.792				6	0.57							5	1.86											
15	0.262				10	0.39							6	1.24											
													9	1.47											
													9A	1.53											
Average CorestoneNi (%)	0.38				0.48				0.916				1.39												
Rind																									
	0.776				2	0.4			2	0.401			1.58												
					6	0.45			12	1.65															
									15A	1.09															
Weighted average Ni (%) (Soil and corestone)	0.673				0.52				0.888				1.43												

¹ L: Limonite, S: Saprolite

13. SAMPLING METHODS

A total of 1,564 samples were taken during the 2007, 2008 and 2009 drilling and trenching programs (combined). A majority of the samples assayed came from the auger rods, while the rest were taken from sonic drilling or from existing trenches. Only 54 samples were taken from mechanical trenches. Also, 4 large composite samples were taken for mineralogical and metallurgical testing.

13.1 SAMPLES FROM AUGER

The samples taken were to be representative of a maximum of 6 ft drilling runs. Rods were carefully cleaned between each drill run. When early corestone refusal was encountered, several attempts were made in the near vicinity to achieve a deeper hole. Figures 13.1 and 13.2 outline the typical auger sampling procedures.

The auger drill sampling method has some advantages and some drawbacks:

- Advantages
 - Auger drills are light and easy to handle;
 - Possibility to obtain hundreds of shallow holes rapidly;
 - Can sample large areas.
- Drawbacks
 - The recovery can be very low especially in saturated materials;
 - The method is ineffective to sample corestones in the saprolite zones; and
 - Is a shallow hole method.

With there are many benefits to using the auger, it under samples the corestones and surface bedrock (which have nickel rich oxide and silicate coating and veins).

13.2 SAMPLES FROM SONIC DRILLING

Samples from sonic drill holes do not have a definite sample length. Sample length varies from 0.5 ft. to 20 ft. Samples from the sonic drill include corestone and bedrock samples, which were assumed to be representative of lithologic changes through the hole. The average nickel grade of the hole can be calculated by excluding or including the corestone. The grade information for each sonic drill hole presented in this report is a weighted average from the surface without external dilution and includes the corestone.

13.3 SAMPLES FROM MECHANICAL TRENCHING

Samples from mechanical trenching were taken along a vertical channel on the side of the trench. The objective was to sample every vertical foot, but some deeper samples were spaced larger than a one foot due to trench stability and safety issues. At those greater depths, the sample was taken using the excavator bucket.

Samples of approximately 1 ft³ were also collected for soils density measurement. Those samples weighed approximately 70 lbs. Also, fist size rock samples were collected for density measurements.

Four composite samples weighing 100 to 280 lbs, depending of the depth of the trench, were taken and sent for mineralogical and metallurgical testing at SGS laboratory in Ontario, Canada. The composites were obtained by blending around 10 lbs of material per vertical foot of trench.

14. SAMPLE PREPARATION, ANALYSIS AND SECURITY

All sampling was performed by professional Oregon geologists under the direct supervision of LLR. Samples were individually wrapped and identified with a unique number. The samples were sent to the assay laboratory quickly after being recovered from the field and a register was continually updated with the results.

The register is also a summary of assay results for nickel, cobalt, iron and magnesium (plus 15 additional elements). The register is attached in Appendix B. Assay results are also provided in Appendix B.

The laboratory selected to perform the assays was ALS Chemex of Vancouver, Canada, using the conventional ME-ICP61 method. This Canadian laboratory is ISO/IEC 17025 certified by the Standards Council of Canada and has its own quality system.

In 2007, AJR performed 6 spot check drill holes and collected 8 samples and in 2009 AJR collected 15 samples of corestone from the trenches. Moreover, in 2007, 10 of the samples already assayed by LLR were re-assayed by AJR for quality control. All assays performed by AJR were completed using the Ni-ICP81 method.

15. DATA VERIFICATION

AJR conducted two field visits, one in 2007 and one in 2009. In 2007, 6 holes stretched along a north-west south-east line covering a distance of around 6,000 ft were verified. Also, in 2007, laboratory quality was verified by randomly selecting 10 already assayed pulp samples, and re-assaying them using the Ni-ICP81 method. The ME-ICP61 method used by LLR, is a 4 acid leach digestion process which provides a near total extraction. This method is the conventional low cost multi-elements package used in exploration geochemistry. The assay verifications were done by AJR using the Ni-ICP81 method which is a 4 acid leach digestion combined with peroxide fusion suited for high grade samples and equivalent to the XRF method. In 2009, AJR collected 15 corestone samples for mineralisation verification.

Table 15.1 presents the assays results and the verification holes are located on Map 3, in Appendix A. Table 14.2 shows the space correlation interpretation of some verification holes in the vicinity of existing LLR holes. In general, results from AJR are in close agreement with results obtained from LLR and demonstrates the strong continuity of the mineralized zones.

Table 15. 1 - Assays results for AJR verification holes

Hole No.	Sample	Ni	Co
	(ft)	(%)	(%)
AJR-01	0 - 6	0.70	0.051
	6 - 7	0.82	0.054
AJR-02	0 – 6	1.33	0.075
AJR-03	0 – 6	1.47	0.071
	6 – 9	1.53	0.057
AJR-04	0 – 6	1.25	0.085
AJR-05	0 – 4	1.01	0.067
AJR-06	0 – 6	0.47	0.033

Table 15. 2 – Interpretation of the verification hole sample results

Verif. No.	Hole AJR	Coordinates ¹		Hole LLR	Coordinates ¹		Ni (%)	Remarks
		East (ft)	North (ft)		East (ft)	North (ft)		
1	AJR-01	3895685	269765				0.71	Verification hole located 36 ft away from checked hole
				45N-15E-6	3895695	269800	1.06	
2	AJR-02	3895468	269733				1.33	Verification hole located 12 ft away from checked hole
				TR-10A-6	3895466	269721	1.32	
3	AJR-03	3894836	271528				1.49	Verification hole located 11 ft away from checked hole
				TR-11A-6	3894847	271528	1.46	
4	AJR-04	3894790	271625				1.25	Verification hole located 25 ft away from checked hole
				63N-6E-06	3894795	271600	1.25	
5	AJR-05	3895334	273020				1.01	Verification hole locate 100 ft away from checked hole
				78N-12E-06	3895395	273100	1.39	
6	AJR-06	3897849	268108				0.47	Verification hole locate 121 ft away from checked hole
				27N-36E-6	3897795	268000	1.02	

¹ State Plane, Oregon South, FIPS, 3602, NAD 1983

Quality control assays are presented in table 15.3. This quality control consists of re-assaying samples to check for reproducibility of results. Samples were selected at random. The average variability is ± 0.03 % Ni, which AJR considers to be low. The average nickel grade is 1.02 % for the LLR samples and 1.04 % for the check samples. This difference between these two is negligible. These results confirm the accuracy and reproducibility of the assays performed by ALS Chemex Laboratories.

Table 15. 3 - - Quality control assay results

SAMPLE NO.	Ni-ICP81 Ni (%) AJR	ICP61 Ni (%) LLR	Diff. Ni (%)
75N-0E-6	0.90	0.87	0.03
69N-15E-6	1.41	1.44	0.03
45N-18E-11	1.36	1.35	0.01
51N-03E-6	0.86	0.88	0.02
63N-33E-9	0.58	0.57	0.01
39N-15E-12	1.11	1.06	0.05
42N-60E-6	0.55	0.53	0.02
45N-27E-6	1.83	1.71	0.12
TR-2B-16	0.58	0.58	0.04
48N-15E-9	1.23	1.19	0
Average	1.04	1.02	0.03

During the 2009 field visit, AJR collected 15 samples of mainly corestone material. The samples cover a range of saprolite alteration from fresh rock to altered rocks. In TR-03-09, some Garnierite Group minerals were sampled and have assayed at 4.26 % Ni. The intensity of alteration does not seem to correlate well with nickel content. The nickel grade within corestone appears to be linked with the possible presence of Garnierite within fractures of rocks.

Table 15. 4 - 2009 Corestone sample taken by AJR

SAMPLE NO.	Ni (%)	Description
RF_AJR_1_6	0.20	Altered corestone
RF_AJR_1_8	0.79	Altered corestone
RF_AJR_1_15	0.26	Fresh corestone
RF_AJR_2_4	0.69	Corestone
RF_AJR_2_6	0.57	Fresh corestone
RF_AJR_2_10	0.39	Corestone
RF_AJR_3_2	0.40	Rind
RF_AJR_3_15	1.01	Fresh corestone
RF_AJR_3_15A	1.09	Rind
RF_AJR_3_GAR	4.26	Grab garnierite
RF_AJR_4_3	1.24	Saprolite loose and porous
RF_AJR_4_5	1.47	Altered corestone
RF_AJR_4_6	1.53	Fresh corestone
RF_AJR_4_9	0.89	Altered corestone
RF_AJR_4_9A	1.86	Altered corestone

16. ADJACENT PROPERTIES

At present there are no metal mines in production in Oregon. The Nickel Mountain laterite deposit, located 60 miles north of the property, was in production between 1954 and 1976, and produced 39 million tons of ore with reported smelter feed grading of 1 % to 1.5 % Ni. The area also contains other nickel laterites which are described in Ramp (1978). The property is bordered to the west by private land owned by South Coast Lumber Co. from Brookings, Oregon.

RFN is also carrying out exploration on the Cleopatra deposit, another nearby nickeliferous laterite property in Curry County, Oregon, located around 50 miles south-east of the Red Flat property. There is also some active gold placer operations, north-east of the property along the Rogue River.

17. ORE PROCESSING AND METALLURGICAL TESTWORK

17.1 SMELTING TEST WORK

Metallurgical testing was first carried out by Hundhausen et al. (1954). They sampled 14.5 tons of material and performed petrographic and spectrographic analysis of composite samples, and conducted continuous smelting tests on a small 3-phase furnace unit. Table 17.1 presents the characteristics of the four original truck loads sent to the smelting research facility.

Table 17. 1 - Characteristics of smelter samples from Hundhausen et al. (1954)

Load	Drill hole area	Earthy material			Rock material		
		Dry Weight	Ni	Fe	Dry Weight	Ni	Fe
		(pound)	(%)	(%)	(pound)	(%)	(%)
1	15 and 16	5,861	0.68	42.0	533.3	0.39	14.6
2	15	8,071	0.86	31.3	1,022.4	0.67	10.0
3	16	8,714	0.78	17.4	770.3	0.72	9.3
4	23	6,415	0.84	25.1	1,416.0	0.98	13.1

Table 17.1 shows that the rock material is rich in nickel. Initially, Hundhausen et al. (1954) sorted the rock material in an attempt to increase the grade. However, upon further analysis the authors concluded that rock removal was not necessary because the rock contained mineralized nickel (see table 17.1). The smelting operation resulted in the recuperation of 94.5 % of the nickel charged to the furnace.

17.2 LEACHING TEST WORK

Two large samples were obtained from four trenches on the Red Flat property and five trenches on the Cleopatra property (AJR Geoconsulting, 2009). These samples were sent for analysis to the SGS laboratory in Lakefield, Ontario, Canada. The objectives of the analysis were to perform:

1. Chemical, grain size and mineralogical characterisation of the ore
2. Leaching program, including Bottle Roll Leach Testing and Agitated Leach Testing

Tables 17.2 and 17.3 present the characteristics of the samples sent to SGS from the Red Flat and Cleopatra properties, respectively. SGS received and prepared a total of 293 kg from Red Flat and 588 kg from Cleopatra, of wet material. Samples were separated into two composite fractions, the limonite (L) and the saprolite (S) fraction. Given that this analysis is a preliminary study and because the deposits are similar,

the limonite fraction and the saprolite fraction from both properties were blended together resulting in one blended limonite fraction and one blended saprolite fraction. The blended sample of limonite from both property totalled 193 kg of material and the blended sample of saprolite from both properties totalled 688 kg, for a total wet weight of 881 kg. The assay results in tables 17.2 and 17.3 are from samples collected by LLR.

At the time of writing this report, only grain size fraction distribution and chemical assay results were available. Mineralogical and leaching analyses were ongoing and the results were expected shortly. When available, the results will be presented in a separate report.

The fractional size analysis of the limonite fraction shows an average head grade of 1.08% Ni. With the -400 mesh fraction being high grade nickel (1.2% Ni). The majority of the nickel exists in the -400 mesh fraction. When screened at 400 mesh, 80.6% of the weight was recovered and the grade increased from 1.08% to 1.2% Ni. Figure 17.1 shows the assay results according with the grain size of the limonite.

For the saprolite fraction the average head grade is 1.08% Ni. The highest grade fractions are + 1inch and -100 mesh. When screened, keeping only the +1 inch and - 100 mesh, 70% of the weight was recovered and the grade increased from 1.08% to 1.3% Ni. Figure 17.2 shows the assay results according with the grain size of the saprolite.

Figure 17.3 shows the cumulative frequency of the different grain sizes. Figure 17.3 illustrates that the limonite is generally composed of finer material as 80 % passes through the 38 μ m sieve, whereas only 50 % of the saprolite passes through the 38 μ m sieve. Also, the saprolite fraction presents a coarse fraction of 10 % bigger than 20 mm.

RED FLAT NICKEL CORP.**Evaluation of the Red Flat Ni/Co Property Mining Potential,
Curry County, Oregon, U.S.A.****NI 43-101 TECHNICAL REPORT****17. Ore Processing and Metallurgical Testwork****Table 17. 2 - Characteristics of the samples from the Redflat property sent to SGS
for mineralogical and metallurgical testing**

Sample ID	Ore Type	Gross Wt	Net Wt*	Ni	Co	Cr	Fe	Mg	Fe/Mg
RF-M-1-1	L	5.83	5.55	0.795	0.071	1.66	36.1	3.31	10.91
RF-M-1-2	L	5.43	5.15	1.26	0.075	1.8	42	2.09	20.10
RF-M-1-3	S	4.67	4.39	1.23	0.104	1.64	36	4.79	7.52
RF-M-1-4	S	5.58	5.30	1.15	0.062	0.864	24.9	9.88	2.52
RF-M-1-5	S	6.11	5.83	1.06	0.046	0.695	22.8	10.95	2.08
RF-M-1-6	S	5.49	5.21	1.08	0.053	0.819	25.8	9.91	2.60
RF-M-1-7	S	6.21	5.93	1.14	0.047	0.958	21.8	11.2	1.95
RF-M-1-8	S	4.97	4.69	0.917	0.028	0.462	13.75	16	0.86
RF-M-1-12	S	12.64	12.36	0.629	0.022	0.38	11.1	17.9	0.62
RF-M-2-1	S	4.63	4.63	0.95	0.049	0.806	25.1	6.53	3.84
RF-M-2-2	S	4.65	4.37	0.783	0.024	0.401	12.3	16.9	0.73
RF-M-2-3	S	4.26	4.26	0.853	0.02	0.296	11.9	16.85	0.71
RF-M-2-4	S	4.88	4.60	0.457	0.024	0.41	14.6	12.75	1.15
RF-M-2-5	S	4.07	3.79	0.605	0.017	0.244	9.83	16.1	0.61
RF-M-2-6	S	4.92	4.92	0.521	0.015	0.213	9.3	17.2	0.54
RF-M-2-7	S	5.99	5.71	0.288	0.014	0.206	8.79	16.75	0.52
RF-M-2-8	S	4.53	4.53	0.283	0.014	0.206	8.83	17.15	0.51
RF-M-3-1	S	8.47	8.47	0.27	0.038	1.21	28.6	2.99	9.57
RF-M-3-2	L	9.49	9.21	0.745	0.029	1.84	46.4	1.09	42.57
RF-M-3-3	L	6.17	5.97	0.815	0.045	1.83	47.9	0.92	52.07
RF-M-3-4	L	9.38	9.10	0.821	0.098	1.91	44.3	1.07	41.40
RF-M-3-5	L	9.51	9.23	0.71	0.18	1.11	39.9	2.07	19.28
RF-M-3-6	L	8.51	8.51	0.782	0.199	1.07	40	2.17	18.43
RF-M-3-7	L	9.67	9.39	1.01	0.176	1.47	43.6	2.06	21.17
RF-M-3-8	S	8.27	8.27	0.765	0.125	0.968	34.8	5.04	6.90
RF-M-3-9	S	8.80	8.52	0.736	0.128	0.87	30.9	5.48	5.64
RF-M-3-10	S	8.19	8.19	0.882	0.126	0.894	32.2	4.51	7.14
RF-M-3-11	S	8.89	8.61	0.919	0.105	0.883	32.5	4.02	8.08
RF-M-3-12	S	8.01	8.01	1.02	0.086	0.823	29.1	4.76	6.11
RF-M-3-13	S	8.07	7.79	1.01	0.078	0.875	29.9	4.53	6.60
RF-M-3-14	S	7.43	7.43	0.979	0.086	0.82	29	6.29	4.61
RF-M-3-15	S	6.93	6.65	1.02	0.075	1.05	27.2	7	3.89
RF-M-3-21	S	9.55	9.55	1.44	0.066	0.628	24.8	7.08	3.50
RF-M-4-1	L	9.06	9.06	1.03	0.086	2.82	50	0.64	78.13
RF-M-4-2	S	9.77	9.49	1.25	0.22	2.07	39.9	4.53	8.81
RF-M-4-3	S	8.96	8.68	1.57	0.187	0.749	28.1	7.08	3.97
RF-M-4-4	S	9.85	9.85	1.75	0.166	0.795	28.4	6.79	4.18
RF-M-4-5	S	10.97	10.69	1.32	0.15	0.61	20.8	11.8	1.76
RF-M-4-6	S	10.41	10.41	1.66	0.179	1.03	29.5	7.19	4.10
RF-M-4-7	S	11.41	11.13	1.48	0.156	0.825	20.7	11.35	1.82

Total 293.43 kg
3.79 kg / sample in comp
40 samples
151.6 kg in comp

*Net Wt excludes plastic sample bag

Table 17. 3 - Characteristics of the samples from the Cleopatra property sent to SGS for mineralogical and metallurgical testing

Sample ID	Ore Type	Gross Wt	Net Wt*	Ni	Co	Cr	Fe	Mg	Fe/Mg
CL-M-1-1	L	15.16	14.88	0.58	0.093	2.49	40.6	2.42	16.8
CL-M-1-2	L	15.62	15.34	0.785	0.133	2.31	42.6	2.09	20.4
CL-M-1-3	L	14.82	14.54	0.841	0.192	2.47	47.5	1.57	30.3
CL-M-1-4	S	17.87	17.59	0.864	0.207	2.45	47.1	1.18	39.9
CL-M-1-5	S	9.37	9.09	0.954	0.202	2.13	46.4	1.25	37.1
CL-M-1-6	S	13.17	12.89	1	0.169	2.25	44.8	1.7	26.4
CL-M-1-7	S	19.81	19.53	1.055	0.148	1.75	40.1	3.76	10.7
CL-M-1-8	S	15.35	15.07	1.05	0.101	1.31	33.6	7.7	4.4
CL-M-1-9	S	12.28	12	1.38	0.149	1.76	39.2	4.37	9.0
CL-M-2-1	L	18.57	18.29	0.928	0.108	1.6	37.9	2.92	13.0
CL-M-2-2	L	17.27	16.99	1.085	0.078	1.28	34.2	4.31	7.9
CL-M-2-3	S	12.51	12.23	1.37	0.054	0.943	27.9	7.4	3.8
CL-M-2-4	S	10.04	9.76	1.29	0.066	0.993	28	7.16	3.9
CL-M-2-5	S	12.76	12.48	1.41	0.061	1.15	28.7	6.72	4.3
CL-M-2-6	S	13.23	12.95	1.3	0.047	0.824	23	10.15	2.3
CL-M-2-7	S	11.04	10.76	1.27	0.057	0.693	20.4	10.95	1.9
CL-M-2-8	S	10.05	9.77	1.37	0.047	0.671	20.4	11.65	1.8
CL-M-2-9	S	12.62	12.34	1.62	0.053	0.687	21.7	13.95	1.6
CL-M-2-10	S	17.34	17.06	1.39	0.055	0.702	19.25	11.3	1.7
CL-M-3-1	L	16.02	15.74	0.969	0.113	1.35	36.2	3.16	11.5
CL-M-3-2	S	9.92	9.64	1.15	0.13	1.51	38.6	2.99	12.9
CL-M-3-3	S	12.48	12.2	0.802	0.123	1.25	31.8	7.08	4.5
CL-M-3-4	S	9.89	9.61	1.02	0.123	1.19	31.6	6.18	5.1
CL-M-3-5	S	12.95	12.67	0.86	0.089	1.06	29.2	8.88	3.3
CL-M-3-6	S	11.3	11.02	0.969	0.074	0.992	27.3	9.53	2.9
CL-M-3-7	S	11	10.72	1.24	0.081	0.769	26.2	10.5	2.5
CL-M-3-8	S	9.13	8.85	0.913	0.058	0.59	20.2	14.05	1.4
CL-M-3-9	S	10.41	10.13	1.32	0.088	0.848	22.6	10.35	2.2
CL-M-3-10	S	10.41	10.13	1.68	0.091	1.43	31.3	6.35	4.9
CL-M-3-11	S	10.1	9.82	1.505	0.107	1.1	28.8	8.52	3.4
CL-M-3-12	S	13.25	12.97	1.57	0.093	0.85	28.5	8.1	3.5
CL-M-4-1	L	13.55	13.27	0.836	0.102	1.28	34.8	2.75	12.7
CL-M-4-2	L	10.47	10.19	1.15	0.14	1.5	37.9	3.09	12.3
CL-M-4-3	S	9.14	8.86	1.4	0.147	1.53	41.6	1.62	25.7
CL-M-4-4	S	10.06	9.78	1.485	0.181	1.42	44.6	1.03	43.3
CL-M-4-5	S	11.49	11.21	1.695	0.152	1.72	40.5	2.25	18.0
CL-M-4-6	S	8.85	8.57	1.63	0.171	2	42.4	1.7	24.9
CL-M-4-7	S	10.94	10.66	1.675	0.142	1.36	40.2	2.63	15.3
CL-M-4-8	S	8.48	8.2	1.36	0.117	1.23	33.5	5.81	5.8
CL-M-4-9	S	8.2	7.92	1.35	0.133	1.45	35.8	4.59	7.8
CL-M-4-10	S	6.87	6.59	1.23	0.116	0.947	23.7	10.5	2.3
CL-M-4-11	S	6.46	6.18	1.39	0.106	1.18	28.9	7.86	3.7
CL-M-4-12	S	9.81	9.53	1.25	0.136	1.13	25.7	8.89	2.9
CL-M-5-1	L	12.2	11.92	1.23	0.137	1.83	42.3	1.65	25.6
CL-M-5-2	S	9.6	9.32	0.919	0.047	0.864	25.3	11.4	2.2
CL-M-5-3	S	10.93	10.65	1.1	0.078	0.984	25.5	11.45	2.2
CL-M-5-4	S	12.01	11.73	1.695	0.135	1.65	38.2	4.16	9.2
CL-M-5-5	S	10.9	10.62	0.583	0.042	0.641	14.9	17.5	0.9
CL-M-5-6	S	8.54	8.26	1.17	0.07	1.48	30.7	8.34	3.7
CL-M-5-7	S	8.42	8.14	0.72	0.026	0.521	15.2	16.7	0.9
CL-M-5-8	S	9.77	9.49	0.862	0.036	0.624	16.2	16.1	1.0
Total			588.15	kg					
			6.18	kg / sample in comp					
			51	samples					
			315.18	kg in comp					

*Net Wt includes plastic sample bag

18. MINERAL RESOURCE AND MINERAL RESERVE ESTIMATION

18.1 GENERAL

The 2007 drilling program validated the 1954 USBM and 1978 DOGAMI drill data. The 2008 drilling program had two objectives: continue the surface and sub-surface auger sampling; and define the depth extension and sample the corestones and bedrock with sonic drilling. In 2009, mechanical trenching was conducted to obtain more accurate geological profiles and to increase the knowledge of the resource.

The locations of the USBM and DOGAMI holes were selected based on the reports from Hundhausen et al. (1954) and Ramp (1978), with an estimated accuracy of ± 50 ft. AJR considered that the inaccuracy in the location of the samples would not significantly affect the resource calculations. The drill holes were integrated in such a way as to minimize the risk of error and ensure that the estimate is as precise as possible. The auger testing conducted in 2007 and 2008 followed a 300 x 300 ft grid. The sonic drill holes and the trenches are located in the most prospective areas where existing roads were available.

18.2 RESOURCE CATEGORY DEFINITIONS

18.2.1 Measured Mineral Resource

As defined by the CIM:

A Measured Mineral Resource is the part of a mineral resource for which quantity, grade or quality, densities, shape, and physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration, sampling and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough to confirm both geological and grade continuity.

18.2.2 Indicated Mineral Resource

As defined by the CIM:

An Indicated Mineral Resource is the part of a mineral resource for which, quantity, grade or quality, densities, shape, and physical characteristics, can be estimated with a level of confidence sufficient to allow the appropriate application of technical and economic parameters, to support mine planning and evaluation of the economic

viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough for geological and grade continuity to be reasonably assumed.

18.2.3 Inferred Mineral Resource

As defined by the CIM:

An Inferred Mineral Resource is the part of a mineral resource for which quantity and grade or quality can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes.

18.3 DEFINITION OF RESERVE CATEGORIES

18.3.1 Proven Mineral Reserve

As defined by the CIM:

Proven Mineral Reserve is the economically minable part of a Measured Mineral Resource demonstrated by at least a Preliminary Feasibility Study. This study must include adequate information on mining, processing, metallurgical, economic, and other relevant factors that demonstrate, at the time of reporting, that economic extraction is justified.

18.3.2 Probable Mineral Reserve

As defined by the CIM:

Probable Mineral Reserve is the economically minable part of an Indicated, and in some circumstances, a Measured Mineral Resource, demonstrated by at least a Preliminary Feasibility Study. This study must include adequate information on mining, processing, metallurgical, economic and other relevant factors that demonstrate, at the time of reporting, that economic extraction can be justified.

18.4 MINERAL RESOURCE

The resource estimate covers lobe A, lobe B, lobe C and lobe D but the measured resource category is limited to lobe A. Data used in the resource estimate came from the 2007 and 2008 auger testing programs, the 2008 sonic drilling program, the 2009 mechanical trenching and also from historical validated drilling data from USBM and DOGAMI. Two cut-offs, 0.7 and 0.8% Ni, (selected to obtain an average grade as

close as possible to 1 % Ni) were used to report resource estimates. While data analysis indicates cobalt, chrome and iron as potential sub-product, the actual resource estimate does not include these elements.

The measured resource was calculated using the half distance method (the limit of the zone of influence for each hole or trench was set at half distance between holes or trenches). The indicated and the inferred resources were calculated using a geostatistical model and block kriging estimates.

Data from the 2008 sonic drilling and the 2009 trenching show corestone and bedrock mineralization (see table 11.1 and 12.1). Hence, the resource is divided into soil and rock.

Inferred resources are based on the hypothesis that nickel mineralization occurs at depths down to 16 ft. This hypothesis is supported by the drilling, mapping and smelting work of Ramp (1978) and Hundhausen et al. (1954).

Table 18.1 presents the statistical parameters for the 473 of 670 auger hole performed by LLR which is included in the resource. Table 18.2 shows the average auger hole depth and mineral grade for two different cut-offs.

Table 18. 1 - Statistical information of auger hole population using a 0.5% Ni cut-off resource (number of samples = 473)

Parameter	Average	Standard deviation	Minimum	Maximum
Ni (%)	0.82	0.23	0.50	1.60
Co (%)	0.06	0.03	0.02	0.27
Cr (%)	0.95	0.41	0.25	2.72
Fe (%)	23.99	7.99	6.97	50.00
Mg (%)	9.26	4.09	0.57	19.80
Borehole depth (ft)	9.30	3.29	3.00	21.00

Table 18. 2 - Auger holes soil sample average value for the cut-offs

Cut-Off	Average depth	Ni (%)	Co (%)	Cr (%)	Fe (%)	Mg (%)	nb. of sample
0.7	9.68	0.94	0.07	1.05	26.39	8.28	307
0.8	10.68	1.03	0.07	1.10	27.68	7.90	236

Table 18.3 presents the resource estimates. On table 18.3, the block kriging average grade differs from the borehole results in table 18.2. This is due to the weighting effect of kriging in a 2D plane space, which depends on borehole locations and Ni grades of the extrapolated blocks. Block-by-block kriging results and a breakdown of the calculation and hypothesis for the depth extension are listed in Appendices C and H respectively.

Table 18. 3 - Summary of the resources estimation results in US Tons

Cut-off Ni (%)	Type	Measured Tons (*1000) Ni (%)		Indicated Tons (*1000) Ni (%)		Inferred Tons (*1000) Ni (%)		Total Inferred Tons (*1000) Ni (%)	
0.7	Soil	1,710	0.91	3,218	0.81	4,169	0.80	9,097	0.82
	Rock	2,277	1.05	3,218	0.81	4,169	0.80	9,664	0.89
	Total	3,987	0.99	6,436	0.81	8,338	0.80	18,761	0.84
0.8	Soil	1,700	0.91	1,684	0.88	1,728	0.88	5,112	0.89
	Rock	2,007	1.10	1,684	0.88	1,728	0.88	5,419	1.00
	Total	3,707	1.01	3,368	0.88	3,686	0.88	10,531	0.92

As a first step, the resource volume was calculated. The total volume was divided into two parts, the rock volume and the soil volume. In some areas, the rock material is not mineralised and was not included in the resource (resource block no. 1, 2, 9 and 11 from table 18.8). But in other areas, where there were nickel-rich rocks, the rock material was included in the resource.

The two volumes were then converted into tons by multiplying the weighed dry density average of 0.75 g/cm³ (50 lbs/ft³) for soils and 2.5 g/cm³ (150 lbs/ft³) for rock. Density measurements were done on limonite/saprolite clay samples and on rock samples.

18.4.1 Bulk Density

The Bulk Dry Density was measured on nine in place large samples of 1 ft³. In situ dry bulk density values are important to evaluate the available bulk dry resource tonnage that can be associated with a metal weight percentage measured on dry samples. Laterites are composed of two different density materials, a limonitic/saprolitic porous clay with low dry density and corestones and saprolite bedrock which consists of heavy ultramafic rocks with higher density. The 2008 sonic drill holes and the 2009 trenching allowed RFN to sample and measure the nickel grade of the corestones and the percentage of corestones in the resource.

Nine large soil samples of around 1 ft³ in volume were collected by LLR and carefully measured for the volume and the wet and dry weights. Figure 18.1 presents the procedures used. Results of in place soil density tests are presented on table 18.4. Soil density samples are located on Map 1, in Appendix A. The average dry bulk density of table 18.5 is 0.75 g/cm³, which is about 50 lbs/pi³.

The literature reports limonitic/saprolitic clay density varies from 0.5 to 2 g/cm³, with average values around 1.0 (Golightly, 2005; Gleeson et al., 2004; see Appendix G). Gleeson et al. (2004) have reported density values from the Eight Dollar Mountain Deposit in Oregon.

Also, 12 rock samples of fist size were collected by LLR for density measurements. Results of rock density tests are presented on table 18.5. The average dry bulk density of table 18.5 is 2.5 g/cm³, which is about 150 lbs/pi³.

Table 18. 4 – In place large scale density measurements on lominitic/saprolitic clay material

Sample no.	Depth (ft)	Location		Bulk Wet Density (g/cm ³)	Bulk Dry Density (g/cm ³)	Moisture Content (%)	Nickel Grade (%)
		X	Y				
2008-1	1	3896110	269424	1.457	30.00	1.016	-
2008-2	1	3896421	270081	1.343	39.50	0.769	-
2008-3	1	3896193	270620	1.350	37.30	0.818	-
2009-1	5	3895742	277368	1.382	39.22	0.83	0.94
2009-1	9	3895742	277368	1.729	41.59	1.00	0.59
2009-3	7	3895315	270918	1.436	40.71	0.85	1.04
2009-3	12	3895315	270918	1.363	52.84	0.65	1.18
2009-3	16	3895315	270918	1.385	55.60	0.62	1.18
2009-4	4	3896402	270087	1.091	46.22	0.59	1.70
Average				1.393		0.794	

The average is 0.794 g/cm³ (± 50 lbs/ft³) in table 18.4 represent the value used in the estimation.

Table 18. 5 – Rock density measurements results

Sample no.	Bulk Dry Density (g/cm³)	Weight (lb/ft³)
1	2.1	131.37
2	3.88	241.96
3	2.32	144.68
4	2.33	145.27
5	2.57	160.29
6	2.34	145.91
7	2.81	175.26
8	2.42	151.05
9	2.34	146.16
10	2.36	147.03
11	1.98	123.39
12	2.22	138.64
Average	2.47	154.25

Table 18.5 shows the average is 2.5 g/cm³ (± 150 lbs/ft³), which represents the value used in the estimation.

18.4.2 Methods Used in the Resources Estimations

The measured resources were calculated using the conventional tributary area method. Measured resources were divided in blocks with a minimum of one sonic drill hole or one trench. The depth of the blocks varies according with the isocontours model presented in figure 18.4. Those isocontours were determined using USBM, sonic drill and trench information. The nickel grade for the soil fraction was based on results from USBM, DOGAMI, Auger drilling, sonic drilling and trenching. The nickel grade for the rock fraction was estimated using the results from the sonic drill holes and the trenches.

For the indicated and inferred resources, the rock percentage and the rock mineralization were assumed based on the results from the measured resource. Hence, 40 % of the volume of the indicated and inferred resource was assumed to be composed of rock and the total resource volume was divided into three types of material: soil, waste rock and resource rock. The breakdown of the resource is summarized in table 18.6.

Table 18. 6 - Volume fraction and resource assumptions

Fraction	(%)	Type of material	(%)
Rock	40	Waste	20
		Resource	20
Soil	60	Resource	60

Twenty per cent of the rock volume is mineralized, and the other 20 % is considered waste material because it has less the 0.5 % Ni. The nickel grade of the rock fraction is assumed to be the same as that of the soil fraction. In other words, when the soil grade is below cut-off, the rock grade will also be below cut-off.

The nickel grade of the soil fraction was calculated using the kriging method, which is a geostatistical method (Journel and Huijbregts, 1991). A block pattern of 300 ft by 300 ft was defined over the entire property. The 300 ft x 300 ft block size was chosen to fit the claim (600 x 1,500 ft) fraction and to ensure that there was at least 1 hole in each block. It was also chosen because this spacing is well under the variogram range of 1,300 ft (see table 18.6 and figure 18.6).

All boreholes were used for the block estimate of Ni grade. Statistical analysis of the data includes frequency distribution analysis and variogram definition. Kriging was used to define the nickel grade of each block. The depth of the block was set at 8 ft, which is conservative given the higher values presented in tables 18.1 and 18.2.

The detailed block kriging results are included in Appendix C and detailed resource calculations are presented in appendix H. The software used was GS+ ver. 9.0 developed by Gamma Design Software, LLR. Figures 18.2 and 18.3 present the histograms of Ni and Co respectively.

Theoretical variogram parameters used for the kriging are shown on table 18.7. The variogram is isotropic. It can be observed that the range for the Ni value is 1,300 ft, which is more than 4 times the sampling spacing of 300 ft.

Table 18. 7 – Variograms parameters for Ni

Parameter	Variogram type	Nugget effect	Sill	Range (ft)
Ni (%)	Spherical	0.04 % ²	0.07 % ²	1300

18.4.3 Measured Resources

The measured resource is limited to the area where the corestone information is available from the USBM drill holes, the sonic drill holes and the trenches. The measured resource area is located in lobe A, where corestone was sampled and assayed.

The measured resource was divided into the 11 blocks presented on figure 18.4. The percentage of soil and rock for each block was calculated using table 11.1 and table 12.1. The depth model is also illustrated in figure 18.4. The volume of each block was calculated with the block area integrated over the depth surface (accounting for

the depth variation inside the block). The block volume was separated into soil and rock parts. Table 18.8 present the summary of measured block parameters.

Table 18. 8 – Summary of measured resources block parameters

Block no.	Information source		Volume of block (ft ³)	Soil ¹				Rock ²			
	Sonic hole	Trenches		(%)	Volume of soil (ft ³)	Tons of soil (ton US)	Ni (%)	(%)	Volume of rock (ft ³)	Tons of rock (ton US)	Ni (%)
1	9	TR2	9445000	50	4722500	118063	0.81	50	4722500	0	< 0.5
2	11		12098000	50	6049000	151225	0.98	50	6049000	0	< 0.5
3	5		7151000	62	4433620	110841	0.86	38	2717380	203804	0.57
4	8		15105000	57	8609850	215246	0.85	43	6495150	487136	0.88
5		TR3	12647000	65	8220550	205514	0.95	35	4426450	331984	0.92
6	7		19085000	40	7634000	190850	0.85	60	11451000	858825	1.26
7	4		10542000	70	7379400	184485	0.90	30	3162600	237195	0.69
8	6		12796000	60	7677600	191940	0.87	40	5118400	383880	0.58
9	3		14051000	80	11240800	281020	0.95	20	2810200	0	< 0.5
10		TR4	4168000	70	2917600	72940	1.30	30	1250400	93780	1.4
11	10		769000	60	461400	11535	0.75	40	307600	0	< 0.5

1. Soil density = 50 lb/ft³

2 Rock density = 150 lb/ft³

The percentage of each block of soil and rock was based on sonic drill and/or trench information. Nickel concentration contours for soil are presented in figure 18.5. The rock fraction was considered mineralized only when average corestone grade was above 0.5 % Ni. When the average corestone grade is under 0.5 % Ni, the rock fraction was not included in the resource. For example, in table 18.8, for blocks no. 1, 2, 9 and 11, the rock fraction was set to zero. Hence, it is not considered part of the resource.

The total resource is the sum of all the blocks with a grade greater than the cut-off grade. The measured resources area is located on Map 4.

18.4.4 Indicated Resource

The indicated resource is limited to the area within 300 ft from an existing auger hole. The indicated resource depth is limited to 8 ft and no depth extension is included in the indicated category. The indicated resource is the sum of the 300 ft X 300 ft blocks, and the resource was estimated using block kriging only. Each block has a Ni grade based on the variogram and a block estimation variance, which gives a level of confidence in the estimation. The volume of each block was separated into two fractions, the soil fraction and the rock fraction. Based on the rock content and the mineralization found in the measured resource area, it is assumed that the indicated

resource is composed of 60 % soil and 40 % rock as described in table 18.6. The resources are calculated with the following equation:

- Block volume = 300 ft x 300 ft x 8 ft.
- The block volume is divided into two fractions:
 - o 60 % of total volume = the soil volume
 - o 40 % of total volume = the rock volume
- Only 20 % of the rock volume is assumed mineralized with the same grade as the soil.
- Block resource (tons)= (Soil volume x 50 lbs/ft³) /2,000lbs/ton + (Mineralized rock volume x 150 lbs/ft³) /2,000lbs/ton.

The total resource is the sum of all the blocks with a grade greater than the cut-off grade. The indicated resources area is located on Map 4.

18.4.5 Inferred Resources

The inferred resource represents the resource beyond 300 ft of an existing auger hole and below the indicated resource for depths between 8 ft and 16 ft. The volume of each block was separated into two fractions, the soil fraction and the rock fraction. Based on the rock content and the mineralization found in the measured resource area, it is assumed that the indicated resource is composed of 60 % soil and 40 % rock as described in table 18.6.

Nickel grade for the inferred resource is assumed to be the same than for the indicated. This assumption is considered conservative because the available information seems to indicate that there is enriched nickel in the lower parts of the deposit (see figure 8.5). The inferred resource area is located on Map 4.

19. OTHER PERTINENT DATA AND INFORMATION

There is no other pertinent data and information.

20. INTERPRETATION AND CONCLUSIONS

1. Garnierite concentration was found within the corestones during the 2009 trenching program, which confirmed the USBM observations. Garnierite accumulation seems to be present underneath high grade soil ($> 1\%$ Ni) and chip samples of garnierite assayed as high as 4.3% Ni.
2. The measured resource was estimated using USBM, sonic drill holes and trench information. The measured resource was split into soil and rock fractions based on the results from the closest sonic hole or trench. The measured resource uses known depths and density parameters. The measured resource covers 181 acres at an average measured depth of 16 ft.
3. The indicated and inferred resources were estimated using conservative assumptions of 60% soil and 40% rock fractions. Half of the rock fraction (20%) is mineralized and the other half (20%) is considered waste.
4. Variogram results show that the Ni (%) grade has a range of 1,300 ft and that the sample grid spacing of 300 ft was adequate and that no in-between holes are required.
5. The deposit shows a strong horizontal continuity of the Ni grade and historical USBM and DOGAMI holes correlate well with the 2007, 2008 and 2009 results. Some local important Ni grade variations were observed but those variations occur at grades that are well above the cut-offs.
6. The depth of the laterite accumulation for the inferred resource area is assumed to be 16 ft (as stated in the report), but according to Hundhausen et al. (1954) it might extend down to 50 ft. This assumption of 16ft is also supported by the sonic drill hole data and the auger data.
7. The geological and chemical verifications performed by AJR agree with the data collected by LLR.
8. The soil bulk dry density of the resource was measured in place and ranges from 0.59 g/cm^3 to 1.01 g/cm^3 for clayed limonitic material. The rock density was also measured and ranges from 1.98 g/cm^3 to 3.88 g/cm^3 . The average soil density is 0.75 g/cm^3 (50 lbs/ft^3) and the average rock density is 2.5 g/cm^3 (150 lbs/ft^3).

21. RECOMMENDATIONS

In no particular order, the recommendations are as follows:

1. Define the depth of the property in lobes B and C through geophysical surveys.
2. Define the thickness of the indicated and inferred zones and upgrade the indicated and inferred resource category with sonic drilling.
3. Increase the number of corestone samples, especially outside the measured resource area, through additional trenching.
4. To carry auger testing program to complete the 300 ft x 300 ft grid, to verify the extension of the high grade soils.
5. Develop a mining scenario adapted to the geometry and the parameters of the deposit.
6. To realize required pre-feasibility and feasibility studies.

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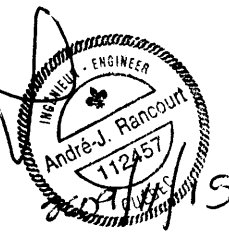
23. SIGNATURE PAGE

NI 43-101 evaluation of the mining potential of Red Flat nickel/cobalt property

Prepared for:

Red Flat Nickel Corp.
888 SW Fifth Avenue, Suite 300
Portland OR
97204-2089


André J. Rancourt, Eng., M.A.Sc.



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St-Jean, Québec
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**24. SUPPLEMENTARY RULES FOR TECHNICAL REPORTS ON PROPERTIES
AT THE DEVELOPMENT STAGE AND PROPERTIES IN PRODUCTION**

Currently, the property is only at the exploration stage.

25. PERMIT MAP

Map 01 is attached in Appendix A.

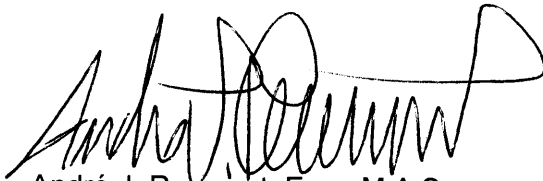
26. CERTIFICATE OF AUTHOR AND CONSENT

I, André J. Rancourt, of St-Jean (Québec), Canada, certifies that:

1. I am a geological engineer, president of AJR Geoconsulting Inc., I reside at 129, Brais, St-Jean (Québec) Canada, J3B 7W4.
2. I graduated from École Polytechnique de Montréal in geological engineering (coop program) in 1993 and I have received my master in mining in 1996.
3. I am a member of the Ordre des Ingénieurs du Québec. Licence No. 112457.
4. I have worked since 1993 as project engineer for several mining, civil and hydro-electric projects around the world.
5. I have read the definition of qualified persons as defined in Regulation 43-101 (NI-43-101). I certify that, given my education, my experience and the nature of the mining project covered by this report, I have the technical capacity required by NI 43-101.
6. I am responsible for the preparation of the technical report entitled Evaluation of the Mining Potential of the Red Flat Nickel/Cobalt Property, Curry County, Oregon, U.S.A., dated November, 2009.
7. I hereby certify that I had no interest in Red Flat Nickel Corp. or the Red Flat property on the date this report was produced, and that I meet the criteria for independence as defined in Section 1.4 of NI 43-101.
8. I attest that, to the best of my knowledge, the report contains all the scientific and technical information that is required to be disclosed so as not to make it misleading.
9. I have read NI 43-101, and the technical report has been prepared in compliance with the instrument.
10. I, André J. Rancourt, consent to the publication of the technical report Evaluation of the Red Flat Ni/Co Property Mining Potential, Curry County, Oregon, U.S.A. and to the inclusion of extracts or a summary of the report of the written information to be filed in 2009 and 2010, by Red Flat Nickel Corp., and to the publication of the technical report and the filling of the report with the securities regulatory authorities.

11. I, André J. Rancourt, undertake to review the written information to be filed in 2009 and 2010 by Red Flat Nickel Corp., and to ensure that it accurately reflects the information contained in this technical report.

Signed in St-Jean, Québec, Canada on November 15th, 2009,



André J. Rancourt, Eng., M.A.Sc.

27. ILLUSTRATIONS



Figure 4. 1 - – Typical corner claim post



Figure 4. 2 - Typical drilling near a claim post



Figure 5. 1 - Typical vegetation on the property



Figure 8. 1 - Typical corestone content



Figure 8. 2 - Bedrock outcropping in lobe A



Figure 8. 3 - Typical exploration trench by the USBM



Figure 8. 4 - Typical exploration trench by the USBM

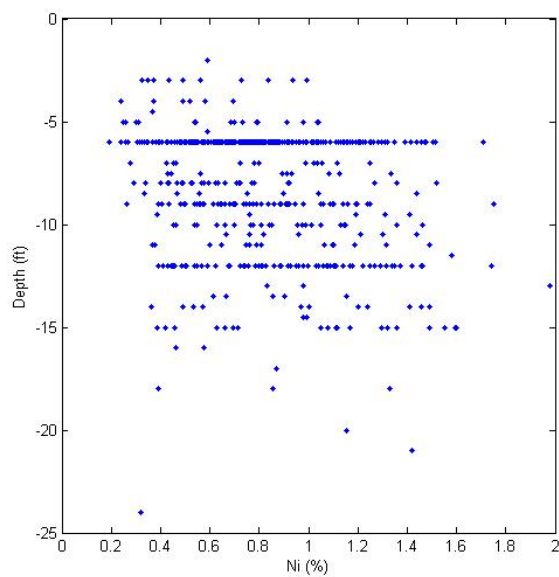


Figure 8. 5 - Variation of Ni versus depth (data 2007)

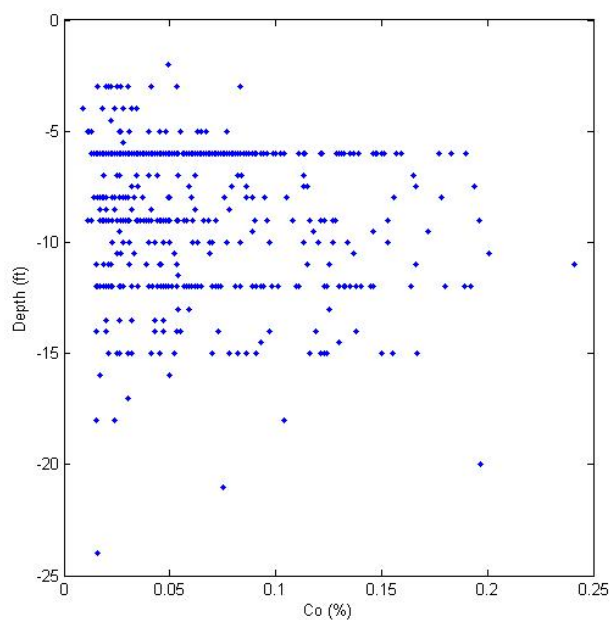


Figure 8. 6 - Variation of Co versus depth (data 2007)

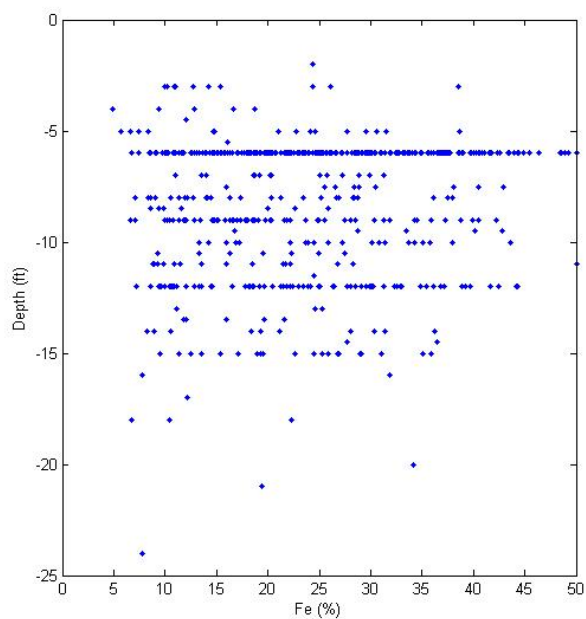


Figure 8. 7 - Variation of Fe versus depth (data 2007)

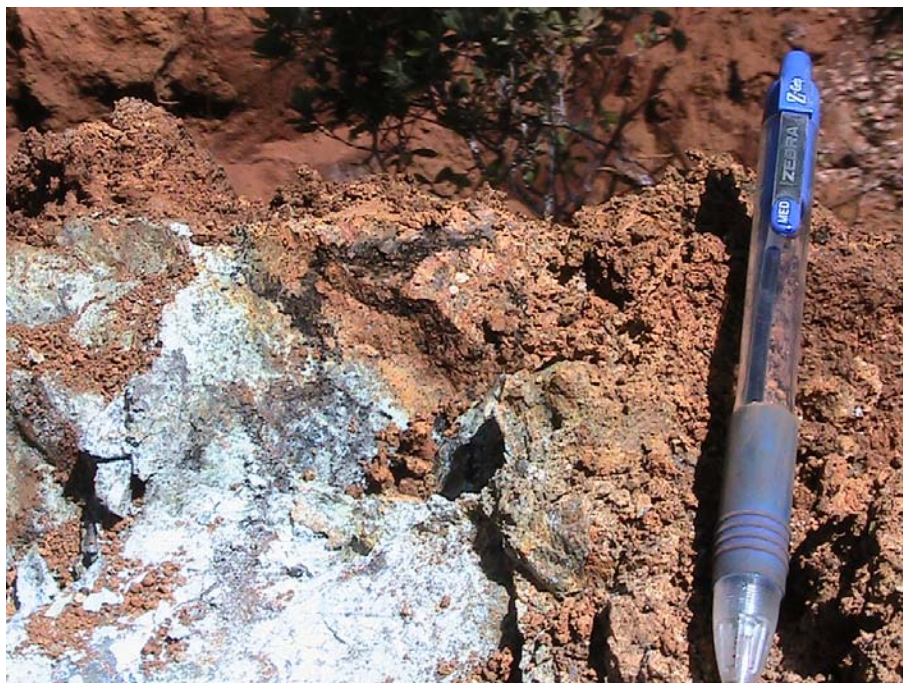


Figure 9. 1 - Garnierite group minerals (bluish) found in trench 2009-03

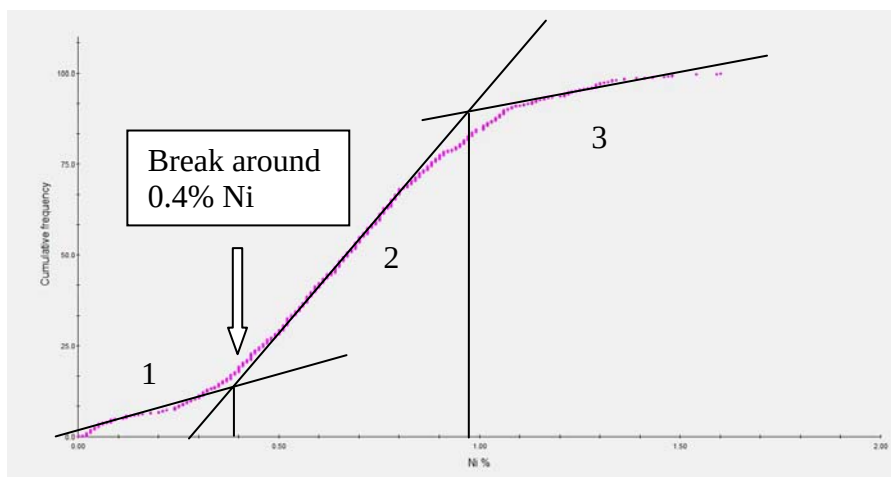


Figure 9. 2 - Cumulative frequency of the samples Ni grade



Figure 11. 1 - Sonic drilling operation



Figure 11. 2 - Sample handling from the sonic drilling



Figure 11. 3 - Auger drilling operation – Photo 1

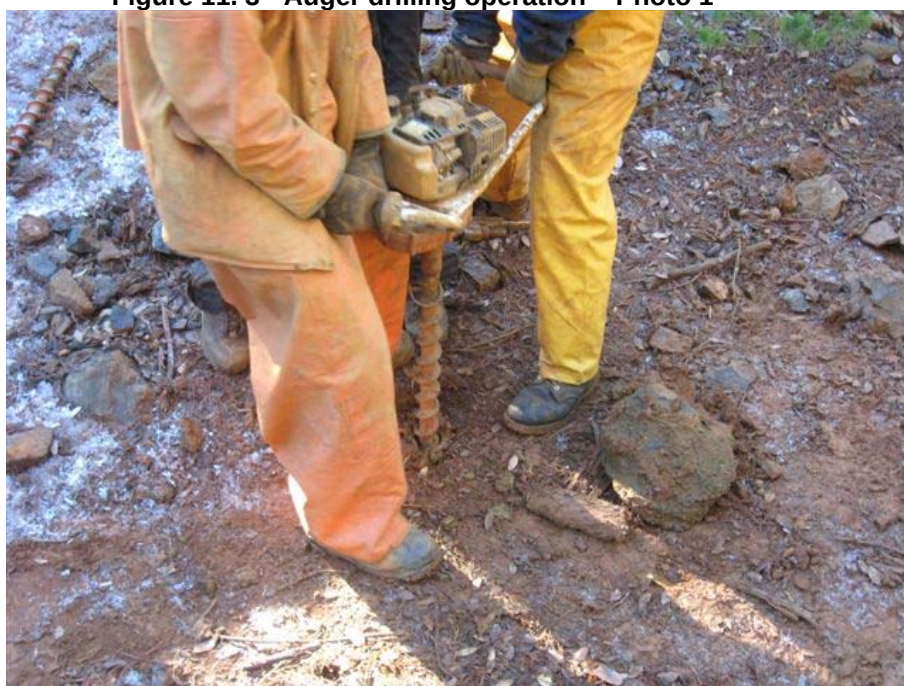


Figure 11. 4 - Drilling operation – Photo 2



Figure 12. 1 – Mechanical trench 09-01



Figure 12. 2 - Mechanical trench 09-02



Figure 12. 3 – Mechanical trench 09-03



Figure 12. 4 - Mechanical trench 09-04



Figure 12. 5 - Typical soil and corestone profile (trench no. 4)



Figure 12. 6 - Typical corestone rind with garnierite (trench no. 3)



Figure 13. 1 - Typical 6 feet sample



Figure 13. 2 - Systematic rod cleaning between sampling runs

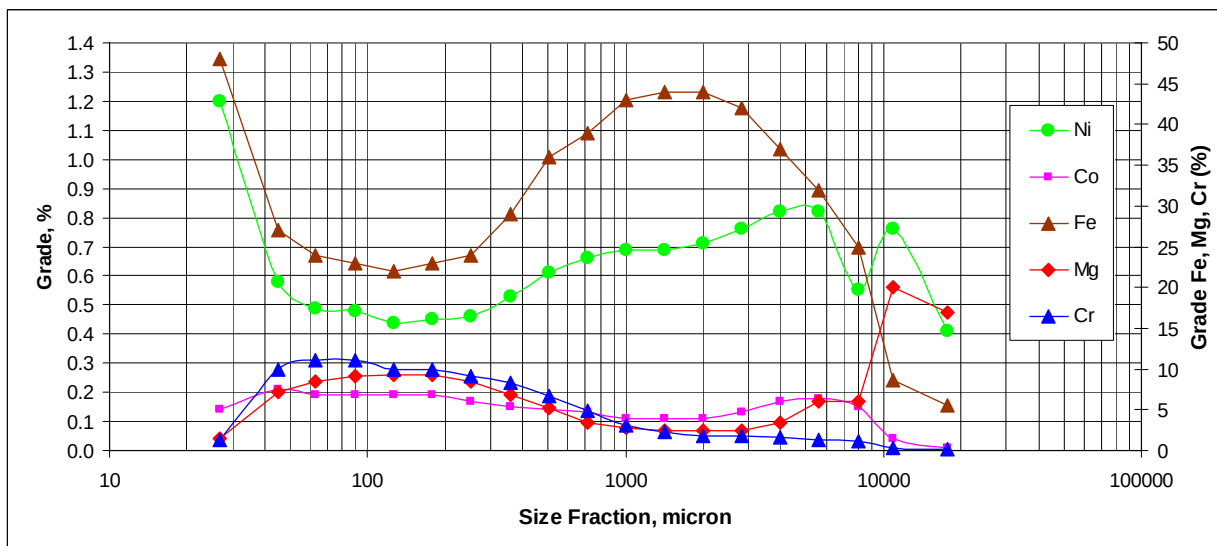


Figure 17. 1 – Assay results according with grain size for the limonite composite sample

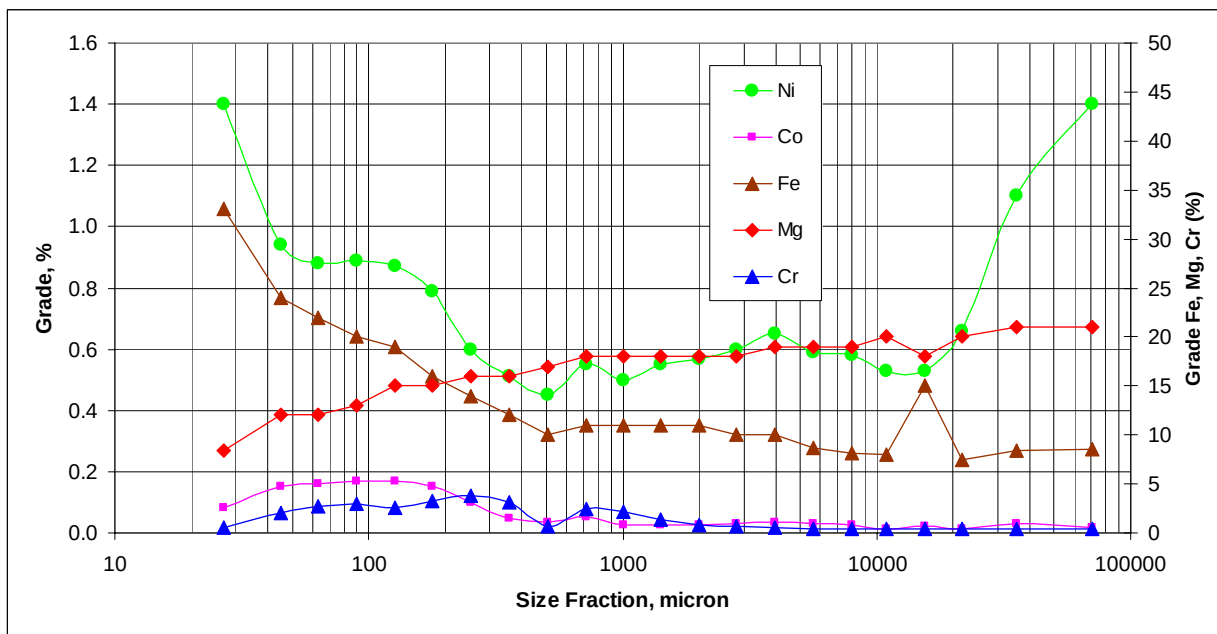


Figure 17. 2 – Assay results according with grain size for the saprolite composite sample

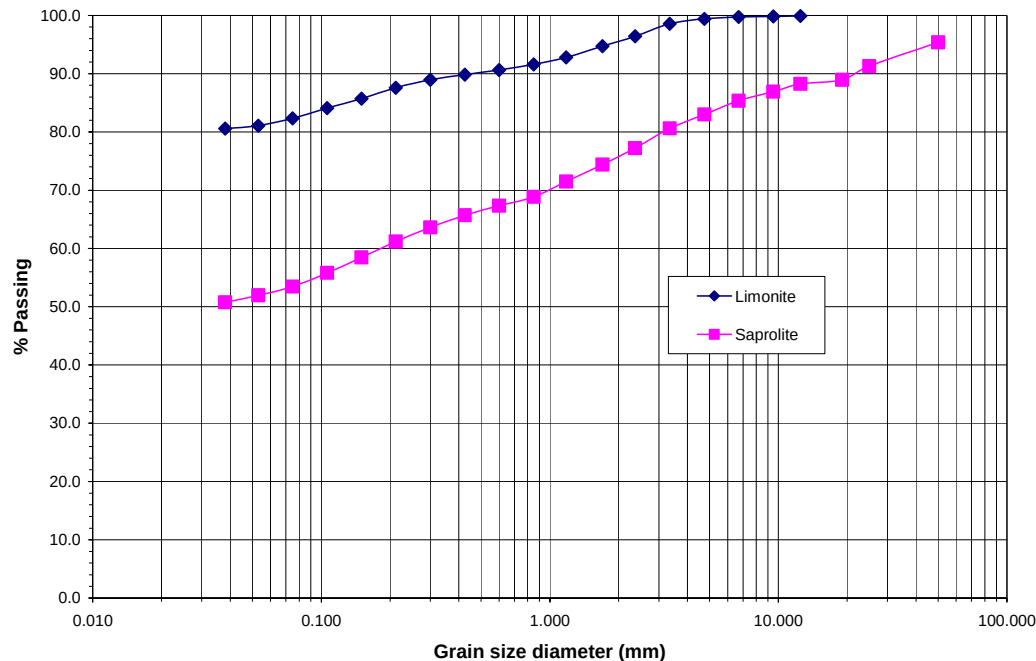
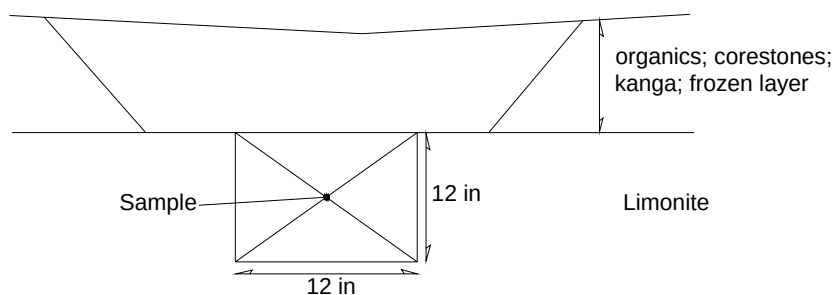


Figure 17. 3 – Cumulative frequency of the different grain size for the limonite and the saprolite fraction



Notes :

Procedure for in place density test

1. Remove the organic cover layer
2. Prepare an horizontal surface
3. Excavate a hole of approximately 12 in X 12 in
4. Carefully sample all the excavated material
5. Measure the exact volume of the hole with pre-measured volume of sand
6. Weight the wet sample (in place density)
7. Oven dry the sample
8. Weight the dry sample (in place dry density)

Figure 18. 1 - In place density sampling procedure

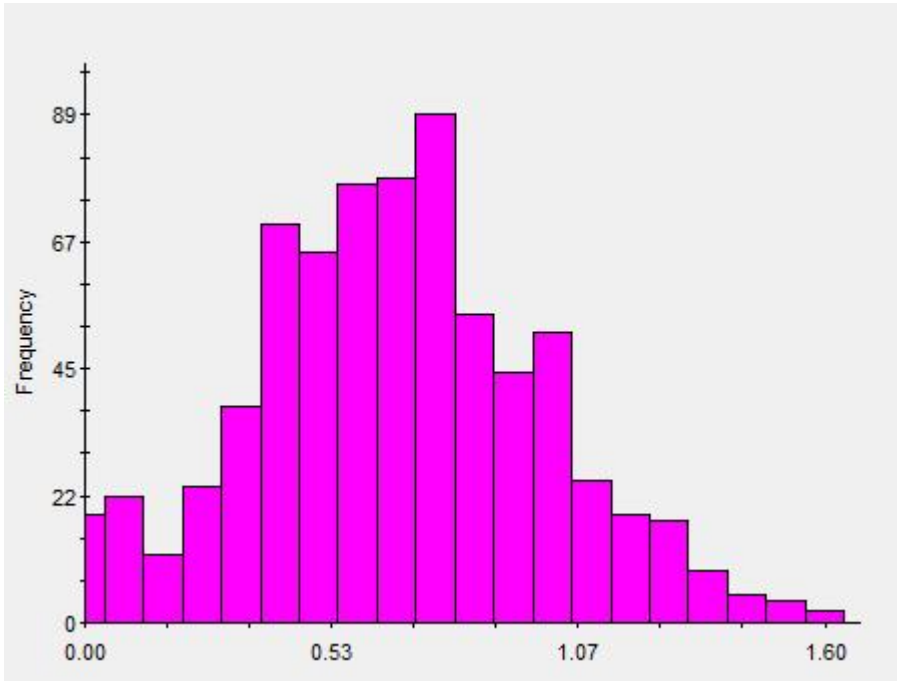


Figure 18. 2 - Histogram of Ni

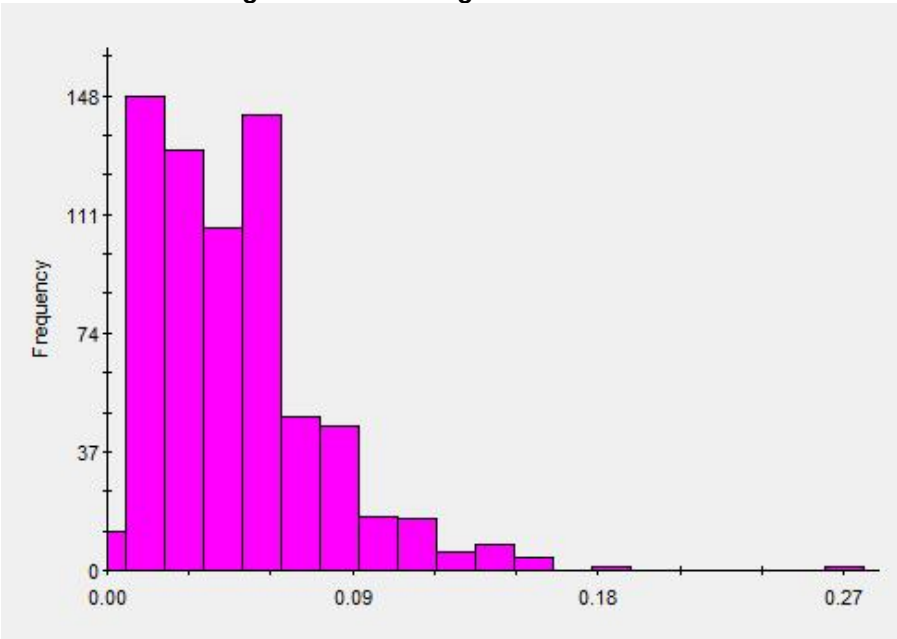


Figure 18. 3 - Histogram of Co

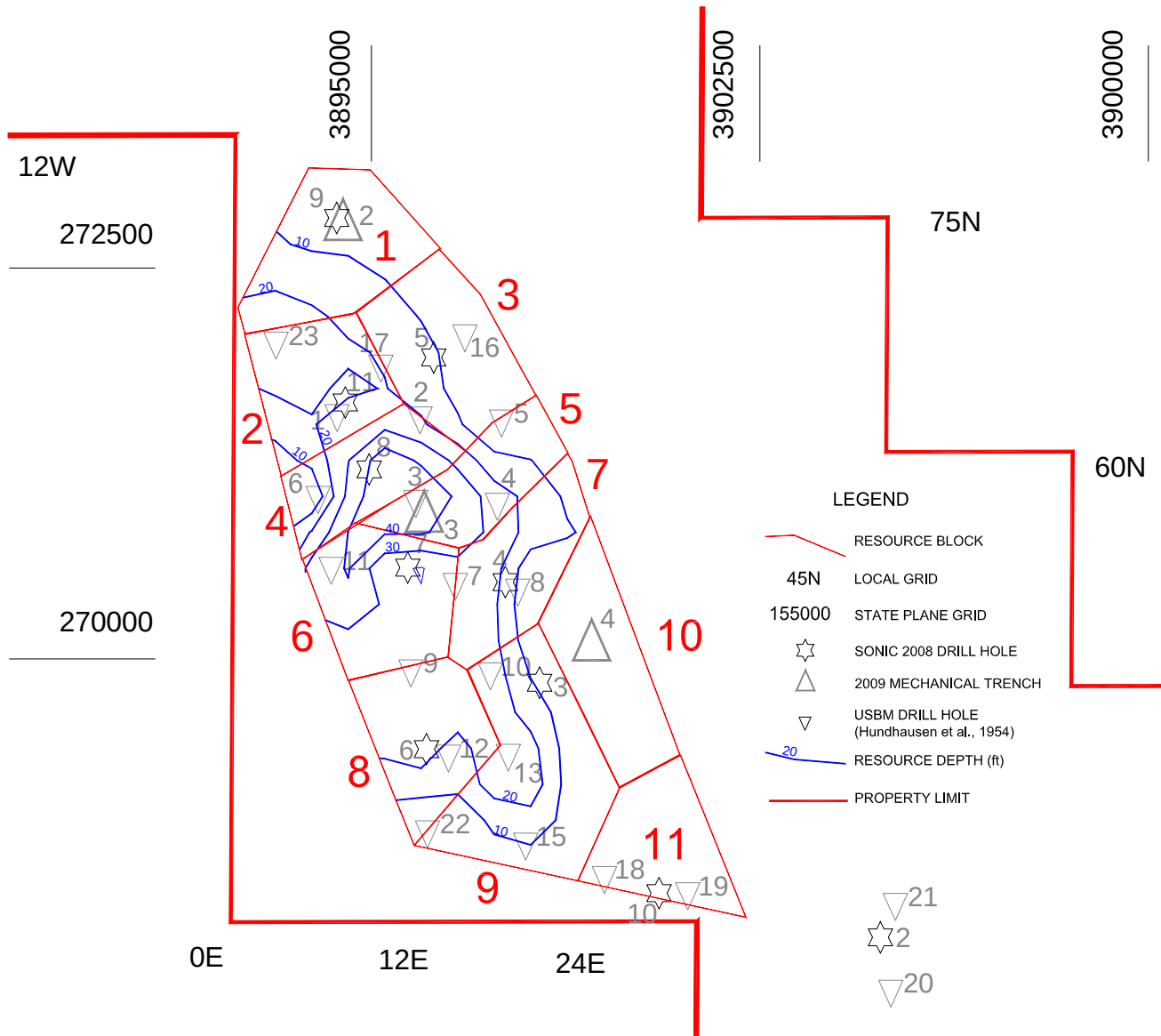


Figure 18. 4 - Measured resource block locations with depth model

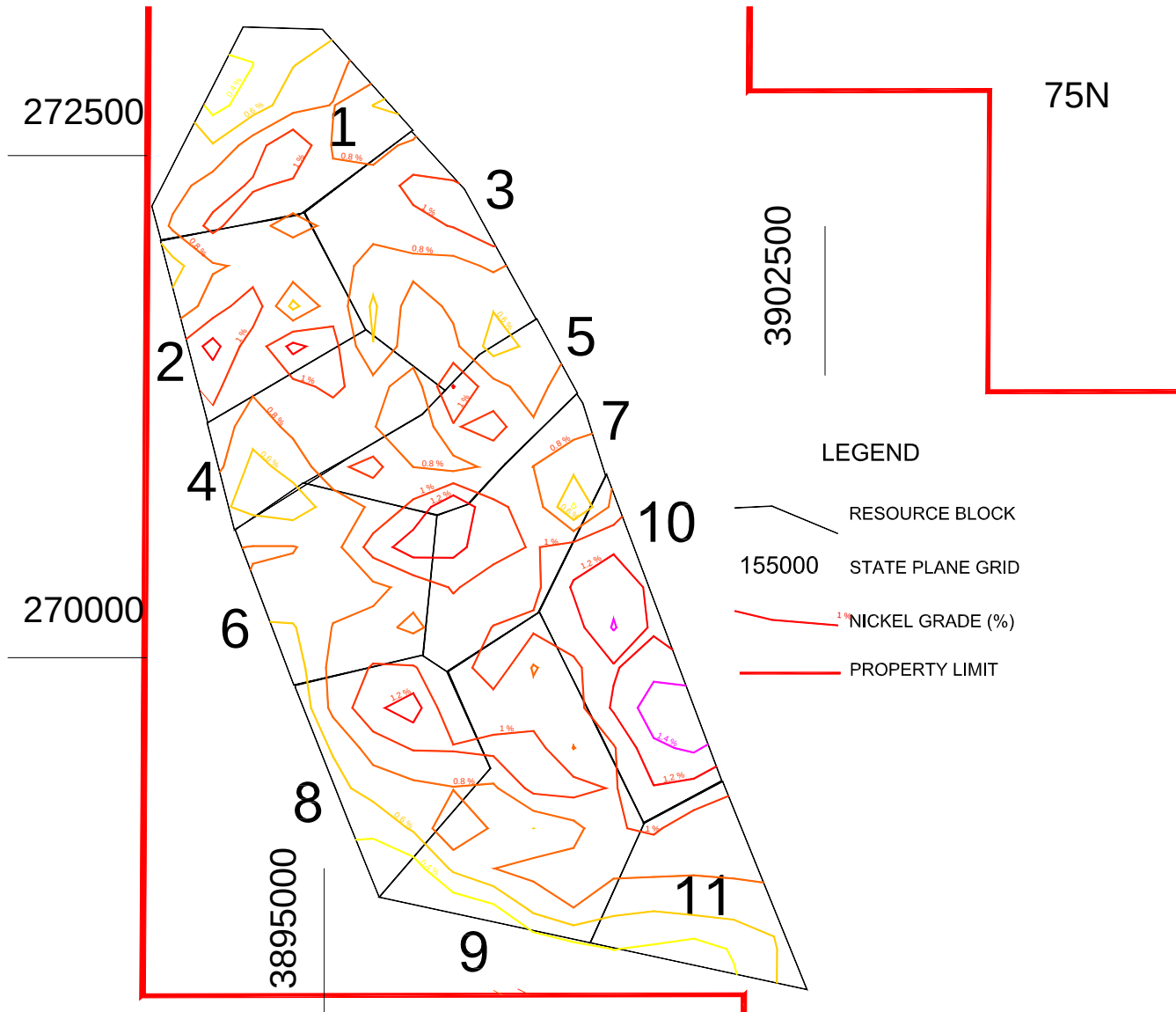
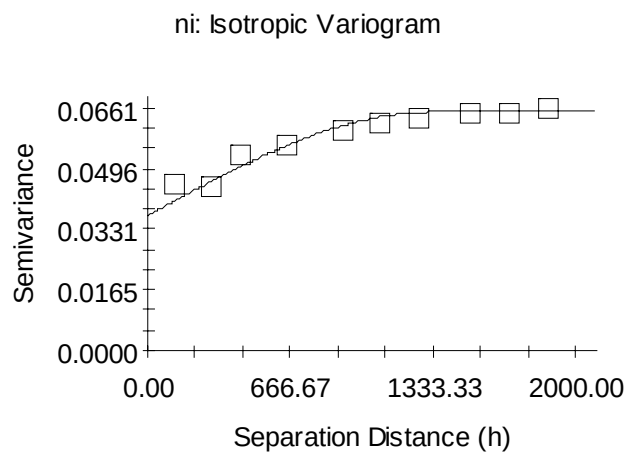


Figure 18. 5 - Measured resource block with nickel grade



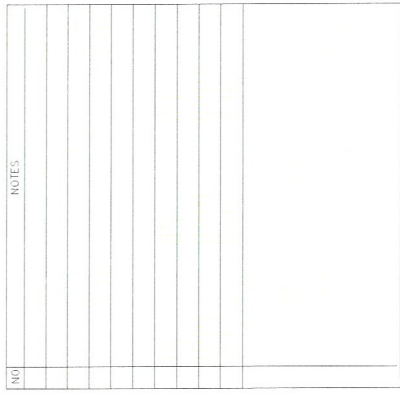
Spherical model ($C_0 = 0.03680$; $C_0 + C = 0.06510$; $A_0 = 1325.17$; $r^2 = 0.954$;
RSS = 4.154E-05)

Figure 18. 6 - Variogram of Ni for the soil fraction

APPENDIX A

MAPS

The map displays the coastal region of Oregon and California. The Pacific Ocean is on the right. Key locations marked include Crescent City, Gold Beach, Grants Pass, Medford, and Yreka. The Red Flat Project is highlighted in a red area near Gold Beach. The map includes a scale bar from 0 to 40 miles and a latitude/longitude grid.



The figure consists of two parts: a geological map and a cross-section labeled 'SECTION A'.

Geological Map:

- Legend:** A color-coded legend at the top identifies various geological units: dark blue, green, red, purple, light blue, white, black, and a red box labeled 'A'.
- Map Features:** The map shows the Pacific Ocean to the west, Gold Beach to the south, and a north arrow. A scale bar at the bottom indicates distances from 0 to 10 km. A line labeled 'A' indicates the location of the cross-section.
- Geological Units:** The map displays various geological units in different colors, including dark blue, green, red, purple, light blue, white, and black.

Cross-section (SECTION A):

- Scale:** A vertical scale on the left indicates elevation from -500 m to 2000 m.
- Topography:** The cross-section shows the topographic profile of the area, with a peak of approximately 2000 m.
- Geological Structure:** The cross-section reveals the subsurface geological structure, showing the Red Flat Deposit (indicated by a red box) and other geological units.
- Labels:** The cross-section is labeled 'SECTION A' and includes a reference to the 'Red Flat Deposit (see detailed cross-section)'.

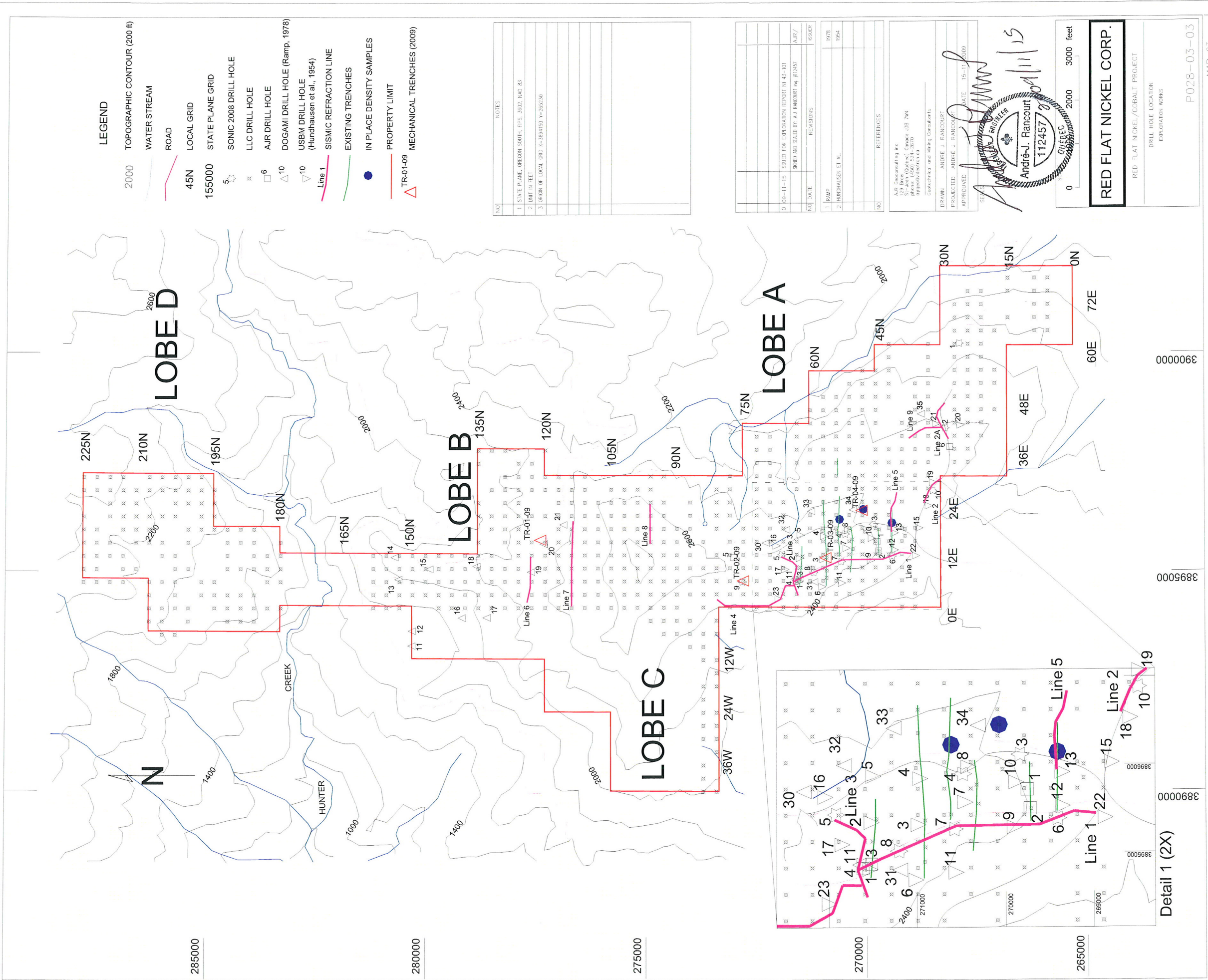
- [illegible]

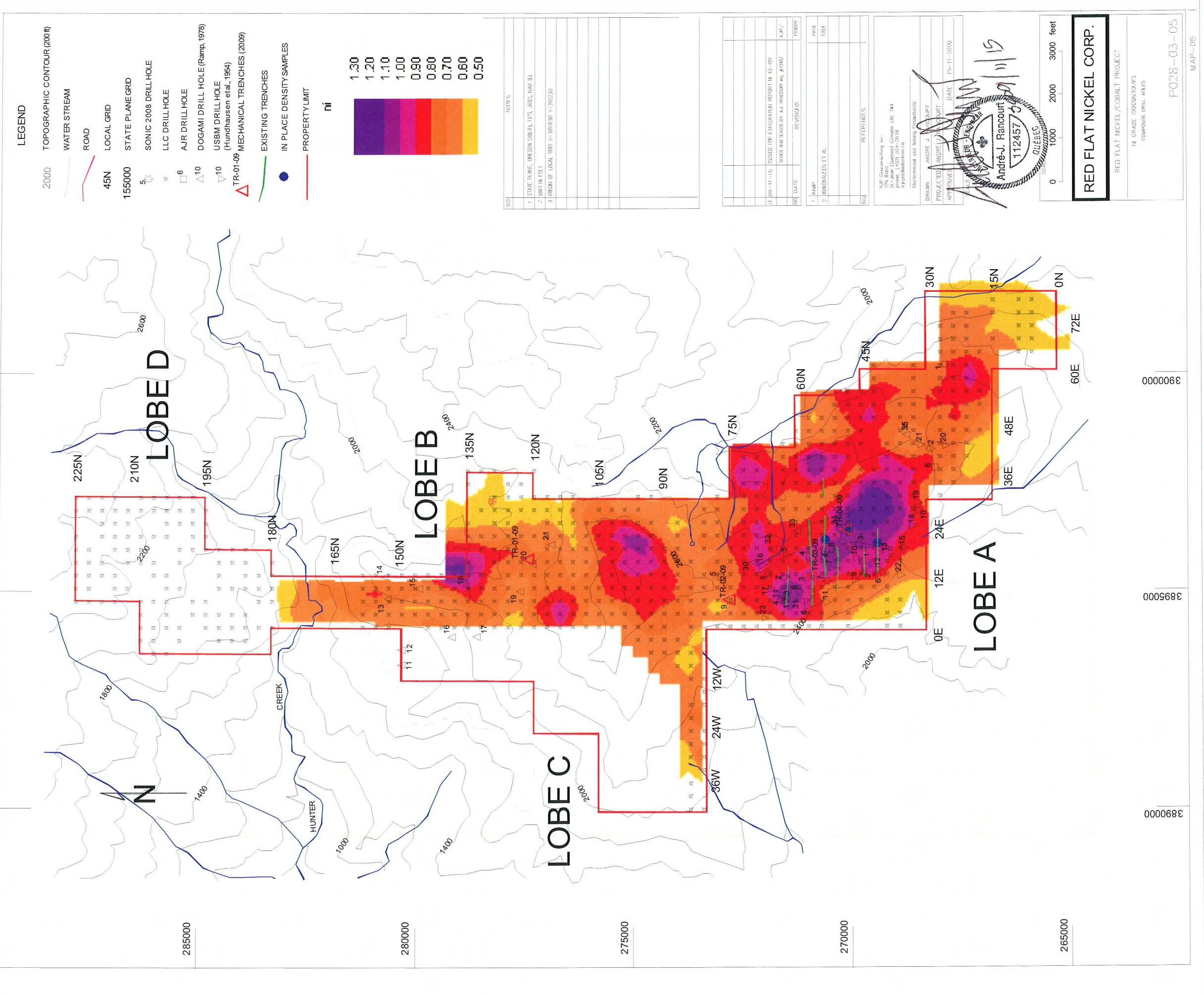
Geotechnical and Mining Consultants	
DRAWN	ANDRÉ J. RANQUART
PROJECTED	ANDRÉ J. RANQUART
APPROVED	<i>[Signature]</i>

RED FLAT NICKEL CORP.

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REGIONAL GEOLOGY

P028-03-02





APPENDIX B

TRENCH LOGS, BOREHOLE LOGS AND ADDITIONNAL PHOTOGRAPHS

Red Flat Drilling Matrix									
Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
225N	6E	287800	3894795	6.0	0.333	0.063	0.692	19.600	12.500
				12.0	0.255	0.017	0.277	10.200	18.000
				14.0	0.254	0.012	0.186	7.120	18.850
	9E		3895095	6.0	0.076	0.010	0.066	13.750	2.380
				8.0	0.086	0.010	0.090	14.250	2.360
	12E		3895395	3.0	0.152	0.010	0.203	8.780	12.150
	15E		3895695	4.0	0.439	0.022	0.402	10.850	16.500
	18E		3895995	5.0	0.392	0.021	0.371	10.400	16.050
	21E		3896295	6.0	0.047	0.008	0.060	14.950	2.830
				9.0	0.060	0.008	0.062	14.150	3.370
	24E		3896595						
	27E		3896895	3.0	0.324	0.018	0.406	12.250	17.500
	30E		3897195	6.0	0.014	0.006	0.019	11.900	1.250
222N	6E	287500	3894795	6.0	0.021	0.006	0.038	12.550	3.020
				8.0	0.019	0.006	0.029	11.600	2.880
	9E		3895095	4.0	0.199	0.016	0.767	12.950	4.630
	12E		3895395	3.0	0.184	0.012	0.297	10.600	7.690
	15E		3895695	3.0	0.431	0.025	0.633	10.550	16.200
	18E		3895995	6.0	0.021	0.006	0.025	11.600	2.650
	21E		3896295						
	24E		3896595						
	27E		3896895	5.0	0.359	0.027	0.529	13.750	16.400
	30E		3897195	4.0	0.347	0.025	0.471	13.250	17.050
219N	6E	287200	3894795	3.0	0.032	0.007	0.032	11.300	3.510
	9E		3895095						
	12E		3895395	3.0	0.052	0.009	0.059	13.750	3.980
	15E		3895695	4.0	0.553	0.034	0.829	17.750	8.300
	18E		3895995						
	21E		3896295	6.0	0.087	0.012	0.367	10.150	3.100
				10.5	0.099	0.009	0.245	8.230	3.980

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	24E		3896595	3.0	0.396	0.027	0.652	13.500	14.750
	27E		3896895	5.0	0.337	0.048	1.280	31.100	4.130
	30E		3897195	3.0	0.262	0.017	0.247	8.850	14.400
216N	6E	286900	3894795	4.0	0.016	0.004	0.018	13.650	2.580
	9E		3895095	5.0	0.021	0.005	0.022	13.950	2.790
	12E		3895395	3.0	0.004	0.002	0.009	10.100	2.420
	15E		3895695						
	18E		3895995	3.0	0.426	0.022	0.508	11.850	14.950
	21E		3896295	3.0	0.326	0.047	1.395	25.000	6.220
	24E		3896595	3.0	0.304	0.017	0.605	12.600	10.850
	27E		3896895	4.0	0.279	0.037	0.777	19.900	11.750
	30E		3897195	3.0	0.068	0.006	0.053	9.760	2.350
213N	6E	286600	3894795						
	9E		3895095	6.0	0.016	0.006	0.019	14.250	2.140
				11.0	0.017	0.005	0.024	13.750	2.110
	12E		3895395						
	15E		3895695	6.0	0.030	0.002	0.058	6.220	2.320
				7.0	0.036	0.003	0.089	7.310	2.580
	18E		3895995	3.0	0.030	0.001	0.031	7.720	3.890
	21E		3896295	4.0	0.048	0.004	0.132	10.600	3.670
	24E		3896595	5.5	0.475	0.027	0.502	14.300	11.400
	27E		3896895	3.0	0.078	0.005	0.144	8.380	9.170
	30E		3897195						
210N	6W	286300	3893595						
	3W		3893895	4.0	0.210	0.011	0.271	6.960	16.200
	0E		3894195	6.0	0.059	0.006	0.124	7.460	5.440
	3E		3894495	6.0	0.031	0.007	0.066	14.200	2.620
				7.0	0.059	0.006	0.109	10.500	7.440
	6E		3894795	6.0	0.042	0.009	0.059	13.850	1.870

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				10.0	0.037	0.008	0.053	14.300	2.240
	9E		3895095						
	12E		3895395						
	15E		3895695	6.0	0.404	0.041	2.040	25.500	3.900
	18E		3895995	5.0	0.082	0.009	0.251	8.580	3.780
	21E		3896295	3.0	0.449	0.029	0.858	13.600	13.150
	24E		3896595						
	27E		3896895	4.0	0.397	0.020	0.428	11.650	13.200
	30E		3897195	3.0	0.277	0.021	0.550	14.250	6.160
207N	6W	286000	3893595	6.0	0.045	0.003	0.045	6.620	2.740
				7.0	0.037	0.003	0.054	7.230	2.630
	3W		3893895	6.0	0.060	0.005	0.152	7.470	3.280
	0E		3894195	6.0	0.037	0.004	0.124	6.970	2.590
				8.0	0.038	0.004	0.112	7.090	2.490
	3E		3894495						
	6E		3894795	6.0	0.025	0.007	0.048	10.500	2.570
				7.0	0.044	0.007	0.031	13.600	1.760
	9E		3895095						
	12E		3895395	6.0	0.116	0.012	0.482	13.250	3.070
	15E		3895695	3.0	0.177	0.013	0.685	13.050	4.050
	18E		3895995						
	21E		3896295	6.0	0.317	0.018	0.496	11.850	12.050
	24E		3896595						
	27E		3896895	3.0	0.396	0.042	0.733	23.300	7.120
	30E		3897195	3.0	0.115	0.013	0.316	13.700	4.990
204N	6W	285700	3893595	3.0	0.032	0.002	0.065	6.010	3.010
	3W		3893895						
	0E		3894195	3.0	0.163	0.017	0.624	14.850	3.970
	3E		3894495	3.0	0.379	0.029	0.727	15.100	12.700
	6E		3894795	5.0	0.304	0.041	0.804	19.900	6.660
	9E		3895095	5.0	0.034	0.005	0.035	11.350	1.940

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	12E		3895395	3.0	0.221	0.012	0.218	7.870	15.250
	15E		3895695						
	18E		3895995						
	21E		3896295	4.0	0.122	0.011	0.368	13.450	2.830
	24E		3896595	4.0	0.523	0.038	1.260	18.800	9.930
	27E		3896895	3.0	0.602	0.037	0.780	15.850	13.650
	30E		3897195	4.0	0.086	0.005	0.544	16.300	0.820
201N	6W	285400	3893595						
	3W		3893895	4.0	0.237	0.017	0.419	11.700	6.390
	0E		3894195	4.0	0.397	0.046	1.150	25.600	5.520
	3E		3894495						
	6E		3894795						
	9E		3895095	3.0	0.564	0.020	0.445	10.950	14.600
	12E		3895395						
	15E		3895695	4.0	0.206	0.011	0.350	9.180	12.000
	18E		3895995	5.0	0.432	0.039	0.889	19.200	7.610
	21E		3896295						
	24E		3896595	3.0	0.322	0.028	0.967	18.300	6.030
	27E		3896895	3.0	0.574	0.038	0.504	15.250	11.050
	30E		3897195	6.0	0.724	0.044	1.540	21.000	10.200
				7.0	0.708	0.046	1.800	22.100	9.470
198N	6W	285100	3893595						
	3W		3893895						
	0E		3894195						
	3E		3894495	5.0	0.430	0.039	0.812	19.500	9.260
	6E		3894795	6.0	0.197	0.041	1.095	29.200	2.760
				7.0	0.289	0.065	0.980	27.900	4.110
	9E		3895095						
	12E		3895395						
	15E		3895695						
	18E		3895995	3.0	0.076	0.006	0.081	10.750	9.700

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	21E		3896295	4.0	0.282	0.015	0.272	11.700	9.860
	24E		3896595	4.0	0.314	0.018	0.316	10.500	13.900
	27E		3896895	3.0	0.341	0.017	0.405	10.000	15.100
	30E		3897195	4.0	0.473	0.024	0.768	11.800	20.400
195N	6W	284800	3893595						
	3W		3893895						
	0E		3894195	6.0	0.048	0.004	0.070	5.590	2.070
	3E		3894495	5.5	0.121	0.012	0.724	13.550	3.320
	6E		3894795	4.0	0.114	0.013	0.332	15.150	3.060
	9E		3895095						
	12E		3895395						
	15E		3895695						
	18E		3895995	6.0	0.030	0.008	0.033	16.000	1.420
				9.0	0.037	0.009	0.031	16.050	1.820
	21E		3896295	4.0	0.121	0.009	0.238	8.140	7.530
	24E		3896595	4.0	0.422	0.026	0.587	12.250	15.500
	27E		3896895	4.0	0.251	0.016	0.319	9.720	13.600
	30E		3897195						
192N	6W	284500	3893595						
	3W		3893895	5.0	0.244	0.014	0.262	8.500	17.650
	0E		3894195	6.0	0.083	0.010	0.245	15.000	3.320
	3E		3894495	4.0	0.513	0.044	1.230	20.500	10.100
	6E		3894795						
	9E		3895095	6.0	0.287	0.049	1.415	37.000	3.440
				9.0	0.475	0.064	0.834	24.200	9.790
	12E		3895395	4.0	0.379	0.029	0.588	15.950	10.950
	15E		3895695	3.0	0.410	0.026	0.852	13.100	16.550
	18E		3895995	5.0	0.201	0.010	0.170	7.360	19.300
189N	6W	284200	3893595						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	3W		3893895	6.0	0.372	0.023	0.424	12.950	14.700
	0E		3894195	5.0	0.285	0.031	0.904	17.250	6.310
	3E		3894495	3.0	0.143	0.008	0.150	8.190	7.160
	6E		3894795						
	9E		3895095	3.0	0.492	0.052	0.978	25.800	4.720
	12E		3895395						
	15E		3895695	4.5	0.050	0.004	0.145	9.530	1.210
	18E		3895995	4.0	0.388	0.027	0.626	14.550	12.500
186N	6W	283900	3893595						
	3W		3893895	3.0	0.051	0.003	0.196	6.240	1.410
	0E		3894195	4.0	0.340	0.029	0.830	17.850	8.260
	3E		3894495	5.0	0.269	0.014	0.289	9.340	12.350
	6E		3894795						
	9E		3895095	3.0	0.461	0.030	0.632	14.700	11.150
	12E		3895395	3.0	0.382	0.022	0.602	10.800	17.100
	15E		3895695	5.0	0.568	0.028	0.550	13.550	14.100
	18E		3895995	3.5	0.396	0.021	0.405	10.300	17.500
183N	6W	283600	3893595						
	3W		3893895						
	0E		3894195	3.0	0.548	0.034	0.593	16.000	11.500
	3E		3894495						
	6E		3894795	3.0	0.361	0.022	0.539	10.500	13.800
	9E		3895095	4.0	0.041	0.002	0.282	8.750	1.200
	12E		3895395	3.0	0.461	0.033	1.340	15.500	11.750
	15E		3895695						
	18E		3895995						
180N	6W	283300	3893595						
	3W		3893895						
	0E		3894195	4.5	0.597	0.031	0.729	15.050	12.950

[illegible]

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
165N	0E	281800	3894195						
	3E		3894495						
	6E		3894795						
	9E		3895095						
	12E		3895395						
162N	0E	281500	3894195						
	3E		3894495						
	6E		3894795						
	9E		3895095						
	12E		3895395						
159N	0E	281200	3894195	6.0	0.777	0.089	0.976	28.700	8.030
				11.0	0.686	0.037	0.391	14.400	14.250
	3E		3894495	6.0	0.451	0.028	0.441	14.000	14.400
				12.5	0.352	0.026	0.433	13.600	14.050
	6E		3894795	6.0	0.671	0.044	0.886	21.500	10.750
	9E		3895095	3.0	0.702	0.046	0.706	24.200	9.030
	12E		3895395	6.0	0.725	0.039	0.767	19.500	11.650
				7.0	0.569	0.023	0.429	11.850	15.550
156N	0E	280900	3894195	6.0	0.496	0.022	0.395	12.750	15.300
				10.0	0.430	0.019	0.280	10.050	17.100
	3E		3894495	6.0	0.710	0.057	1.420	35.800	4.010
				12.0	1.365	0.030	0.580	16.100	14.300
				15.0	1.005	0.034	0.800	21.700	10.950
	6E		3894795	6.0	0.997	0.071	1.260	34.500	4.060
				8.0	0.927	0.045	0.814	23.800	8.510
	9E		3895095	6.0	0.737	0.058	1.580	26.200	8.680
				10.0	0.293	0.015	0.256	8.000	18.950
	12E		3895395	6.0	0.933	0.077	1.720	31.700	5.900
				10.0	0.661	0.039	0.824	18.800	12.500
153N	0E	280600	3894195	6.0	0.564	0.035	0.708	16.550	12.450

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				9.0	0.450	0.017	0.268	9.530	18.100
	3E		3894495	6.0	0.521	0.041	1.440	30.900	3.720
				12.0	1.195	0.085	1.550	34.600	2.860
				15.0	1.060	0.054	1.020	25.900	7.780
	6E		3894795	6.0	0.864	0.052	1.270	25.000	6.940
				10.5	0.676	0.039	1.050	18.450	10.250
	9E		3895095	6.0	0.844	0.053	1.080	24.300	8.180
				9.5	0.668	0.040	0.687	17.750	12.450
	12E		3895395	6.0	0.506	0.026	0.455	12.250	16.350
				11.0	0.547	0.028	0.489	13.450	14.700
150N	12W	280300	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195						
	3E		3894495	6.0	0.587	0.037	1.870	27.100	6.590
				12.0	0.451	0.022	0.471	13.250	14.650
	6E		3894795	6.0	1.220	0.059	1.280	30.000	8.070
	9E		3895095	6.0	0.716	0.064	1.420	31.100	5.450
				12.0	0.607	0.034	0.633	17.400	13.550
				15.0	0.572	0.033	0.594	16.700	13.800
	12E		3895395	5.0	0.653	0.030	0.418	15.500	14.350
147N	12W	280000	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195						
	3E		3894495	6.0	0.613	0.031	0.591	16.450	13.050
				7.0	0.649	0.035	0.669	17.150	11.800
	6E		3894795	6.0	0.652	0.063	1.360	32.600	4.900
				9.0	0.702	0.040	0.689	20.000	11.150

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	9E		3895095	6.0	0.781	0.035	0.712	25.400	7.190
				12.0	0.813	0.047	0.483	16.250	14.500
				15.0	0.824	0.056	0.595	17.050	14.350
	12E		3895395	6.0	0.575	0.034	0.803	17.200	12.900
				9.0	0.764	0.032	0.548	15.100	13.600
144N	12W	279700	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.437	0.043	0.699	19.100	8.550
				8.0	0.540	0.047	0.799	19.450	8.860
	3E		3894495	6.0	0.408	0.025	0.410	13.200	15.100
				9.0	0.361	0.022	0.321	11.050	16.250
	6E		3894795	6.0	1.000	0.075	1.460	30.800	6.180
				10.0	1.115	0.050	0.695	20.700	11.350
	9E		3895095	6.0	0.673	0.040	0.908	26.300	5.620
				8.0	0.691	0.034	0.694	20.100	8.370
	12E		3895395	6.0	1.120	0.048	1.050	22.500	11.400
				11.0	1.060	0.038	0.805	18.500	12.100
141N	12W	279400	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.991	0.081	1.940	39.300	2.420
				8.0	0.909	0.037	0.573	16.350	13.700
	3E		3894495	6.0	0.422	0.027	0.411	13.550	14.100
				11.0	0.370	0.022	0.320	11.600	15.350
	6E		3894795	6.0	0.991	0.054	0.763	20.700	11.350
				9.0	0.791	0.043	0.662	18.150	11.500
	9E		3895095	6.0	0.259	0.026	0.556	19.700	4.500
	12E		3895395	6.0	1.075	0.079	1.530	33.500	7.110
				8.0	1.000	0.071	1.340	29.700	8.690

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
138N	12W	279100	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.807	0.072	2.570	31.200	4.380
				11.0	1.160	0.049	1.115	24.400	8.730
	3E		3894495	6.0	0.368	0.021	0.342	11.500	14.700
				12.0	0.454	0.017	0.293	10.300	14.850
	6E		3894795	6.0	0.508	0.041	0.828	28.400	5.250
				12.0	0.675	0.069	0.572	20.100	9.540
	9E		3895095	6.0	0.853	0.063	1.330	27.900	7.720
				7.0	1.060	0.038	0.558	17.250	14.250
	12E		3895395	6.0	0.566	0.066	1.050	33.800	3.820
				10.0	0.577	0.059	0.636	20.500	9.500
135N	12W	278800	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.704	0.046	1.320	23.400	7.070
				9.0	0.787	0.036	0.686	17.350	11.600
	3E		3894495	6.0	0.441	0.025	0.441	13.700	14.450
				10.0	0.419	0.021	0.420	11.750	16.050
	6E		3894795	6.0	0.526	0.040	0.989	19.200	11.050
				10.0	0.422	0.019	0.370	10.700	16.550
	9E		3895095	6.0	1.120	0.053	0.534	23.200	8.750
				10.0	1.540	0.076	0.808	29.100	6.220
	12E		3895395	6.0	1.260	0.058	1.730		
				11.0	1.690	0.050	0.640		
	15E		3895695	6.0	1.010	0.040	0.580		
				10.0	1.060	0.040	0.490		
	18E		3895995						
	21E		3896295	6.0	0.290	0.010	0.150		

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	24E		3896595	6.0	0.490	0.030	0.690		
				7.0	0.460	0.020	0.240		
	27E		3896895						
	30E		3897195						
	33E		3897495	3.0	0.530	0.020	0.610		
	36E		3897795	4.0	0.500	0.040	1.460		
132N	12W	278500	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.594	0.032	0.863	16.000	11.150
				12.0	0.601	0.022	0.432	12.000	13.750
				15.0	0.568	0.022	0.392	11.500	14.000
	3E		3894495	6.0	0.441	0.024	0.457	13.900	13.200
	6E		3894795	6.0	0.932	0.041	0.941	20.700	10.800
				8.0	0.700	0.016	0.279	10.050	16.750
	9E		3895095	6.0	1.085	0.126	1.565	36.300	4.510
				9.0	1.465	0.035	0.655	14.050	14.600
	12E		3895395	6.0	1.490	0.072	1.060	24.800	10.050
				7.0	1.405	0.056	0.780	19.750	12.550
	15E		3895695						
	18E		3895995	6.0	0.610	0.040	0.880		
	21E		3896295	5.0	0.650	0.040	1.460		
	24E		3896595						
	27E		3896895	5.0	0.430	0.020	0.760		
	30E		3897195						
	33E		3897495						
	36E		3897795	4.0	0.310	0.010	0.850		
129N	12W	278200	3892995						
	9W		3893295						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.910	0.053	1.595	25.500	6.300
				8.0	0.926	0.032	0.668	17.150	10.600
	3E		3894495	6.0	0.864	0.055	1.205	26.500	7.900
	6E		3894795	6.0	0.780	0.105	1.090	32.200	5.600
				12.0	0.876	0.050	0.628	21.200	8.660
	9E		3895095	6.0	0.884	0.132	1.400	37.100	3.980
				9.0	0.867	0.124	0.811	25.900	8.350
	12E		3895395						
	15E		3895695	6.0	0.931	0.042	0.891	21.500	6.080
				12.0	1.400	0.035	0.579	20.000	8.910
	18E		3895995	6.0	0.588	0.028	0.536	13.200	13.850
				8.0	0.564	0.029	0.638	13.800	12.800
	21E		3896295	6.0	0.667	0.043	1.660	18.500	11.200
	24E		3896595	6.0	0.331	0.013	0.287	6.920	19.300
	27E		3896895	6.0	0.658	0.040	1.210	20.200	11.700
				7.0	0.574	0.032	0.999	16.250	13.800
	30E		3897195	4.0	0.312	0.014	0.273	7.170	19.800
	33E		3897495						
	36E		3897795	3.0	0.379	0.025	0.685	12.950	14.300
126N	12W	277900	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.602	0.041	0.909	22.200	9.150
				8.0	0.538	0.033	0.626	18.150	11.600
	3E		3894495	6.0	1.350	0.034	0.798	17.450	13.600
				9.0	0.690	0.033	0.761	16.250	13.300
	6E		3894795	6.0	0.537	0.056	1.010	28.100	5.250
				12.0	0.704	0.061	0.694	23.800	6.530

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				15.0	0.828	0.063	0.627	22.400	7.180
	9E		3895095	6.0	0.557	0.093	1.010	36.200	3.050
				9.0	0.850	0.164	1.010	32.600	4.820
	12E		3895395	6.0	0.498	0.060	0.982	31.000	4.530
				12.0	0.745	0.043	0.641	23.100	7.650
				15.0	0.726	0.042	0.628	21.500	8.190
	15E		3895695	6.0	0.824	0.075	1.430	29.100	4.020
				11.0	1.115	0.059	0.902	25.200	6.330
	18E		3895995	3.0	0.710	0.045	1.610	22.000	11.200
	21E		3896295	5.0	0.463	0.024	0.483	11.250	17.100
	24E		3896595	6.0	0.724	0.038	0.944	19.850	11.350
				7.5	0.626	0.032	0.692	16.250	13.700
	27E		3896895	4.0	0.838	0.051	1.080	23.600	10.200
	30E		3897195	4.0	0.424	0.027	0.579	11.800	17.100
	33E		3897495	6.0	0.615	0.032	0.988	16.150	14.800
				12.0	0.376	0.017	0.378	8.610	19.100
				13.0	0.324	0.015	0.290	7.390	19.450
	36E		3897795						
123N	12W	277600	3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.312	0.014	0.397	6.710	19.400
				11.0	0.553	0.024	0.343	12.000	15.750
	3E		3894495	6.0	0.403	0.017	0.223	9.420	17.250
				7.5	1.055	0.051	1.180	29.500	7.160
	6E		3894795	6.0	1.080	0.037	0.795	20.400	12.000
				10.0	0.772	0.049	1.730	38.300	1.460
	9E		3895095						
	12E		3895395	6.0	0.659	0.049	1.250	33.200	3.890
				9.0	0.615	0.080	0.766	29.600	3.770

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	15E		3895695	6.0	1.220	0.086	0.928	22.400	9.670
				9.0	0.662	0.047	1.090	23.100	10.600
	18E		3895995						
	21E		3896295	6.0	0.356	0.017	0.241	10.050	17.150
				12.0	0.382	0.019	0.278	9.770	18.400
				15.0	0.302	0.015	0.247	7.610	19.350
	24E		3896595						
	27E		3896895	6.0	0.627	0.034	0.749	15.700	15.450
				9.5	0.481	0.030	0.628	13.500	16.450
	30E		3897195	6.0	0.957	0.050	1.200	24.700	9.500
				12.0	0.386	0.018	0.331	8.700	18.650
	33E		3897495	6.0	0.510	0.028	0.838	13.500	15.700
	36E		3897795						
120N	24W	277300	3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	5.0	0.282	0.017	0.353	9.900	16.300
	3E		3894495	6.0	0.515	0.026	0.509	13.900	14.050
				12.0	0.466	0.024	0.405	12.250	15.750
				15.0	0.492	0.022	0.389	11.800	16.750
	6E		3894795	6.0	0.381	0.016	0.229	9.090	16.750
	9E		3895095	5.0	0.441	0.024	0.584	16.300	8.730
	12E		3895395	6.0	0.539	0.051	1.020	28.800	4.500
				12.0	0.806	0.042	0.656	22.100	6.800
				15.0	0.780	0.039	0.632	20.700	7.540
	15E		3895695	6.0	1.025	0.148	2.150	43.700	1.330

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				12.0	1.030	0.086	1.270	30.300	6.230
				15.0	0.990	0.050	0.761	21.000	10.200
	18E		3895995						
	21E		3896295	6.0	0.821	0.054	1.030	23.100	9.520
				12.0	0.680	0.052	0.968	23.000	9.920
	24E		3896595						
	27E		3896895	6.0	0.704	0.043	0.751	20.500	11.450
				11.0	0.448	0.026	0.430	12.600	15.200
	30E		3897195	6.0	0.588	0.039	0.753	17.950	13.150
				10.0	1.070	0.067	1.485	27.900	7.760
	33E		3897495						
	36E		3897795	4.0	0.911	0.054	1.070	22.700	10.400
117N	24W	277000	3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.620	0.075	0.925	28.600	5.590
				12.0	0.869	0.082	0.702	23.900	7.600
				13.5	0.903	0.083	0.707	24.200	7.330
	3E		3894495	6.0	1.090	0.067	1.370	30.400	6.340
				8.0	1.125	0.035	0.428	18.350	11.000
	6E		3894795	6.0	0.687	0.046	0.959	29.500	5.110
				11.0	0.975	0.037	0.569	20.700	8.920
	9E		3895095	5.0	0.749	0.036	0.745	21.900	8.530
	12E		3895395	6.0	0.598	0.060	0.830	29.600	3.440
				12.5	0.958	0.045	0.712	24.600	6.070
	15E		3895695	6.0	0.610	0.026	0.397	13.600	13.850

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	18E		3895995	6.0	0.467	0.019	0.378	8.530	17.800
				9.0	0.465	0.016	0.238	9.000	16.900
	21E		3896295	6.0	0.526	0.017	0.277	9.110	17.000
				12.0	0.626	0.029	0.718	14.850	14.150
	24E		3896595	6.0	0.465	0.032	0.766	15.000	14.600
				8.0	0.309	0.013	0.315	7.970	19.200
	27E		3896895	6.0	0.414	0.027	0.573	13.900	15.900
	30E		3897195	5.0	0.262	0.013	0.234	6.900	20.400
114N	24W	276700	3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.696	0.043	1.240	25.700	7.300
				12.0	0.806	0.036	0.682	18.800	11.950
	3E		3894495	6.0	0.734	0.035	0.616	19.100	10.650
				11.0	0.991	0.030	0.488	17.000	11.200
	6E		3894795	6.0	0.416	0.054	1.395	25.400	5.270
				12.0	1.180	0.046	0.627	20.400	9.950
	9E		3895095	6.0	0.252	0.033	0.490	21.500	1.300
				11.0	0.897	0.078	0.699	22.500	8.240
	12E		3895395	6.0	0.781	0.036	0.709	18.250	12.350
				8.5	0.719	0.028	0.549	14.750	13.600
	15E		3895695	6.0	0.780	0.040	0.840		
				12.0	0.650	0.030	0.490		
				17.0	0.460	0.020	0.220		
	18E		3895995	6.0	0.890	0.040	0.630		
				8.0	0.730	0.040	0.990		

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	21E		3896295	6.0	0.964	0.047	2.140	24.200	7.330
				8.0	0.679	0.031	0.907	15.700	12.600
	24E		3896595	6.0	0.570	0.030	0.610		
				10.0	0.680	0.030	0.840		
	27E		3896895	6.0	0.670	0.040	0.910		
				12.0	0.400	0.020	0.400		
	30E		3897195	6.0	0.660	0.040	0.890		
				8.0	0.390	0.020	0.280		
111N	24W	276400	3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	1.275	0.074	1.460	34.100	5.590
				12.0	1.315	0.038	0.718	20.100	11.800
				15.0	1.150	0.040	0.732	20.300	12.050
	3E		3894495	6.0	1.185	0.094	2.080	41.300	2.650
				12.0	1.205	0.096	2.080	41.500	2.660
				15.0	1.630	0.068	1.225	31.400	6.720
				18.0	1.570	0.066	1.160	30.200	6.920
				24.0	1.660	0.055	1.070	25.800	8.980
	6E		3894795	6.0	0.894	0.027	0.418	17.350	9.980
				12.0	0.868	0.023	0.371	13.150	14.700
				15.0	0.829	0.024	0.378	13.600	14.450
				18.0	0.684	0.024	0.399	13.550	14.600
				23.5	0.621	0.024	0.410	13.800	14.150
	9E		3895095	6.0	0.877	0.038	0.865	21.200	8.800
				12.0	0.658	0.019	0.332	10.950	17.600
				14.0	0.687	0.026	0.489	14.800	14.550

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	12E		3895395	6.0	0.683	0.018	0.271	10.800	16.300
				9.0	0.889	0.026	0.462	14.150	15.600
	15E		3895695	6.0	0.736	0.030	0.696	23.500	6.660
				9.0	0.977	0.038	0.842	22.600	9.170
	18E		3895995	6.0	0.978	0.044	0.862	22.100	10.500
				12.0	0.404	0.016	0.237	8.710	18.450
	21E		3896295	6.0	0.508	0.015	0.260	9.130	17.350
				9.0	0.522	0.018	0.341	9.940	17.250
	24E		3896595	6.0	0.451	0.024	0.537	12.650	15.800
				9.0	0.329	0.015	0.298	8.590	18.350
	27E		3896895	6.0	0.320	0.013	0.460	6.970	19.800
	30E		3897195	6.0	0.449	0.023	0.518	12.900	15.700
108N	24W	276100	3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.635	0.041	0.720	19.250	8.600
				7.0	0.710	0.055	1.420	29.300	3.490
	3E		3894495	6.0	0.877	0.055	1.270	27.200	6.730
				11.0	1.035	0.041	0.773	20.800	10.650
	6E		3894795	6.0	0.884	0.056	1.390	27.400	6.520
				12.0	0.661	0.030	0.520	14.900	14.450
				17.0	0.720	0.048	1.110	24.200	10.300
	9E		3895095	6.0	0.592	0.032	0.603	15.700	14.150
				10.0	0.489	0.020	0.350	10.650	16.700
	12E		3895395	6.0	0.583	0.033	0.745	18.100	11.400
				12.0	0.620	0.027	0.415	14.850	13.950

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				15.0	0.644	0.037	0.853	20.800	9.570
				18.0	0.499	0.028	0.546	15.500	12.900
	15E		3895695	6.0	0.593	0.026	0.427	13.400	13.800
				12.0	0.616	0.033	0.841	16.100	13.850
	18E		3895995	6.0	0.359	0.016	0.325	7.670	19.000
				9.0	0.319	0.015	0.284	7.370	19.650
	21E		3896295	6.0	0.546	0.050	1.345	24.000	6.200
				12.0	0.309	0.015	0.215	7.510	19.100
				15.0	0.303	0.014	0.238	7.560	19.500
				18.0	0.295	0.014	0.222	7.340	20.400
	24E		3896595	6.0	0.759	0.044	1.005	22.100	10.700
	27E		3896895						
	30E		3897195						
105N	42W	275800	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.382	0.022	0.554	13.600	12.800
				9.0	0.444	0.020	0.517	13.000	14.100
	3E		3894495	6.0	0.679	0.027	0.574	17.400	11.500
				12.0	0.459	0.016	0.232	9.090	18.400

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	6E		3894795	6.0	0.691	0.075	0.764	24.000	6.980
				7.0	0.706	0.088	0.825	27.300	6.220
	9E		3895095	6.0	0.742	0.046	1.440	23.800	7.520
				11.5	0.859	0.070	0.921	27.100	5.650
	12E		3895395	6.0	0.517	0.027	0.537	14.350	14.400
				8.0	0.493	0.026	0.542	13.950	14.650
	15E		3895695	6.0	0.492	0.024	0.515	13.500	14.850
	18E		3895995	6.0	0.745	0.051	1.280	26.700	8.060
				8.0	0.516	0.029	0.604	15.200	14.550
	21E		3896295	6.0	0.740	0.096	1.700	40.500	2.420
				12.0	0.995	0.117	1.060	30.500	6.430
				15.0	1.045	0.087	0.704	21.600	10.400
				18.0	1.110	0.037	0.559	16.900	13.150
				20.0	1.050	0.031	0.535	15.400	14.150
	24E		3896595	6.0	0.872	0.054	1.590	26.700	9.490
				8.0	0.896	0.055	1.480	24.900	9.860
	27E		3896895	6.0	0.723	0.048	1.440	20.600	8.700
	30E		3897195						
102N	42W	275500	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	3W		3893895						
	0E		3894195	6.0	0.627	0.025	0.478	16.350	12.250
				12.0	0.711	0.025	0.491	13.850	15.100
	3E		3894495	6.0	0.786	0.041	0.843	20.100	11.950
				12.0	0.537	0.025	0.430	12.850	15.350
	6E		3894795	6.0	0.693	0.028	0.535	18.900	8.520
				11.0	1.120	0.044	0.485	22.900	8.850
	9E		3895095	6.0	0.829	0.045	0.748	24.800	6.440
				9.0	0.708	0.024	0.330	13.800	12.850
	12E		3895395	6.0	1.050	0.079	1.045	32.100	4.580
				12.0	1.385	0.054	0.676	24.300	7.800
				14.0	1.400	0.031	0.359	15.300	13.250
	15E		3895695	6.0	0.801	0.033	0.618	17.450	13.600
				9.0	0.412	0.017	0.300	9.260	18.100
	18E		3895995	6.0	0.979	0.071	1.710	42.600	1.510
				12.0	1.300	0.162	1.735	40.200	3.030
	21E		3896295	6.0	1.135	0.056	1.220	28.000	7.450
				10.0	1.005	0.048	0.876	23.900	10.450
	24E		3896595	6.0	0.855	0.040	0.900	20.100	11.550
				12.0	0.728	0.037	0.843	17.850	12.900
				15.0	0.480	0.023	0.452	11.550	16.250
				18.0	0.305	0.014	0.231	7.100	18.300
				21.0	0.306	0.014	0.247	7.110	18.700
	27E		3896895	4.0	0.752	0.044	0.819	22.700	10.800
	30E		3897195						
99N	42W	275200	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895						
	0E		3894195	6.0	0.425	0.024	0.298	13.450	14.000
				7.0	0.417	0.023	0.280	12.150	14.900
	3E		3894495	6.0	0.567	0.033	0.729	19.850	11.550
	6E		3894795	6.0	1.015	0.063	0.798	23.700	8.640
	9E		3895095	6.0	0.676	0.051	0.813	26.600	5.450
				9.5	0.692	0.035	0.584	20.600	7.890
	12E		3895395	6.0	0.984	0.053	0.836	27.600	5.790
				9.0	0.876	0.033	0.568	18.450	10.200
	15E		3895695	6.0	0.643	0.031	0.491	16.800	12.100
				9.0	0.541	0.027	0.391	14.500	13.900
	18E		3895995	6.0	0.831	0.064	1.400	33.700	2.640
	21E		3896295	6.0	1.025	0.082	0.958	34.500	5.180
				8.0	0.997	0.059	0.658	22.600	9.110
	24E		3896595	5.0	0.473	0.025	0.540	12.500	16.450
	27E		3896895	6.0	0.752	0.039	1.175	20.100	13.050
	30E		3897195						
96N	42W	274900	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595						
	3W		3893895	6.0	0.294	0.020	1.530	29.200	1.310
				8.0	0.339	0.036	1.480	28.700	2.080
	0E		3894195	6.0	0.680	0.058	1.780	32.400	3.270
				8.0	1.060	0.072	1.550	33.800	4.850
	3E		3894495	6.0	0.821	0.041	0.716	23.300	7.200
				8.0	0.708	0.032	0.530	17.700	10.350
	6E		3894795	6.0	0.955	0.031	0.551	17.050	11.700
	9E		3895095	6.0	0.708	0.067	0.828	28.800	4.880
				12.0	0.809	0.079	0.644	22.700	6.600
				15.0	0.874	0.050	0.581	20.100	7.330
	12E		3895395	6.0	0.718	0.071	1.190	29.500	5.580
				12.0	1.475	0.071	0.587	23.000	6.850
				14.0	1.350	0.048	0.418	17.300	10.800
	15E		3895695	6.0	0.865	0.048	0.914	26.900	4.590
				8.5	0.735	0.034	0.539	18.500	10.150
	18E		3895995	6.0	1.275	0.186	2.290	44.800	1.640
				12.0	1.485	0.339	2.150	44.700	2.050
				15.0	1.440	0.282	1.960	39.300	4.210
	21E		3896295	6.0	1.070	0.045	0.960	21.500	8.940
				8.5	0.955	0.041	0.850	19.900	10.600
	24E		3896595	6.0	0.695	0.037	0.702	18.550	12.450
				7.0	0.717	0.039	0.836	19.300	11.500
	27E		3896895	5.0	0.450	0.024	0.448	12.300	16.850
	30E		3897195	6.0	0.400	0.021	0.333	10.000	17.450
93N	42W	274600	3889995						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595	6.0	0.832	0.069	1.385	33.800	4.940
				7.0	0.519	0.021	0.371	13.250	13.600
	3W		3893895	6.0	0.675	0.025	0.368	13.550	13.700
	0E		3894195	6.0	1.080	0.064	1.340	29.200	7.680
				10.0	0.836	0.047	0.921	22.100	11.650
	3E		3894495	6.0	0.957	0.036	1.490	40.100	1.910
				8.0	1.025	0.074	0.792	24.300	8.440
	6E		3894795	6.0	0.845	0.037	0.740	21.400	8.540
				7.0	0.861	0.029	0.463	16.150	11.950
	9E		3895095	6.0	0.628	0.048	0.912	29.600	4.310
				7.0	0.781	0.043	0.678	24.100	6.270
	12E		3895395	6.0	1.120	0.053	1.220	27.300	9.190
				8.0	0.956	0.037	0.781	18.100	13.050
	15E		3895695	6.0	0.817	0.084	1.430	33.700	3.710
				12.0	1.330	0.086	0.834	26.900	6.640
				15.0	1.355	0.049	0.586	19.100	11.600
	18E		3895995	6.0	1.275	0.060	0.970	27.200	7.040
				12.0	1.375	0.040	0.577	18.850	11.450
	21E		3896295	6.0	0.672	0.046	1.210	23.400	9.780
				12.0	0.484	0.024	0.288	11.900	15.250
				13.0	0.502	0.028	0.361	13.150	15.000

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	24E		3896595	6.0	0.560	0.032	0.624	14.800	14.500
	27E		3896895						
	30E		3897195	6.0	0.664	0.037	0.725	17.050	13.450
90N	42W	274300	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295						
	6W		3893595	6.0	0.584	0.031	0.619	18.850	10.800
	3W		3893895	6.0	0.614	0.060	0.828	31.300	3.940
				9.0	0.627	0.022	0.271	12.700	15.400
	0E		3894195	6.0	0.714	0.076	1.920	42.000	1.580
				11.0	1.055	0.114	0.790	25.500	7.400
	3E		3894495	6.0	0.667	0.046	0.752	25.500	7.410
				12.0	0.851	0.061	0.744	23.800	8.030
	6E		3894795	6.0	0.801	0.051	1.080	27.100	5.800
				12.0	0.517	0.026	0.426	13.500	14.200
	9E		3895095	6.0	0.842	0.071	1.440	37.500	2.660
				8.0	1.135	0.126	2.000	42.000	2.730
	12E		3895395	6.0	0.929	0.038	0.779	21.600	8.830
				7.0	0.772	0.031	0.533	17.250	11.050
	15E		3895695	6.0	0.669	0.040	1.400	38.400	2.890
				7.0	1.205	0.135	1.380	38.700	3.270
	18E		3895995	6.0	0.878	0.054	1.060	26.700	8.300

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				7.0	0.682	0.044	1.070	20.800	10.850
	21E		3896295						
	24E		3896595						
	27E		3896895						
	30E		3897195						
87N	42W	274000	3889995						
	39W		3890295						
	36W		3890595						
	33W		3890895						
	30W		3891195						
	27W		3891495						
	24W		3891795						
	21W		3892095						
	18W		3892395						
	15W		3892695						
	12W		3892995						
	9W		3893295	6.0	0.546	0.068	0.968	30.600	4.880
				9.0	0.709	0.040	0.616	19.950	8.620
	6W		3893595	6.0	0.538	0.047	0.775	29.900	6.100
				11.0	0.769	0.084	0.534	21.100	9.100
	3W		3893895	4.0	0.625	0.030	0.480	17.000	10.050
	0E		3894195						
	3E		3894495	6.0	0.778	0.034	0.610	19.050	8.800
	6E		3894795	6.0	0.879	0.043	0.772	23.000	7.870
				8.0	0.958	0.047	0.688	21.000	9.770
	9E		3895095	6.0	1.105	0.051	0.980	27.300	8.080
				12.0	1.055	0.028	0.466	15.550	14.200
				13.0	0.960	0.022	0.306	11.700	16.300
	12E		3895395	6.0	0.786	0.058	2.000	27.700	5.540
				8.0	0.576	0.030	0.726	14.100	13.400
	15E		3895695	6.0	0.865	0.041	0.802	16.900	11.650

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				10.0	0.809	0.040	0.799	17.750	11.600
	18E		3895995	3.0	0.443	0.033	0.633	17.200	12.300
	21E		3896295	3.0	0.239	0.010	0.120	5.570	19.650
	24E		3896595	5.0	0.581	0.029	0.540	14.500	14.450
	27E		3896895						
	30E		3897195						
84N	42W	274100	3889995	4.5	0.454	0.034	0.447	15.300	11.350
	39W		3890295	6.0	0.127	0.019	0.385	17.000	3.840
	36W		3890595	6.0	0.157	0.012	0.201	7.430	13.850
	33W		3890895						
	30W		3891195	4.5	0.408	0.024	0.511	13.400	16.300
	27W		3891495	6.0	0.581	0.052	1.090	27.100	5.030
				11.0	0.531	0.027	0.576	16.400	10.150
	24W		3891795	6.0	0.596	0.053	0.813	31.000	5.250
				10.0	0.635	0.041	0.470	20.100	9.090
	21W		3892095	6.0	0.965	0.078	1.540	34.900	3.650
				9.0	0.719	0.040	0.701	20.300	9.910
	18W		3892395	6.0	0.568	0.039	0.478	18.850	11.500
				10.0	0.458	0.022	0.304	12.800	15.300
	15W		3892695						
	12W		3892995	6.0	0.606	0.031	0.637	19.200	11.600
				7.5	0.607	0.035	0.560	19.500	13.050
	9W		3893295	6.0	0.378	0.029	1.020	37.600	2.840
				8.0	0.468	0.067	1.080	33.800	4.680
	6W		3893595	6.0	0.489	0.052	1.050	32.900	5.180
				8.0	0.531	0.089	0.977	28.500	7.260
	3W		3893895						
	0E		3894195	6.0	0.854	0.049	0.573	21.600	6.590
	3E		3894495	6.0	0.631	0.034	0.544	20.200	10.900
				12.0	0.446	0.016	0.309	9.440	17.400
				15.0	0.459	0.021	0.398	12.550	15.500
	6E		3894795	6.0	1.035	0.038	0.722	18.100	13.150

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				12.0	0.549	0.020	0.332	9.940	17.500
	9E		3895095	6.0	0.649	0.037	0.764	18.800	12.400
				8.0	0.485	0.026	0.560	13.950	16.900
	12E		3895395						
	15E		3895695	6.0	0.267	0.013	0.173	6.710	20.700
	18E		3895995						
	21E		3896295						
	24E		3896595						
	27E		3896895						
	30E		3897195						
81N	42W	273400	3889995	3.0	0.271	0.014	0.201	7.790	19.650
	39W		3890295						
	36W		3890595						
	33W		3890895	6.0	0.601	0.037	0.514	20.100	9.220
				7.0	0.730	0.039	0.598	21.200	8.130
	30W		3891195	6.0	1.005	0.068	1.690	35.700	2.650
				12.0	1.385	0.054	1.060	27.700	6.960
				15.0	1.285	0.045	0.847	24.000	8.150
	27W		3891495	6.0	0.705	0.070	0.894	26.500	6.870
				9.0	0.728	0.051	0.551	18.650	10.700
	24W		3891795	6.0	0.910	0.108	1.440	42.000	1.890
				8.0	0.737	0.040	0.455	15.900	14.100
	21W		3892095						
	18W		3892395	6.0	0.708	0.062	1.260	30.100	5.470
				7.5	0.763	0.067	0.600	20.400	11.000
	15W		3892695	6.0	0.657	0.053	0.921	32.200	5.100
				12.0	0.785	0.030	0.407	17.650	11.850
				15.0	0.711	0.026	0.371	15.550	13.000
	12W		3892995	6.0	0.488	0.038	0.892	30.300	5.500
				8.0	0.632	0.049	1.070	30.300	6.330
	9W		3893295						
	6W		3893595	6.0	0.895	0.067	1.170	34.100	3.690

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				7.0	0.751	0.049	1.100	25.000	10.200
	3W		3893895	6.0	0.424	0.018	0.311	10.950	17.050
				12.0	0.218	0.010	0.151	7.920	18.200
				13.0	0.234	0.011	0.169	7.970	18.250
	0E		3894195						
	3E		3894495	6.0	0.801	0.042	0.705	21.700	10.200
				10.0	0.660	0.031	0.549	16.850	12.350
	6E		3894795	6.0	0.602	0.039	0.848	19.950	10.100
				8.0	0.292	0.014	0.216	7.070	18.300
	9E		3895095	6.0	0.793	0.053	0.876	32.500	4.060
	12E		3895395	6.0	0.634	0.042	0.700	20.100	11.750
				11.0	0.376	0.021	0.315	10.900	17.000
	15E		3895695						
	18E		3895995	6.0	1.010	0.078	1.640	38.600	3.260
	21E		3896295	6.0	0.819	0.052	0.921	24.900	9.380
				10.5	0.794	0.047	0.861	24.600	9.880
	24E		3896595	6.0	0.705	0.035	0.615	18.000	15.550
				9.0	0.544	0.021	0.364	10.000	18.350
	27E		3896895	6.0	0.495	0.021	0.401	10.400	18.500
				9.0					
	30E		3897195						
78N	0E	273100	3894195	6.0	0.690	0.044	0.523	15.700	12.350
				10.0	0.808	0.047	0.326	14.250	11.750
	3E		3894495	6.0	0.383	0.016	0.240	10.350	16.350
				11.0	0.366	0.015	0.239	8.890	17.450
	6E		3894795	5.0	0.544	0.031	0.572	21.000	9.240
	9E		3895095	6.0	0.569	0.027	0.563	14.000	15.850
	12E		3895395	6.0	1.390	0.061	0.976	30.000	6.780
				11.0	1.095	0.031	0.488	15.950	13.450
	15E		3895695	6.0	0.455	0.028	0.633	15.200	15.800
	18E		3895995						
	21E		3896295	6.0	0.393	0.019	0.355	11.000	15.350

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	24E		3896595	6.0	0.802	0.047	0.889	23.700	10.400
				9.0	0.644	0.034	0.591	16.600	14.000
	27E		3896895	6.0	0.993	0.081	1.870	40.300	2.450
				10.0	0.698	0.047	0.989	23.700	11.100
	30E		3897195	4.0	0.696	0.034	0.707	18.750	12.050
75N	0E	272800	3894195	6.0	0.874	0.026	0.452	14.700	13.050
				12.0	0.625	0.021	0.389	12.850	14.800
				13.5	0.616	0.020	0.364	11.850	15.450
	3E		3894495	6.0	0.308	0.014	0.221	8.560	17.750
	6E		3894795	6.0	0.837	0.022	0.378	12.850	15.900
				12.0	0.884	0.032	0.589	17.800	11.950
				15.0	0.715	0.030	0.490	17.150	12.450
	9E		3895095	6.0	0.847	0.053	0.495	19.800	11.150
				9.0	0.810	0.053	0.414	17.950	12.800
	12E		3895395	6.0	0.552	0.028	0.405	13.250	16.200
				12.0	0.458	0.019	0.277	9.490	18.450
				18.0	0.351	0.017	0.205	7.810	18.150
				24.0	0.319	0.016	0.267	7.830	19.050
	15E		3895695	5.0	0.911	0.055	0.946	29.600	7.150
	18E		3895995	3.0	0.938	0.027	0.360	14.250	14.700
	21E		3896295						
	24E		3896595						
	27E		3896895						
	30E		3897195						
	33E		3897495						
	36E		3897795						
	39E		3898095						
	42E		3898395						
72N	0E	272500	3894195	6.0	0.910	0.026	0.414	13.900	14.500
				12.0	0.678	0.020	0.278	10.700	16.700
				14.0	0.573	0.020	0.315	10.500	17.250
	3E		3894495	3.0	0.729	0.030	0.652	15.350	14.000

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	6E		3894795	6.0	1.280	0.067	1.070	25.400	8.920
	9E		3895095	6.0	0.828	0.039	0.849	22.200	10.100
				7.0	0.453	0.019	0.258	11.000	16.050
	12E		3895395	6.0	0.871	0.034	0.370	16.050	13.250
				12.0	0.888	0.035	0.369	16.550	13.250
				13.5	0.903	0.032	0.393	15.950	13.550
	15E		3895695	6.0	0.848	0.079	0.689	21.600	10.350
				9.0	0.777	0.057	0.840	30.300	4.550
	18E		3895995	6.0	0.545	0.029	0.289	13.050	15.300
	21E		3896295	6.0	0.913	0.042	0.867	19.900	13.400
				9.0	0.907	0.025	0.450	11.900	16.800
	24E		3896595	6.0	0.669	0.038	0.702	18.400	13.150
	27E		3896895	6.0	0.579	0.036	0.801	17.450	14.050
	30E		3897195	6.0	1.015	0.089	1.985	48.900	1.590
				12.0	1.075	0.098	1.425	36.800	5.350
	33E		3897495	6.0	1.155	0.059	1.275	25.300	10.500
				9.0	1.160	0.045	0.916	20.300	12.600
	36E		3897795	6.0	0.986	0.082	1.850	41.500	3.440
				12.0	1.090	0.040	0.595	18.550	13.700
	39E		3898095	6.0	0.775	0.043	1.180	23.900	11.500
	42E		3898395						
69N	0E	272200	3894195	6.0	0.699	0.040	0.840	20.800	10.650
				9.0	0.662	0.039	0.816	20.200	11.000
	3E		3894495	6.0	1.145	0.044	0.647	20.300	12.300
				12.0	0.828	0.028	0.409	13.500	15.650
				14.5	0.994	0.093	1.980	36.500	4.000
	6E		3894795	6.0	0.753	0.021	0.294	10.850	17.350
	9E		3895095	6.0	0.951	0.025	0.593	16.100	14.150
				9.0	0.701	0.040	0.653	18.750	13.500
	12E		3895395	6.0	1.030	0.044	0.663	21.200	13.250
	15E		3895695	6.0	1.440	0.150	1.890	36.600	3.120
				9.0	1.060	0.123	1.750	37.300	3.030

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	18E		3895995	6.0	1.140	0.057	1.210	30.400	5.630
				12.0	1.290	0.051	0.914	25.000	9.520
				14.0	1.490	0.043	0.686	18.400	13.150
	21E		3896295	6.0	1.010	0.061	1.570	36.900	3.430
				12.0	1.460	0.073	1.310	27.700	9.470
				15.0	1.490	0.070	1.320	26.900	7.870
	24E		3896595	6.0	0.849	0.048	0.771	23.300	11.200
				9.0	0.977	0.041	0.672	17.750	15.350
	27E		3896895	5.0	1.040	0.067	2.090	31.500	10.050
	30E		3897195	6.0	0.895	0.059	1.180	26.600	10.850
				10.0	0.806	0.047	1.040	22.200	11.950
	33E		3897495	6.0	1.230	0.190	2.000	41.100	3.740
				12.0	1.370	0.081	1.450	30.100	6.940
	36E		3897795	6.0	0.578	0.040	0.998	18.700	14.500
	39E		3898095	6.0	0.872	0.062	1.810	30.100	7.840
	42E		3898395						
66N	0E	271900	3894195	6.0	0.441	0.019	0.247	9.160	18.500
				8.0	0.492	0.016	0.220	8.600	18.400
	3E		3894495	6.0	0.640	0.023	0.284	10.150	18.100
				8.0	0.575	0.017	0.215	8.400	18.400
	6E		3894795	6.0	1.130	0.032	0.624	14.000	16.550
				8.5	0.897	0.020	0.339	9.440	19.450
	9E		3895095	6.0	0.788	0.072	1.090	28.400	8.170
				12.0	0.745	0.044	0.685	17.350	14.700
				18.0	0.393	0.015	0.199	6.780	19.950
	12E		3895395	6.0	0.570	0.046	1.930	33.600	2.840
				12.0	1.220	0.098	1.020	32.600	8.100
				15.0	0.713	0.025	0.301	9.490	18.300
	15E		3895695	6.0	0.763	0.069	1.370	29.600	5.180
	18E		3895995	6.0	0.629	0.042	1.050	33.800	3.880
				9.0	0.678	0.048	0.613	22.200	10.150

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	21E		3896295	6.0	0.582	0.050	1.130	33.300	2.700
				10.0	0.987	0.120	1.030	30.800	4.470
	24E		3896595	6.0	0.487	0.027	0.391	13.600	15.050
				9.0	0.500	0.029	0.450	15.100	14.200
	27E		3896895						
	30E		3897195						
	33E		3897495						
	36E		3897795						
	39E		3898095						
	42E		3898395						
63N	0E	271600	3894195	6.0	0.876	0.027	0.350	11.800	16.200
				11.0	0.788	0.019	0.270	9.260	17.900
	3E		3894495	6.0	1.200	0.177	1.860	40.800	3.040
				10.5	1.440	0.201	0.688	19.550	11.200
	6E		3894795	6.0	1.250	0.044	0.791	19.850	11.700
				10.0	1.360	0.040	0.688	17.250	12.850
	9E		3895095	6.0	1.070	0.130	1.150	34.000	5.650
				8.0	1.520	0.178	1.850	37.500	5.020
	12E		3895395	6.0	0.724	0.021	1.540	41.800	1.280
				12.0	0.927	0.111	1.070	32.900	3.950
				15.0	1.360	0.091	1.160	35.900	4.810
	15E		3895695	6.0	0.621	0.056	1.630	28.600	3.220
				12.0	0.916	0.060	0.691	18.150	9.080
	18E		3895995						
	21E		3896295						
	24E		3896595						
	27E		3896895	6.0	0.635	0.064	1.170	36.800	2.850
				12.0	0.783	0.094	1.330	37.100	3.130
				13.5	0.668	0.043	0.433	21.600	9.220
	30E		3897195						
	33E		3897495	6.0	0.638	0.032	0.595	15.350	15.450

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				9.0	0.574	0.023	0.437	10.750	17.800
	36E		3897795	6.0	0.690	0.049	1.030	22.900	11.700
	39E		3898095	6.0	0.521	0.032	0.908	16.050	15.250
				8.0	0.467	0.029	0.746	14.500	14.450
	42E		3898395	6.0	0.852	0.062	1.380	31.800	6.030
				12.0	0.564	0.035	0.686	18.150	13.200
60N	0E	271300	3894195	6.0	0.978	0.060	1.170	29.500	13.350
				7.5	0.561	0.032	0.569	16.000	13.400
	3E		3894495	6.0	1.020	0.081	0.791	27.700	5.950
				9.0	0.909	0.054	0.431	14.550	13.450
	6E		3894795	6.0	0.725	0.064	1.690	42.600	1.510
				12.0	0.800	0.140	1.600	42.400	1.940
				15.0	1.050	0.167	1.070	31.100	5.960
				18.0	0.849	0.167	1.350	40.600	2.290
				20.0	1.155	0.197	1.190	34.200	5.110
	9E		3895095	6.0	0.731	0.066	1.700	42.300	0.550
				12.0	1.270	0.123	1.180	34.800	3.660
				14.0	1.410	0.119	0.954	30.400	4.920
	12E		3895395	6.0	0.442	0.043	1.200	33.600	1.710
				12.0	0.453	0.057	1.190	32.900	1.900
				16.0	0.460	0.050	1.170	31.800	2.300
	15E		3895695	6.0	1.130	0.076	0.767	25.600	7.470
				12.0	1.340	0.053	0.495	18.250	11.750
				14.0	1.200	0.055	0.530	19.250	10.500
	18E		3895995	6.0	0.667	0.044	0.894	33.100	2.790
				12.0	0.725	0.101	0.828	30.000	4.660
				13.0	0.977	0.125	0.699	25.300	6.290
	21E		3896295	6.0	0.784	0.036	0.658	19.300	9.460
				12.0	1.180	0.091	0.805	29.100	4.710
	24E		3896595	6.0	0.842	0.050	0.966	29.700	5.650
				9.0	0.549	0.018	0.332	12.050	14.550
	27E		3896895	6.0	0.806	0.034	0.464	18.750	10.150

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	30E		3897195						
	33E		3897495	6.0	0.992	0.074	1.500	34.300	6.060
				8.0	0.768	0.033	0.756	17.350	13.750
	36E		3897795	5.0	1.035	0.048	1.270	24.100	10.050
	39E		3898095	6.0	0.816	0.036	0.599	18.550	13.250
				11.0	0.598	0.022	0.350	11.450	16.750
	42E		3898395	6.0	0.570	0.031	0.774	17.000	13.450
				8.0	0.429	0.023	0.433	12.700	16.200
	45E		3898695	6.0	0.746	0.058	1.910	29.600	6.760
				9.0	0.435	0.020	0.607	11.300	16.100
	48E		3898995						
	51E		3899295						
	54E		3899595						
57N	0E	271000	3894195	6.0	0.858	0.104	1.170	34.100	5.120
	3E		3894495	6.0	0.932	0.063	1.580	29.900	7.030
				8.0	0.779	0.050	1.160	23.500	9.550
	6E		3894795	6.0	0.728	0.052	1.230	32.500	3.920
				12.0	1.060	0.074	1.020	28.000	8.370
				14.0	0.968	0.047	0.753	21.100	11.950
	9E		3895095	6.0	0.922	0.047	0.746	26.200	4.940
				10.0	1.010	0.043	0.701	24.500	5.950
	12E		3895395	6.0	0.570	0.042	1.140	34.900	2.520
				12.0	0.754	0.093	0.958	35.400	2.920
				14.0	1.000	0.138	1.020	36.200	2.770
	15E		3895695	6.0	0.704	0.061	1.060	32.700	2.310
				8.0	0.663	0.049	0.238	16.300	7.220
	18E		3895995	6.0	0.685	0.096	1.260	36.800	2.830
				10.0	1.130	0.077	0.704	23.900	6.120
	21E		3896295	6.0					
				9.0					
	24E		3896595	6.0	0.765	0.042	0.902	20.400	10.150

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				8.0	0.722	0.037	0.690	20.300	11.600
	27E		3896895	5.0	0.730	0.065	1.050	27.700	4.550
	30E		3897195	5.0	0.796	0.027	0.540	14.650	13.400
	33E		3897495	6.0	1.415	0.091	1.550	33.200	5.760
				9.0	1.240	0.036	0.656	17.000	13.150
	36E		3897795	6.0	1.515	0.057	1.510	30.400	6.800
				9.0	1.750	0.066	1.300	31.800	5.640
	39E		3898095	6.0	0.754	0.033	0.826	16.250	13.950
				9.0	0.858	0.041	1.020	19.800	11.800
	42E		3898395	5.0	0.536	0.026	0.537	14.850	14.650
	45E		3898695	4.0	0.518	0.032	0.800	16.650	12.450
	48E		3898995	6.0	0.597	0.031	0.625	15.700	13.850
				9.0	0.540	0.028	0.622	14.650	15.500
	51E		3899295						
	54E		3899595						
54N	0E	270700	3894195	6.0	0.677	0.030	0.451	15.450	13.900
	3E		3894495	6.0	0.619	0.030	0.403	16.500	11.700
	6E		3894795	6.0	0.367	0.034	1.020	33.100	4.390
				12.0	0.488	0.132	0.980	28.500	5.840
				15.0	0.692	0.116	0.798	25.900	6.060
	9E		3895095	6.0	0.605	0.075	0.864	30.900	5.320
				8.0	0.921	0.089	0.816	28.400	4.590
	12E		3895395	6.0	0.958	0.100	1.830	>50	0.610
				11.0	1.185	0.241	1.360	>50	0.530
	15E		3895695	6.0	1.505	0.067	1.220	26.000	9.060
				7.5	1.125	0.166	2.330	42.900	2.280
	18E		3895995	6.0	1.040	0.049	2.860	25.600	8.350
				7.0	1.115	0.040	1.910	20.300	11.700
	21E		3896295	6.0	0.347	0.027	1.230	35.000	1.000
				8.0	0.339	0.030	1.470	36.100	0.980
	24E		3896595	6.0	1.205	0.032	0.519	16.350	13.400
	27E		3896895	6.0	0.553	0.034	0.832	18.150	10.000

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				8.0	0.402	0.024	0.430	11.950	16.300
	30E		3897195	6.0	0.613	0.054	1.770	27.200	3.840
				12.0	0.676	0.083	1.160	31.300	4.400
	33E		3897495	6.0	0.901	0.058	0.916	29.400	5.600
				12.0	1.080	0.049	0.804	22.200	9.550
				13.5	1.155	0.047	0.686	19.650	10.750
	36E		3897795	6.0	0.915	0.082	1.850	36.600	3.680
				9.0	1.090	0.108	1.750	34.300	6.110
	39E		3898095	6.0	0.850	0.049	1.030	22.000	10.750
				9.0	0.390	0.013	0.214	6.580	19.250
	42E		3898395	6.0	0.480	0.024	0.423	11.550	17.500
	45E		3898695	6.0	0.564	0.030	1.090	14.600	14.350
	48E		3898995	3.0	0.370	0.021	0.350	9.920	16.450
	51E		3899295						
	54E		3899595						
51N	0E	270400	3894195						
	3E		3894495	6.0	0.880	0.046	0.720	23.400	10.150
				9.0	0.777	0.072	0.716	25.500	8.750
	6E		3894795	6.0	0.759	0.075	0.720	25.600	8.480
				10.0	0.851	0.097	0.806	30.100	4.420
	9E		3895095	6.0	0.615	0.064	1.040	30.100	4.840
				10.0	0.972	0.069	0.676	27.300	4.880
	12E		3895395	6.0	0.750	0.113	1.110	32.800	6.130
				7.5	0.895	0.194	1.030	26.600	9.750
	15E		3895695	6.0	1.110	0.094	0.954	21.300	12.350
				12.0	0.978	0.053	0.709	14.500	16.050
	18E		3895995	6.0	0.854	0.093	1.540	37.400	3.180
	21E		3896295	6.0	0.875	0.079	0.900	36.500	2.270
				12.0	1.455	0.070	0.570	21.800	9.090
				13.0	1.980	0.054	0.647	24.600	13.750
	24E		3896595	6.0	1.160	0.146	1.580	37.600	5.060

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				10.5	1.300	0.069	0.707	22.300	11.450
	27E		3896895	6.0	0.786	0.044	1.060	20.400	11.600
				10.5	0.668	0.033	0.693	16.250	13.600
	30E		3897195	6.0	0.653	0.052	2.160	22.500	5.400
				10.0	0.540	0.050	2.090	27.300	3.440
	33E		3897495	6.0	0.811	0.099	1.280	37.700	2.570
				10.0	1.145	0.063	0.794	25.900	6.820
	36E		3897795	6.0	1.090	0.076	0.392	14.750	15.250
	39E		3898095	6.0	0.670	0.075	1.770	33.700	3.870
				7.5	0.913	0.086	1.940	40.500	3.130
	42E		3898395	6.0	0.753	0.090	1.560	38.500	3.190
				9.0	0.789	0.096	1.610	39.900	3.100
	45E		3898695	6.0	0.868	0.051	1.090	26.100	7.790
				9.0	0.887	0.047	0.976	23.700	9.340
	48E		3898995	6.0	1.110	0.131	1.800	37.000	3.720
	51E		3899295	6.0	1.255	0.041	0.723	19.000	12.000
				9.0	0.920	0.027	0.487	13.400	15.600
	54E		3899595						
48N	0E	270100	3894195	6.0	0.494	0.023	0.302	11.700	14.100
				12.0	0.443	0.020	0.299	10.750	15.100
				14.0	0.363	0.015	0.219	8.270	16.500
	3E		3894495	6.0	0.522	0.029	0.673	15.800	12.700
	6E		3894795	6.0	0.515	0.099	1.710	44.000	0.660
				9.0	0.560	0.153	1.310	42.200	0.810
	9E		3895095	6.0	0.784	0.129	1.260	32.600	5.440
				12.0	0.977	0.124	0.770	23.500	6.610
	12E		3895395	6.0	0.722	0.059	1.110	33.800	4.040
	15E		3895695	6.0	0.758	0.049	1.020	23.700	8.520
				9.0	1.190	0.061	0.611	17.950	12.450
	18E		3895995	6.0	0.936	0.087	1.590	37.200	3.560
				7.5	1.335	0.113	1.200	28.900	7.610

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	21E		3896295	6.0	1.170	0.099	1.440	35.900	4.930
				9.0	1.095	0.068	0.985	28.100	6.150
	24E		3896595	6.0	1.060	0.060	1.560	40.800	1.960
				10.0	1.460	0.070	1.220	34.300	5.940
	27E		3896895	6.0	0.816	0.041	0.828	18.250	13.400
				9.0	0.696	0.036	0.729	16.500	14.150
	30E		3897195	6.0	1.060	0.073	0.927	22.900	10.700
	33E		3897495	6.0	0.422	0.038	1.410	25.600	3.310
				7.5	0.442	0.035	1.510	30.500	2.440
	36E		3897795						
	39E		3898095	6.0	1.170	0.073	1.480	34.000	5.000
				12.0	1.105	0.051	0.989	24.900	9.210
	42E		3898395	6.0	0.596	0.063	0.823	29.600	5.420
				7.0	0.721	0.084	0.910	28.900	6.080
	45E		3898695	6.0	0.921	0.121	1.630	41.700	2.510
				9.5	1.190	0.172	1.700	40.200	2.980
	48E		3898995	6.0	0.404	0.020	0.280	9.710	17.650
				9.0	0.615	0.040	0.972	18.000	13.000
	51E		3899295	6.0	1.190	0.093	2.190	41.500	2.490
				11.0	1.065	0.046	0.956	21.700	10.700
	54E		3899595	6.0	0.458	0.019	0.310	9.970	17.050
45N	0E	269800	3894195						
	3E		3894495						
	6E		3894795	6.0	0.345	0.031	2.260	31.800	1.700
	9E		3895095	6.0	0.895	0.114	2.070	45.500	1.990
				8.0	1.270	0.156	1.560	38.000	4.660
	12E		3895395	6.0	1.120	0.139	1.590	36.700	4.730
				12.0	1.420	0.146	1.340	32.300	7.620
	15E		3895695	6.0	0.672	0.048	0.922	30.500	4.670
				7.0	1.055	0.044	0.796	25.000	5.970
	18E		3895995	6.0	1.265	0.093	0.965	40.600	3.030

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				11.0	1.315	0.115	0.389	18.450	13.700
	21E		3896295	6.0	0.891	0.102	1.520	44.400	0.960
				11.0	1.100	0.166	0.706	28.300	7.600
	24E		3896595	6.0	1.180	0.121	2.980	43.500	1.140
				12.0	1.740	0.051	0.673	19.700	11.550
				15.0	1.550	0.150	1.720	25.300	9.870
	27E		3896895	6.0	1.710	0.050	0.651	19.300	11.400
				9.5	1.410	0.118	2.590	28.800	8.420
	30E		3897195	6.0	1.350	0.147	2.310	45.500	1.780
				11.0	1.490	0.125	1.120	26.800	10.150
	33E		3897495	3.0	0.563	0.041	1.020	24.400	8.740
	36E		3897795	6.0	0.811	0.051	0.733	25.200	4.920
	39E		3898095						
	42E		3898395	6.0	0.674	0.065	0.849	29.900	4.050
				9.0	0.762	0.034	0.536	18.500	9.110
	45E		3898695	6.0	1.470	0.028	0.336	14.300	13.300
				12.0	0.951	0.017	0.214	8.620	17.450
	48E		3898995	6.0	1.180	0.054	0.751	22.100	11.100
				12.0	0.884	0.022	0.330	10.800	16.000
				13.5	0.856	0.026	0.348	12.050	16.450
	51E		3899295	6.0	0.780	0.057	1.230	24.000	10.200
				10.5	1.210	0.025	0.398	13.250	15.000
	54E		3899595	6.0	0.395	0.021	0.344	10.100	17.300
				8.0	0.333	0.017	0.281	8.630	18.400
	57E		3899895						
	60E		3900195						
42N	0E	269500	3894195						
	3E		3894495						
	6E		3894795						
	9E		3895095	6.0	0.483	0.034	1.060	37.000	1.660
				11.0	0.809	0.053	0.597	22.200	9.390

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	12E		3895395	6.0	0.591	0.083	2.410	48.600	1.070
				12.0	1.110	0.189	1.630	36.100	5.870
				15.0	1.320	0.124	0.874	26.800	8.370
	15E		3895695	6.0	0.994	0.060	1.200	26.600	9.660
				9.0	1.050	0.046	0.981	21.600	11.900
	18E		3895995	6.0	0.977	0.068	2.370	48.900	0.870
				12.0	1.170	0.164	2.140	44.200	2.840
				18.0	1.330	0.104	0.900	22.300	12.200
				21.0	1.420	0.075	0.800	19.400	13.700
	21E		3896295	6.0	0.794	0.064	0.732	24.700	7.360
	24E		3896595	6.0	1.020	0.151	0.810	>50	0.590
				11.5	1.580	0.054	0.852	24.500	9.370
	27E		3896895	6.0	1.210	0.083	1.370	40.000	2.310
				12.0	1.350	0.192	1.120	39.700	4.450
				15.0	1.600	0.045	0.591	19.500	11.550
	30E		3897195	6.0	0.873	0.077	2.030	46.400	1.620
				12.0	1.030	0.046	0.882	23.000	11.150
	33E		3897495	5.0	0.787	0.040	0.631	22.800	9.810
	36E		3897795	6.0	1.220	0.062	1.120	30.900	6.190
	39E		3898095						
	42E		3898395						
	45E		3898695						
	48E		3898995	5.5	0.591	0.028	0.456	16.050	14.500
	51E		3899295	6.0	1.320	0.075	1.610	31.000	6.990
				8.0	0.525	0.028	0.433	14.100	15.750
	54E		3899595	6.0	0.675	0.038	0.889	18.400	13.900
				9.0	0.645	0.038	0.956	18.550	13.500
	57E		3899895	6.0	0.315	0.015	0.219	7.440	20.000
				9.5	1.310	0.089	1.770	33.500	5.340
	60E		3900195	6.0	0.534	0.033	0.670	17.900	12.250
39N	0E	269200	3894195	6.0	0.323	0.018	0.313	11.350	16.650
				9.0	0.261	0.011	0.180	7.090	19.550

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	3E		3894495	6.0	0.759	0.048	1.260	24.600	11.100
				12.0	0.408	0.020	0.405	10.500	18.050
	6E		3894795	6.0	0.581	0.044	1.530	25.700	8.170
	9E		3895095	6.0	0.505	0.031	0.409	12.900	14.850
				9.0	0.483	0.019	0.233	9.970	16.850
	12E		3895395	6.0	0.692	0.066	1.060	23.100	10.650
				8.5	0.468	0.032	0.456	11.550	16.050
	15E		3895695	6.0	1.030	0.080	0.924	22.000	12.250
				12.0	1.060	0.044	0.578	12.050	16.450
	18E		3895995	6.0	0.798	0.157	2.580	49.200	0.670
				12.0	0.998	0.180	2.360	44.300	1.090
				14.0	1.455	0.073	0.763	19.250	12.100
	21E		3896295						
	24E		3896595	6.0	1.070	0.075	0.769	18.400	13.000
				7.0	0.990	0.082	0.876	20.200	12.600
	27E		3896895	6.0	0.843	0.090	2.160	44.900	1.800
				10.0	0.955	0.127	1.915	43.600	2.280
	30E		3897195	6.0	1.220	0.133	1.290	30.200	9.120
				12.0	1.295	0.086	0.713	22.600	8.670
				18.0	0.671	0.086	1.060	36.100	3.260
	33E		3897495	6.0	0.951	0.100	0.740	26.700	5.080
				7.5	1.085	0.079	0.895	25.500	5.050
	36E		3897795	6.0	1.050	0.056	1.230	27.100	7.350
				9.0	0.739	0.041	0.849	19.100	12.250
	39E		3898095	6.0	0.430	0.030	1.300	28.900	2.310
				7.0	0.463	0.025	1.310	31.300	1.320
	42E		3898395	6.0	0.635	0.037	0.610	20.400	9.700
	45E		3898695						
	48E		3898995						
	51E		3899295						
	54E		3899595						
	57E		3899895						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	60E		3900195						
36N	0E	268900	3894195	3.0	0.432	0.022	0.482	10.900	16.600
	3E		3894495	6.0	0.430	0.046	0.968	23.400	7.750
				7.0	0.424	0.034	0.677	18.600	11.050
	6E		3894795	3.0	0.323	0.016	0.458	11.000	12.950
	9E		3895095						
	12E		3895395						
	15E		3895695	6.0	0.628	0.057	0.586	19.650	7.360
				11.0	0.649	0.046	0.659	21.500	9.240
	18E		3895995	6.0	0.799	0.040	2.350	48.400	0.840
				10.0	1.050	0.134	1.470	35.100	6.460
	21E		3896295						
	24E		3896595						
	27E		3896895	6.0	0.808	0.096	1.180	29.600	8.260
				8.0	0.717	0.095	1.020	28.700	9.240
	30E		3897195	6.0	0.772	0.082	1.360	37.300	3.170
				9.0	0.907	0.121	0.721	24.900	7.610
	33E		3897495	6.0	0.760	0.035	0.934	35.500	2.800
				12.0	1.080	0.089	0.850	30.100	3.510
				15.0	1.170	0.078	0.825	29.100	3.440
	36E		3897795	6.0	0.787	0.080	1.340	40.500	1.870
				9.0	0.917	0.196	1.490	38.800	4.620
	39E		3898095	6.0	0.240	0.017	0.539	23.600	0.440
				7.0	0.278	0.019	0.620	25.800	0.460
	42E		3898395	6.0					
				10.0	0.549	0.063	1.410	38.000	2.840
	45E		3898695	6.0	0.924	0.081	1.740	42.300	2.340
				8.5	1.040	0.078	0.951	25.900	8.920
	48E		3898995	6.0	0.426	0.043	0.706	22.300	3.840
				10.0	0.626	0.113	1.360	35.800	4.050
	51E		3899295	6.0	0.884	0.135	1.900	45.400	1.750

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				10.0	0.570	0.096	0.962	28.500	5.160
	54E		3899595						
	57E		3899895						
	60E		3900195						
33N	0E	268600	3894195						
	3E		3894495						
	6E		3894795						
	9E		3895095						
	12E		3895395						
	15E		3895695						
	18E		3895995						
	21E		3896295						
	24E		3896595						
	27E		3896895	6.0	0.485	0.054	1.160	33.800	2.870
				7.5	0.427	0.059	0.843	28.400	4.780
	30E		3897195	6.0	0.512	0.091	0.768	25.300	6.280
				12.0	0.501	0.062	0.820	26.400	6.080
				14.0	0.531	0.053	0.855	28.000	6.500
	33E		3897495	6.0	1.010	0.064	0.859	27.100	7.140
				10.0	1.150	0.153	1.510	33.700	5.170
	36E		3897795	6.0	0.922	0.079	1.640	39.000	2.270
				12.0	1.100	0.059	1.160	29.600	6.760
	39E		3898095	6.0	0.717	0.085	0.971	28.800	2.510
	42E		3898395	6.0	0.663	0.072	0.932	34.000	2.410
				12.0	0.681	0.130	0.383	14.550	13.850
				15.0	0.626	0.123	0.360	13.550	13.900
	45E		3898695	6.0	0.864	0.073	1.470	41.500	2.300
				9.0	0.836	0.127	0.833	27.500	7.070
	48E		3898995	6.0	0.803	0.096	1.580	37.500	4.000
				12.0	1.220	0.042	0.711	21.200	11.650
	51E		3899295	6.0	0.816	0.051	1.040	21.800	11.050
				12.0	0.738	0.063	0.367	10.450	18.700

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				13.0	0.831	0.059	0.376	11.100	18.600
	54E		3899595	6.0	0.525	0.045	1.370	31.000	5.300
				10.0	0.840	0.047	0.543	15.900	12.850
	57E		3899895	6.0	0.741	0.044	0.654	22.200	10.250
				9.0	0.774	0.034	0.612	15.200	14.350
	60E		3900195	6.0	0.431	0.038	1.470	38.500	2.270
30N	0E	368300	3894195						
	3E		3894495						
	6E		3894795						
	9E		3895095						
	12E		3895395						
	15E		3895695						
	18E		3895995						
	21E		3896295						
	24E		3896595						
	27E		3896895						
	30E		3897195	6.0	0.506	0.072	0.950	30.900	3.960
				8.0	0.709	0.105	0.754	25.200	4.620
	33E		3897495	6.0	0.747	0.183	1.530	32.800	5.580
				9.0	0.561	0.045	0.554	14.850	14.000
	36E		3897795	6.0	0.718	0.028	1.000	34.300	3.280
				12.0	0.862	0.065	0.974	33.000	3.970
				15.0	1.110	0.121	0.851	29.000	3.720
	39E		3898095	6.0	0.194	0.016	0.202	10.800	2.670
				10.0	0.462	0.028	0.395	14.200	14.700
	42E		3898395	6.0	0.878	0.137	1.620	44.300	1.410
				12.0	0.962	0.138	1.210	39.200	2.310
				14.5	0.977	0.130	0.817	27.700	5.670
	45E		3898695	3.0	0.835	0.083	1.530	38.500	3.950
	48E		3898995	6.0	0.629	0.027	0.409	11.600	15.650
				8.5	0.558	0.024	0.348	9.800	16.200
	51E		3899295						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	54E		3899595						
	57E		3899895						
	60E		3900195						
	63E		3900495						
	66E		3900795						
	69E		3901095						
	72E		3901395						
	75E		3901695						
	78E		3901995						
27N	30E	268000	3897195	6.0	0.554	0.046	0.700	20.700	8.480
				7.0	0.451	0.026	0.480	14.050	13.500
	33E		3897495	6.0	0.502	0.070	1.090	29.100	5.040
				8.0	0.633	0.086	0.832	21.200	6.920
	36E		3897795	6.0	1.020	0.074	0.916	19.900	11.200
				7.0	0.800	0.054	0.921	19.150	11.300
	39E		3898095	6.0	0.626	0.057	0.900	34.400	2.160
				9.0	1.140	0.128	1.050	40.500	1.910
	42E		3898395	6.0	0.578	0.066	0.909	33.200	2.360
				10.0	0.766	0.083	0.660	27.200	4.890
	45E		3898695	5.0	0.977	0.077	1.450	38.700	3.970
	48E		3898995	6.0	0.672	0.078	1.630	31.400	4.550
				7.0	0.781	0.113	1.070	27.300	8.400
	51E		3899295	6.0	0.777	0.053	1.320	30.100	5.640
				9.0	0.561	0.031	0.517	16.250	12.900
	54E		3899595	6.0	0.767	0.111	1.850	38.900	2.450
				7.5	0.932	0.115	1.920	38.100	3.300
	57E		3899895	6.0	0.966	0.043	0.624	20.200	9.950
				8.0	1.360	0.076	1.270	26.900	7.950
	60E		3900195	6.0	0.571	0.045	1.290	25.200	7.380
				9.0	0.577	0.028	0.648	15.850	14.350
	63E		3900495	6.0	0.602	0.026	0.769	17.650	12.100

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				10.0	0.775	0.023	0.489	13.300	14.250
	66E		3900795	6.0	0.717	0.060	1.100	26.200	8.590
				12.0	0.546	0.023	0.355	10.850	16.150
	69E		3901095	5.0	0.685	0.045	1.280	24.600	8.060
	72E		3901395						
	75E		3901695						
	78E		3901995						
24N	30E	267700	3897195						
	33E		3897495	4.0	0.492	0.024	0.435	12.800	12.900
	36E		3897795	5.0	0.250	0.011	0.188	7.470	18.150
	39E		3898095	4.5	0.365	0.022	0.433	12.000	15.700
	42E		3898395	6.0	0.882	0.073	1.820	34.400	4.120
	45E		3898695	6.0	0.794	0.096	0.994	35.600	2.440
				10.5	0.962	0.137	0.745	27.500	4.800
	48E		3898995	6.0	0.662	0.040	0.502	17.150	12.450
				11.0	0.761	0.045	0.276	9.850	15.400
	51E		3899295	6.0	0.948	0.122	1.420	39.800	4.080
	54E		3899595	6.0	1.310	0.104	1.780	39.700	2.500
				7.0	1.250	0.084	1.080	29.900	6.250
	57E		3899895	6.0	1.160	0.053	0.975	25.300	8.330
				9.0	1.100	0.049	0.791	21.800	9.500
	60E		3900195	6.0	0.501	0.020	0.231	14.300	9.630
				9.0	0.559	0.023	0.395	12.800	13.200
	63E		3900495	6.0	0.499	0.033	1.710	43.400	0.890
				9.5	0.759	0.146	1.400	42.800	1.640
	66E		3900795	6.0	0.740	0.025	0.491	12.650	15.350
	69E		3901095	6.0	0.669	0.050	1.380	24.800	6.600
				8.0	0.595	0.050	1.400	26.700	3.330
	72E		3901395	5.0	0.258	0.013	0.167	5.750	19.100
	75E		3901695						
	78E		3901995						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
21N	30E	267400	3897195						
	33E		3897495						
	36E		3897795						
	39E		3898095	3.0	0.490	0.025	0.435	12.750	14.250
	42E		3898395	6.0	0.536	0.023	0.301	12.800	14.100
	45E		3898695	4.0	0.581	0.028	0.555	16.600	11.000
	48E		3898995	6.0	0.732	0.132	0.899	29.200	5.130
				9.0	0.947	0.090	0.522	19.750	8.970
	51E		3899295	6.0	0.811	0.067	2.270	>50	0.830
				12.0	1.080	0.145	0.720	23.900	6.820
				15.0	1.080	0.155	0.847	24.500	7.170
	54E		3899595	6.0	0.726	0.049	1.110	33.200	3.480
				9.0	0.912	0.116	1.220	35.900	2.810
	57E		3899895	6.0	0.821	0.076	1.810	32.400	2.580
				9.0	0.634	0.047	1.710	34.500	2.090
	60E		3900195	6.0	0.469	0.019	0.402	9.750	18.250
				9.0	0.556	0.025	0.544	11.850	16.350
	63E		3900495	6.0	0.528	0.053	1.370	27.700	7.400
				10.0	0.453	0.061	1.770	31.400	4.020
	66E		3900795	6.0	0.620	0.057	1.860	32.700	2.350
				9.0	0.631	0.058	1.830	31.300	2.500
	69E		3901095	6.0	0.729	0.038	0.894	20.800	11.650
	72E		3901395	6.0	0.549	0.029	0.603	15.050	14.000
				8.0	0.435	0.018	0.340	9.070	17.650
	75E		3901695						
	78E		3901995						
18N	30E	267100	3897195						
	33E		3897495						
	36E		3897795						
	39E		3898095						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	42E		3898395						
	45E		3898695	5.0	0.311	0.013	0.227	8.300	18.050
	48E		3898995						
	51E		3899295	6.0	0.597	0.035	0.735	18.900	10.850
				12.0	0.507	0.022	0.507	13.250	14.050
				14.0	0.491	0.015	0.329	8.880	17.500
	54E		3899595	6.0	0.722	0.021	0.347	11.550	16.150
				8.0	0.625	0.019	0.302	10.500	16.800
	57E		3899895						
	60E		3900195						
	63E		3900495	6.0	0.700	0.063	1.430	30.600	6.550
	66E		3900795						
	69E		3901095						
	72E		3901395						
	75E		3901695						
	78E		3901995						
15N	30E	266800	3897195						
	33E		3897495						
	36E		3897795						
	39E		3898095						
	42E		3898395						
	45E		3898695						
	48E		3898995						
	51E		3899295						
	54E		3899595						
	57E		3899895						
	60E		3900195						
	63E		3900495						
	66E		3900795	6	0.477	0.040	0.826	24.400	7.090
				9.5	0.387	0.026	0.389	16.800	11.000
	69E		3901095						

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	72E		3901395	6	0.406	0.048	1.010	29.900	3.430
				9	0.884	0.050	1.040	24.800	6.730
	75E		3901695	6	0.549	0.036	0.673	21.200	8.930
				9	0.407	0.017	0.310	10.200	15.900
	78E		3901995						
12N	60E	266500	3900195						
	63E		3900495						
	66E		3900795						
	69E		3901095						
	72E		3901395						
	75E		3901695						
	78E		3901995						
9N	60E	266200	3900195						
	63E		3900495	6	0.594	0.072	0.918	25.100	5.490
	66E		3900795	6	0.256	0.030	1.430	30.100	2.700
				12	0.444	0.058	0.675	21.500	9.640
				15	0.387	0.041	0.665	18.950	10.550
	69E		3901095	6	0.739	0.057	1.600	32.600	6.050
				8.5	0.752	0.041	1.030	22.600	11.350
	72E		3901395	6	0.678	0.048	0.917	24.900	8.640
				8	0.528	0.020	0.371	11.300	16.100
	75E		3901695	5	0.301	0.012	0.253	6.640	19.850
	78E		3901995						
6N	60E	265900	3900195						
	63E		3900495	6	0.473	0.045	0.940	23.200	9.400
				9	0.387	0.024	0.436	13.050	14.300
	66E		3900795	6	0.394	0.044	0.940	27.200	5.070
				8	0.566	0.060	1.440	28.300	6.190
	69E		3901095	6	0.544	0.057	1.270	27.200	6.520
				12	0.536	0.048	0.925	22.400	8.900
				15	0.419	0.032	0.631	15.350	14.750
	72E		3901395	4	0.373	0.018	0.374	9.360	17.650

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
	75E		3901695	4	0.238	0.009	0.182	4.860	20.800
	78E		3901995						
3N	60E	265600	3900195						
	63E		3900495						
	66E		3900795						
	69E		3901095						
	72E		3901395						
	75E		3901695						
	78E		3901995						
0N	60E	265300	3900195						
	63E		3900495						
	66E		3900795						
	69E		3901095						
	72E		3901395						
	75E		3901695						
	78E		3901995	2	0.590	0.049	1.450	24.400	9.880
				3	0.346	0.020	0.402	10.150	16.500
38.27	16.19	269127	3895814	6	0.860	0.054	0.544	18.050	13.650
				12	0.742	0.047	0.591	19.150	13.000
				15	0.659	0.026	0.356	11.400	16.700
38.27	17.76	269128	3895971	6	0.656	0.106	2.190	40.800	2.150
				12	0.428	0.026	0.296	9.650	19.400
41.24	19.15	269424	3896110	6	1.250	0.100	1.330	34.000	5.100
				12	1.110	0.073	1.080	26.300	9.520
				18	0.855	0.024	0.316	10.400	18.800
41.29	13.98	269429	3895593	6	0.616	0.027	0.280	10.200	17.600
				12	0.592	0.021	0.245	9.510	19.800
				16	0.577	0.017	0.222	7.830	19.700
44.21	12.71	269721	3895466	6	1.320	0.067	0.647	18.200	11.950
44.24	17.65	269724	3895960	6	0.950	0.085	0.644	20.200	13.150
				8	0.915	0.037	0.389	12.150	17.550

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				12	0.813	0.027	0.373	11.100	17.250
47.45	17.17	270045	3895912	6	1.060	0.129	0.943	25.000	8.150
				7	1.035	0.062	0.298	13.500	15.000
				12	1.040	0.083	0.616	20.500	10.400
47.81	22.26	270081	3896421	6	1.295	0.089	0.891	23.000	11.650
				9	1.195	0.050	0.544	15.800	15.800
				11	0.747	0.039	0.427	13.500	16.300
50.14	13.27	270314	3895522	6	1.010	0.019	0.290	9.100	18.550
				11	1.100	0.019	0.258	8.760	18.700
50.34	15.41	270334	3895736	3	0.994	0.053	1.110	26.100	10.350
53.20	19.98	270620	3896193	6	1.160	0.040	0.599	19.150	12.950
53.22	12.04	270622	3895399	6	1.475	0.148	1.260	28.500	9.200
53.78	16.79	270678	3895874		1.015	0.066	1.130	29.800	9.060
56.15	8.33	270915	3895028	6	0.857	0.131	0.895	27.200	6.020
				12	1.140	0.058	0.586	18.500	11.750
				17	0.871	0.030	0.382	12.100	15.550
56.18	11.35	270918	3895331	6	0.797	0.067	0.944	28.200	4.690
				12	1.315	0.072	0.614	24.100	7.050
				14	1.240	0.097	1.060	31.400	5.070
56.19	6.68	270919	3894863	6	0.547	0.026	0.397	13.300	14.000
56.97	21.34	270997	3896329	6	0.459	0.059	1.600	32.000	4.090
				9	1.250	0.030	0.358	15.050	14.850
57.21	17.36	271021	3895931	6	0.986	0.159	0.701	25.000	7.270
				7	1.020	0.165	0.537	18.700	10.550
59.23	8.95	271223	3895090	6	0.958	0.080	1.130	34.500	4.680
				12	1.360	0.120	0.910	29.300	7.050
				15	1.595	0.052	0.485	19.350	11.500
61.68	11.56	271468	3895351	6	0.744	0.100	1.430	40.500	1.170
				12	0.807	0.110	1.460	41.600	1.250
				15	1.115	0.082	1.060	35.100	4.630
62.11	9.03	271511	3895098	6	0.781	0.034	0.447	12.450	16.800
62.28	6.52	271528	3894847	6	1.455	0.071	0.807	18.900	12.200

Proposed drill/sample locations				Sample Information					
Grid cords		State Plane		Sample No. / Depth	Assay values (in percent)				
N-S	E-W	Northing	Easting		Ni	Co	Cr	Fe	Mg
				9	1.440	0.062	0.854	20.000	11.500
				11	0.759	0.027	0.338	9.250	18.200
		total sites:	1120						

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-1 (Page 1 of 5)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/11/08 Date Completed : 9/11/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic	Sampling Method : Continuous Total Depth : 97 Feet Logged By : Obie Strickler Grid Northing : 27 + 32N Grid Easting : 61 + 89E			
Depth in Feet 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0' - 1.5'	Medium reddish brown, oxidized surface soil layer	RFS_1_4	4	0.60	0.04	1.05
1.5' - 4'	Medium yellowish brown, limonite					
4' - 8.5'	Light grey pulverized and fractured serpentine	RFS_1_8.5	4.5	0.12	0.01	0.06
8.5' - 15'	Medium brownish green soil with rock chips	RFS_1_15	6.5	0.70	0.02	0.28
15' - 17'	Medium greenish brown soil with fractured serpentine	RFS_1_17	2	0.36	0.01	0.12
17' - 23'	Medium brownish yellow grading to medium green soil, limonite with serpentine rock chips	RFS_1_23	6	0.47	0.02	0.30
RFS-1 was located just off edge of main road. Top 1' of material was road fill						

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-1

(Page 2 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/11/08
Date Completed : 9/11/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 97 Feet
Logged By : Obie Strickler
Grid Northing : 27 + 32N
Grid Easting : 61 + 89E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20		RFS_1_23	6	0.47	0.02	0.30
21						
22						
23	23' - 25' Medium yellowish brown limonite	RFS_1_25	2	0.34	0.01	0.16
24						
25	25' - 27' Light grey fractured serpentine	RFS_1_27	2	0.12	0.01	0.09
26						
27	27' - 35' Medium brownish grey soil, with rock chips and highly weathered serpentine	RFS_1_35	8	0.23	0.01	0.12
28						
29						
30						
31						
32						
33						
34						
35	35' - 40' Medium yellowish brown soil with fractured serpentine	RFS_1_40	5	0.45	0.01	0.21
36						
37						
38						
39						
40						

RFS-1 was located just off edge of main road. Top 1' of material was road fill

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-1

(Page 3 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/11/08
Date Completed : 9/11/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 97 Feet
Logged By : Obie Strickler
Grid Northing : 27 + 32N
Grid Easting : 61 + 89E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40	40' - 47' Light to medium brownish grey soil with light bluish/greenish highly weathered serpentine	RFS_1_47	7	0.37	0.01	0.13
41						
42						
43						
44						
45						
46						
47	47' - 52' Medium brownish green soil with rock chips. Some light yellowish brown material on exterior of core	RFS_1_52	5	0.22	0.01	0.14
48						
49						
50						
51						
52						
53						
54	52' - 60' Medium brownish grey, highly weathered serpentine	RFS_1_60	8	0.24	0.01	0.14
55						
56						
57						
58						
59						
60						

RFS-1 was located just off edge of main road. Top 1' of material was road fill

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-1

(Page 4 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/11/08
Date Completed : 9/11/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 97 Feet
Logged By : Obie Strickler
Grid Northing : 27 + 32N
Grid Easting : 61 + 89E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60	60' - 70' Medium brownish grey, highly weathered serpentine	RFS_1_70	10	0.22	0.01	0.13
61						
62						
63						
64						
65						
66						
67						
68						
69						
70	70' - 77' Medium brownish grey soil with rock chips, pulverized serpentine from 74.5' to 75.5' bgs	RFS_1_77	7	0.22	0.01	0.14
71						
72						
73						
74						
75						
76						
77						
78						
79						
80	77' - 82' Medium to dark brown and medium to dark grey soil, very coarse grained, possibly highly fractured serpentine	RFS_1_82	5	0.19	0.01	0.13

RFS-1 was located just off edge of main road. Top 1' of material was road fill

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-1

(Page 5 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/11/08
Date Completed : 9/11/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 97 Feet
Logged By : Obie Strickler
Grid Northing : 27 + 32N
Grid Easting : 61 + 89E

Depth in Feet

DESCRIPTION

Sample ID

Sample Interval (Feet)

Ni%

Co%

Cr%

80

81

RFS_1_82

5

0.19

0.01

0.13

82

82' - 97' Light to medium grey fractured serpentine up to 2 to 3" in diameter

83

84

85

86

87

88

89

No Sample

15

NA

NA

NA

90

91

92

93

94

95

96

97

End RFS-1 @ 97' bgs

98

99

100

RFS-1 was located just off edge of main road. Top 1' of material was road fill

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-2 (Page 1 of 2)						
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/11/08 Date Completed : 9/11/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic		Sampling Method : Continuous Total Depth : 27 Feet Logged By : Obie Strickler Grid Northing : 30 + 02N Grid Easting : 42 + 43E				
Depth in Feet	DESCRIPTION			Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0 - 1.5' Light to medium reddish brown, oxidized surface soil layer.			RFS-2-5	5	0.76	0.12	1.76
1								
2	1.5 -10.5' Light to medium yellowish brown, limonite, transition to serpentine at 9.2'			RFS-2-10.5	5.5	0.65	0.09	0.87
3								
4				RFS-2-27	16.5	0.26	0.01	0.18
5								
6								
7								
8								
9								
10								
11	10.5' - 27' Light grey pulverized and fractured serpentine							
12								
13								
14								
15								
16								
17								
18								
19								
20								

Notes:
Boring located off road in open area with good exposure of red, oxidized, surface soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-2A

(Page 1 of 1)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/11/08
Date Completed : 9/11/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 22 Feet
Logged By : Obie Strickler
Grid Northing : 30 + 08N
Grid Easting : 42 + 46E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0 - 1.5' Light to medium reddish brown, oxidized surface soil layer.	RFS-2A-5	5	0.80	0.16	2.14
1						
2	1.5 -9' Medium yellowish brown, limonite	RFS-2A-10	5	0.58	0.09	0.97
3						
4		RFS-2A-12.6	2.6	0.58	0.03	0.43
5						
6		No Sample	9.4			
7						
8		No Sample	9.4			
9	9' - 9.8' Boulder					
10	9.8' - 12.6' Medium yellowish brown, limonite	No Sample	9.4			
11						
12		No Sample	9.4			
13	12.6' - 22' Light grey pulverized and fractured serpentine					
14		No Sample	9.4			
15						
16		No Sample	9.4			
17						
18		No Sample	9.4			
19						
20		No Sample	9.4			
21						
22	End RFS-2A at 22' bgs.	No Sample	9.4			

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-3

(Page 1 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/24/08
Date Completed : 9/24/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 118 Feet
Logged By : Obie Strickler
Grid Northing : 45 + 67N
Grid Easting : 19 + 99E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 1.5' Medium reddish brown, oxidized surface soil	RFS-3-1.5	1.5	0.71	0.06	0.92
1						
2	1.5' - 8' Medium reddish brown to medium yellowish brown soil with rock chips	RFS-3-8	6.5	0.65	0.02	0.32
3						
4						
5						
6						
7						
8	8' - 10' Medium reddish to medium yellowish brown with some light greenish grey soil	RFS-3-10	2	0.28	0.01	0.22
9						
10	10' - 11' Light grey pulverized and fractured serpentine	RFS-3-11	1	0.26	0.01	0.19
11	11' - 11.5' Light to medium bluish/greenish grey highly weathered serpentine	RFS-3-11.5	0.5	0.23	0.01	0.15
12	11.5' - 12.5' Medium reddish to yellowish brown soil	RFS-3-12.5	1	0.44	0.02	0.31
13	12.5' - 13' Light grey pulverized and fractured serpentine	RFS-3-13	0.5	0.26	0.01	0.16
14	13' - 16' Medium brown saprolite (?) with light grey pulverized and fractured serpentine. Small area from 15' to 15.2' bgs of light bluish/greenish grey highly weathered serpentine	RFS-3-16	3	0.24	0.01	0.15
15						
16	16' - 19.5' Light grey pulverized and fractured serpentine	RFS-3-19.5	3.5	0.23	0.01	0.13
17						
18						
19						
20	19.5' - 20' Medium brown saprolite (?) with orange tint	RFS-3-20	0.5	0.25	0.01	0.15

RFS_3 was located on an old skid road, very brushy with red, oxidized surface soil

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-3 (Page 2 of 6)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/24/08 Date Completed : 9/24/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic	Sampling Method : Continuous Total Depth : 118 Feet Logged By : Obie Strickler Grid Northing : 45 + 67N Grid Easting : 19 + 99E			
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20	20' - 21' Light grey pulverized and fractured serpentine	RFS-3-21	1	0.22	0.01	0.12
21	21' - 22.5' Medium orangish brown saprolite(?) with rock chips	RFS-3-22.5	1.5	0.25	0.01	0.17
22						
23	22.5' - 23' Light to medium grey pulverized and fractured serpentine	RFS-3-23	1.5	0.23	0.01	0.16
24	23' - 25' Medium orangish brown saprolite (?) with rock chips	RFS-3-25	2	0.27	0.01	0.16
25	25' - 26' Light grey pulverized and fractured serpentine	RFS-3-26	1	0.29	0.01	0.16
26	26' - 27' Light to medium brown saprolite (?)	RFS-3-27	1	0.30	0.01	0.16
27	27' - 29' Light to dark grey pulverized and fractured serpentine	RFS-3-29	2	0.28	0.01	0.18
28						
29	29' - 29.5' Medium orangish brown soil with rock chips	RFS-3-29.5	0.5	0.30	0.01	0.07
30	29.5' - 31' Light grey pulverized and fractured serpentine	RFS-3-31	1.5	0.24	0.01	0.18
31	31' - 32.5' Medium orangish brown saprolite (?) with rock chips	RFS-3-32.5	1.5	0.33	0.01	0.05
32						
33	32.5' - 33' Light grey pulverized and fractured serpentine	RFS-3-33	0.5	0.33	0.01	0.13
34	33' - 33.5' Light to medium bluish/greenish grey highly weathered serpentine	RFS-3-33.5	0.5	0.26	0.01	0.14
35	33.5' - 35' Light grey pulverized and fractured serpentine	RFS-3-35	1.5	0.25	0.01	0.15
36	35' - 37.5' Medium orangish brown to light grey saprolite (?) with rock chips	RFS-3-37.5	2.5	0.25	0.01	0.18
37						
38	37.5' - 44' Alternating layers of light grey pulverized and fractured serpentine and light bluish/greenish grey highly weathered serpentine	RFS-3-44	6.5	0.23	0.01	0.13
39						
40						

RFS_3 was located on an old skid road, very brushy with red, oxidized surface soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-3

(Page 3 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/24/08
Date Completed : 9/24/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 118 Feet
Logged By : Obie Strickler
Grid Northing : 45 + 67N
Grid Easting : 19 + 99E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40						
41						
42		RFS-3-44	6.5	0.23	0.01	0.13
43						
44	44' - 48' Intermixed layers of medium brown saprolite (?) and light bluish/greenish grey highly weathered serpentine					
45						
46		RFS-3-48	4	0.24	0.01	0.19
47						
48	48' - 51' Light grey pulverized and fractured serpentine					
49						
50		RFS-3-51	3	0.23	0.01	0.18
51						
52	51' - 52' Medium brown saprolite (?) with rock chips	RFS-3-52	1	0.28	0.01	0.22
53	52' - 53' Light bluish/greenish grey highly weathered serpentine	RFS-3-53	1	0.21	0.01	0.14
54	53' - 61' Light grey pulverized and fractured serpentine and light bluish/greenish grey highly weathered serpentine					
55						
56						
57		RFS-3-61	8	0.21	0.01	0.15
58						
59						
60						

RFS_3 was located on an old skid road, very brushy with red, oxidized surface soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-3

(Page 4 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/24/08
Date Completed : 9/24/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 118 Feet
Logged By : Obie Strickler
Grid Northing : 45 + 67N
Grid Easting : 19 + 99E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60		RFS-3-61	8	0.21	0.01	0.15
61	61' - 68' Intermixed layers of light to medium brown saprolite (?) and light bluish/greenish grey highly weathered serpentine					
62	Grab sample of light to medium brown saprolite (?) from 66.5' bgs					
63						
64		RFS-3-66.5	5.5	0.24	0.01	0.15
65						
66						
67		RFS-3-68	1.5	0.24	0.01	0.14
68	68' - 88' Light grey pulverized and fractured serpentine. Only 1.5' of recovery from 78' to 88' due to driller using water					
69						
70						
71						
72						
73						
74		RFS-3-88	20	0.21	0.01	0.13
75						
76						
77						
78						
79						
80						

RFS_3 was located on an old skid road, very brushy with red, oxidized surface soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-3

(Page 6 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/24/08
Date Completed : 9/24/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 118 Feet
Logged By : Obie Strickler
Grid Northing : 45 + 67N
Grid Easting : 19 + 99E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
100						
101		RFS-3-103	9	0.22	0.01	0.13
102						
103	103' - 106.5' Light to medium grey pulverized and fractured serpentine and light bluish/greenish grey highly weathered serpentine					
104		RFS-3-106.5	3.5	0.19	0.01	0.14
105						
106						
107	106.5' - 108' Light to medium yellowish brown soil surrounding rock. Rock content is 80 to 90%.	RFS-3-108	1.5	0.37	0.02	0.24
108	108' - 111' Light brown to light grey pulverized and fractured serpentine					
109		RFS-3-111	3	0.21	0.01	0.16
110						
111	111' - 114' Medium to dark brown soil with rock chips					
112		RFS-3-114	3	0.21	0.01	0.13
113						
114	114' - 118' Light grey pulverized and fractured serpentine					
115		No Sample	4	NA	NA	NA
116						
117						
118	End RFS-3 @ 118 feet bgs					
119						
120						

RFS_3 was located on an old skid road, very brushy with red, oxidized surface soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 1 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 2' Light to medium reddish brown, oxidized surface soil layer.	RFS-4-6	6	1.07	0.08	1.14
1						
2	2' -6' Medium reddish brown soil with rock chips. Lost part of core while moving bag					
3		RFS-4-14	8	0.98	0.02	0.31
4						
5						
6	6' - 14' Medium brown to medium red soil with rock chips					
7						
8		RFS-4-16	2	0.69	0.01	0.19
9						
10	14' - 16' Light grey pulverized and fractured serpentine with rock chips. Small amount of medium brown soil					
11		RFS-4-17.5	1.5	0.94	0.02	0.21
12	16' - 17.5' Medium brown soil, very little rock (10-20%)					
13		RFS-4-26	8.5	0.23	0.01	0.13
14	17.5' - 19.5' Medium brown soil with large amount of rock chips (>60%)					
15						
16						
17						
18						
19						
20						

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 2 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20	19.5' - 26' Light grey pulverized serpentine with rock chips	RFS-4-26	8.5	0.23	0.01	0.13
21						
22						
23						
24						
25	26' - 30.5' Medium grey pulverized and fractured serpentine	RFS-4-30.5	4.5	0.30	0.01	0.16
26						
27						
28						
29						
30	30.5' - 33' Medium brown with yellowish tinge soil, with minor amounts of rock (10-20%)	RFS-4-33	2.5	0.41	0.01	0.17
31						
32	33' - 34' Light grey pulverized and fractured serpentine	RFS-4-34	1	0.28	0.01	0.15
33						
34	34' - 34.5' Medium brownish soil with rock chips	RFS-4-34.5	0.5	0.34	0.01	0.15
35	34.5' - 42' Light grey pulverized and fractured serpentine	RFS-4-42	7.5	0.23	0.01	0.14
36						
37						
38						
39						
40						

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 3 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40						
41		RFS-4-42	7.5	0.23	0.01	0.14
42	42' - 46.5' Medium yellowish soil with rock chips					
43						
44		RFS-4-46.5	4.5	0.31	0.01	0.17
45						
46						
47	46.5' - 48' Light grey pulverized and fractured serpentine	RFS-4-48	1.5	0.30	0.01	0.14
48	48' - 50' Light to medium reddish brown/yellow saprolite (?)					
49		RFS-4-50	2	0.46	0.01	0.17
50	50' - 52' Light grey pulverized and fractured serpentine					
51		RFS-4-52	2	0.27	0.01	0.14
52	52' - 53.5' Light to medium yellowish brown saprolite (?)					
53		RFS-4-53.5	1.5	0.36	0.01	0.16
54	53.5' - 54.5' Light grey pulverized and fractured serpentine	RFS-4-54.5	1	0.27	0.01	0.13
55	54.5' - 59' Medium brown rock chips and saprolite (?)					
56						
57		RFS-4-59	4.5	0.24	0.01	0.11
58						
59	59' - 61' Light grey pulverized and fractured serpentine					
60		RFS-4-61	2	0.21	0.01	0.14

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 4 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60		RFS-4-61	2	0.21	0.01	0.14
61	61' - 62' Medium yellowish brown saprolite (?)	RFS-4-62	1	0.34	0.01	0.19
62	62' - 66' Light grey pulverized and fractured serpentine					
63						
64		RFS-4-66	4	0.28	0.01	0.15
65						
66	66' - 69' Medium yellowish brown soil with saprolite (?)					
67		RFS-4-69	3	0.26	0.01	0.15
68						
69	69' - 70' Light grey pulverized and fractured serpentine	RFS-4-70	1	0.21	0.01	0.15
70	70' - 74' Medium to dark brown soil with saprolite, large rock fragment from 72' to 72.5'					
71						
72		RFS-4-74	4	0.29	0.01	0.13
73						
74	74' - 75' Light grey pulverized and fractured serpentine	RFS-4-75	1	0.20	0.01	0.14
75	75' - 77.5' Medium to dark brown soil and saprolite (?) with rock chips					
76		RFS-4-77.5	2.5	0.25	0.01	0.15
77						
78	77.5' - 83' Light grey pulverized and fractured serpentine from 77.5' to 80' while drilling dry. Solid rock core from 80' to 83' while drilling wet					
79		RFS-4-83	5.5	0.19	0.01	0.13
80						

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 5 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
80						
81		RFS-4-83	5.5	0.19	0.01	0.13
82						
83	83' - 84' Medium brown to dark grey soil with saprolite (?) and rock chips	RFS-4-84	1	0.20	0.01	0.12
84	84' - 88.5' Light grey pulverized and fractured serpentine					
85		RFS-4-88.5	4.5	0.19	0.01	0.13
86						
87						
88						
89	88.5' - 92.5' Medium to dark brownish grey soil with rock chips					
90		RFS-4-92.5	4.5	0.22	0.01	0.15
91						
92						
93	92.5' - 96' Light grey pulverized serpentine					
94		RFS-4-96	3.5	0.23	0.01	0.13
95						
96	96' - 106' Alternating layers of medium brown and light grey soil and rock					
97		RFS-4-106	10	0.26	0.01	0.13
98						
99						
100						

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-4

(Page 6 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/12/08
Date Completed : 9/12/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 106 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 03N
Grid Easting : 17 + 61E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
100	End RFS-4 @ 106 feet bgs	RFS-4-106	10	0.26	0.01	0.13
101						
102						
103						
104						
105						
106						
107						
108						
109						
110						
111						
112						
113						
114						
115						
116						
117						
118						
119						
120						

RFS-4 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-5 (Page 1 of 6)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/13/08 Date Completed : 9/16/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic		Sampling Method : Continuous Total Depth : 117 Feet Logged By : Obie Strickler Grid Northing : 66 + 25N Grid Easting : 12 + 54E		
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 2.5' Medium reddish brown, oxidized surface layer	RFS-5-2.5	2.5	0.77	0.04	2.16
1						
2						
3	2.5' - 7' Boulder, only 0.5' of recovery	RFS-5-7	4.5	0.57	0.02	0.38
4						
5						
6						
7	7' - 12' Medium yellowish brown, limonite, rock chips in soil	RFS-5-12	5	0.89	0.04	0.66
8						
9						
10						
11						
12	12' - 17' Boulder	RFS-5-17	5	0.34	0.01	0.18
13						
14						
15	Master cylinder on rotating head breaks. Stop drilling. Resume drilling on 9/15/08					
16						
17	17' - 18' Medium yellowish brown to medium brown soil with rock chips	RFS-5-18	1	0.50	0.03	0.33
18	18' - 18.5' Light grey pulverized and fractured serpentine	RFS-5-18.5	0.5	0.19	0.01	0.16
19	18.5' - 20.5' Medium grey to medium brownish grey soil with rock chips	RFS-5-20.5	2	0.22	0.01	0.13
20						

RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-5

(Page 2 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/13/08
Date Completed : 9/16/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 66 + 25N
Grid Easting : 12 + 54E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20		RFS-5-20.5	2	0.22	0.01	0.13
21	20.5' - 27' Light grey pulverized and fractured serpentine					
22						
23						
24		RFS-5-27	6.5	0.19	0.01	0.13
25						
26						
27	27' - 28' Medium brown soil with rock chips	RFS-5-28	1	0.22	0.01	0.17
28	28' - 29' Light grey pulverized and fractured serpentine	RFS-5-29	1	0.20	0.01	0.12
29	29' - 30' Medium brown to medium grey soil, saprolite (?), and rock chips	RFS-5-30	1	0.20	0.01	0.14
30	30' - 31' Medium grey with some medium brown, pulverized and fractured serpentine with some saprolite (?)	RFS-5-31	1	0.23	0.01	0.16
31	31' - 32' Medium grey to medium brown soil with light bluish/greenish grey highly weathered serpentine	RFS-5-32	1	0.23	0.01	0.10
32	32' - 33' Light to medium grey pulverized and cemented serpentine	RFS-5-33	1	0.23	0.01	0.16
33	33' - 34' Light grey pulverized and fractured serpentine	RFS-5-34	1	0.23	0.01	0.18
34	34' - 35' Medium brown to medium grey soil with light bluish/greenish grey highly weathered serpentine	RFS-5-35	1	0.22	0.01	0.15
35	35' - 37' Light grey pulverized and fractured serpentine					
36		RFS-5-37	2	0.23	0.01	0.17
37	37' - 41' Medium brown soil with light bluish/greenish grey highly weathered serpentine					
38		RFS-5-41	4	0.23	0.01	0.16
39						
40						

RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-5

(Page 3 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/13/08
Date Completed : 9/16/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 66 + 25N
Grid Easting : 12 + 54E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40		RFS-5-41	4	0.23	0.01	0.16
41	41' - 41.5' Light grey pulverized and fractured serpentine	RFS-5-41.5	0.5	0.24	0.01	0.17
42	41.5' - 42' Medium bluish/greenish grey highly weathered serpentine	RFS-5-42	0.5	0.23	0.01	0.16
43	42' - 43.5' Light grey pulverized and fractured serpentines	RFS-5-43.5	1.5	0.24	0.01	0.16
44	43.5' - 44.5' Medium grey to medium bluish/greenish grey highly weathered serpentine	RFS-5-44.5	1	0.22	0.01	0.11
45	44.5' - 45.5' Light grey pulverized and fractured serpentine	RFS-5-45.5	1	0.21	0.01	0.16
46	45.5' - 46' Medium to dark brownish grey soil	RFS-5-46	0.5	0.20	0.01	0.12
47	46' - 49.5' Light grey pulverized and fractured serpentine	RFS-5-49.5	3.5	0.07	0.01	0.05
48						
49						
50	49.5' - 52' Mottled coloring (orangish brown, light to medium grey, and medium brown) soil with rock chips. Small amount of saprolite (?). Rock appears to have an orange colored rind	RFS-5-52	2.5	0.20	0.01	0.20
51						
52	52' - 52.5' Light grey pulverized and fractured serpentine	RFS-5-52.5	0.5	0.22	0.01	0.17
53	52.5' - 56' Medium brown to light grey soil with light bluish/greenish grey highly weathered serpentine	RFS-5-56	3.5	0.21	0.01	0.19
54						
55						
56	56' - 56.5' Light grey pulverized and fractured serpentine	RFS-5-56.5	0.5	0.20	0.01	0.16
57	56.5' - 57' Medium brown rind surrounding light bluish/greenish grey highly weathered serpentine	RFS-5-57	0.5	0.20	0.01	0.16
58	57' - 59' Medium brownish grey soil with rock chips	RFS-5-59	2	0.21	0.05	0.16
59	59' - 59.5' Light grey pulverized serpentine	RFS-5-59.5	0.5	0.21	0.01	0.11
60	59.5' - 60' Medium brown saprolite (?)	RFS-5-60	0.5	0.21	0.01	0.10

RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-5

(Page 4 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/13/08
Date Completed : 9/16/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 66 + 25N
Grid Easting : 12 + 54E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60	60' - 62' Light grey highly weathered serpentine	RFS-5-62	2	0.20	0.01	0.12
61						
62	62' - 67' Medium brown rind surrounding light bluish/greenish grey highly weathered serpentine with rock chips	RFS-5-67	5	0.23	0.01	0.13
63						
64						
65						
66						
67	67' - 73' Medium yellowish brown to medium brownish grey soil with rock chips	RFS-5-73	6	0.25	0.01	0.15
68						
69						
70						
71						
72						
73	73' - 77' Medium brown rind surrounding light bluish/greenish grey highly weathered serpentine	RFS-5-77	4	0.22	0.01	0.15
74						
75						
76						
77	77' - 78.5' Medium bluish/greenish grey highly weathered serpentine	RFS-5-78.5	1.5	0.19	0.01	0.15
78						
79	78.5' - 79' Medium brown rind surrounding medium bluish/greenish grey highly weathered serpentine	RFS-5-79	0.5	0.21	0.01	0.14
80	79' - 80.5' Light grey serpentine, highly weathered and pulverized	RFS-5-80.5	1.5	0.2	0.01	0.14

RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-5

(Page 5 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/13/08
Date Completed : 9/16/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 66 + 25N
Grid Easting : 12 + 54E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
80		RFS-5-80.5	1.5	0.2	0.01	0.14
81	80.5' - 81.5' Medium brown saprolite (?) with rock chips	RFS-5-81.5	1	0.19	0.01	0.15
82	81.5' - 83' Light grey pulverized and fractured serpentine, highly weathered	RFS-5-83	1	0.21	0.01	0.15
83	83' - 87' Medium brown saprolite (?) and light bluish/greenish grey highly weathered serpentine	RFS-5-86.5	1.53.5	0.19	0.01	0.15
84						
85						
86	Grab sample	RFS-5-87	0.5	0.19	0.01	0.14
87	87' - 88' Medium to dark grey pulverized and fractured serpentine (wet from advancing casing)	RFS-5-88	1	0.19	0.01	0.16
88	88' - 93' Medium yellowish brown to light bluish/greenish grey soil surrounding rock chips	RFS-5-93	5	0.19	0.01	0.16
89						
90						
91						
92						
93	93' - 94' Light grey pulverized and fractured serpentine	RFS-5-94	1	0.19	0.01	0.15
94	94' - 95' Medium brownish orange soil and saprolite (?) with rock chips	RFS-5-95	1	0.23	0.01	0.16
95	95' - 96.5' Light to medium bluish/greenish grey highly weathered serpentine	RFS-5-96.5	1.5	0.18	0.01	0.13
96						
97	96.5' - 98' Dark brown to medium bluish/greenish grey highly weathered serpentine	RFS-5-98	1.5	0.18	0.01	0.13
98	98' - 102' Medium brownish grey soil with rock chips	RFS-5-102	4	0.18	0.01	0.14
99						
100						

RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-5

(Page 6 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/13/08
Date Completed : 9/16/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 66 + 25N
Grid Easting : 12 + 54E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
100						
101		RFS-5-102	4	0.18	0.01	0.14
102	102' - 102.5' Light bluish/greenish grey highly weathered serpentine	RFS-5-102.5	0.5	0.19	0.01	0.15
103	102.5' - 109' Medium brown soil with rock chips					
104						
105						
106		RFS-5-109	6.5	0.19	0.01	0.15
107						
108						
109	109' - 110.5' Light to medium bluish/greenish grey highly weathered serpentine	RFS-5-110.5	1.5	0.17	0.01	0.13
110						
111	110.5' - 111.5' Medium brown and light grey to black saprolite (?) or consolidated serpentine	RFS-5-111.5	1	0.19	0.01	0.14
112	111.5' - 117' Light grey pulverized and fractured serpentine					
113						
114		RFS-5-117	5.5	0.19	0.01	0.17
115						
116						
117	End RFS-5 @ 117 feet bgs					
118						
119						
120						
RFS_5 was located on a skid road. No road fill, surface is red, oxidized soil						

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-6 (Page 1 of 4)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/25/08 Date Completed : 9/25/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic	Sampling Method : Continuous Total Depth : 77 Feet Logged By : Obie Strickler Grid Northing : 41 + 20N Grid Easting : 12 + 84E			
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 2' Medium to dark reddish brown, oxidized surface soil layer.	RFS-6-2	2	0.78	0.15	1.93
1	2' - 7' Medium greenish brown soil with rock chips	RFS-6-7	5	0.97	0.15	0.45
2						
3						
4						
5						
6	7' - 11' Medium yellowish brown limonite, rock chips from 7' to 8' bgs	RFS-6-11	4	1.16	0.08	0.45
7						
8						
9						
10						
11	11' - 12' Medium brown soil with light bluish grey exterior	RFS-6-12	1	0.65	0.04	0.25
12	12' - 12.5' Light grey pulverized and fractured serpentine with minor amounts of soil	RFS-6-12.5	0.5	0.70	0.03	0.19
13	12.5' - 14.5' Medium yellowish brown soil with rock chips	RFS-6-14.5	2	0.93	0.06	0.28
14	14.5' - 16.5' Light grey pulverized and fractured serpentine with minor amounts of yellowish brown soil	RFS-6-16.5	2	0.72	0.03	0.21
15						
16	16.5' - 18' Medium yellowish brown limonite intermixed with light bluish/greenish grey highly weathered serpentine	RFS-6-18	2.5	0.61	0.02	0.24
17						
18	18' - 20.5' Light grey pulverized and fractured serpentine with minor amounts of medium to dark brown soil	RFS-6-20.5	2.5	0.40	0.01	0.23
19						
20						

RFS-6 was located just off a road near trench. Red oxidized surface soil with potentially some overburden from trench located approximately 10 feet to the east.

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-6

(Page 2 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/25/08
Date Completed : 9/25/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 41 + 20N
Grid Easting : 12 + 84E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20		RFS-6-20.5	2.5	0.40	0.01	0.23
21	20.5' - 21.5' Medium orangish brown (soil/saprolite?) with rock chips	RFS-6-21.5	1	0.81	0.03	0.24
22	21.5' - 22' Medium orangish brown pulverized and fractured peridotite	RFS-6-22	0.5	0.71	0.02	0.22
22	22' - 22.5' Medium to dark brown saprolite (?) with rock chips	RFS-6-22.5	0.5	0.64	0.02	0.21
23	22.5' - 24' Medium brown to light orangish brown pulverized and fractured rock (peridotite)	RFS-6-24	1.5	0.52	0.01	0.23
24	24' - 24.5' Medium brown to light bluish/greenish grey highly weathered serpentine	RFS-6-24.5	0.5	0.43	0.01	0.15
25	24.5' - 25.5' Medium yellowish brown soil (limonite?) with very little rock	RFS-6-25.5	1	0.70	0.02	0.29
26	25.5' - 27' Medium to dark brown (saprolite ?) with layers of light bluish/greenish grey highly weathered serpentine	RFS-6-27	1.5	0.32	0.01	0.21
27	27' - 30' Medium to dark brown soil surrounding rock, small layer of light bluish/greenish grey highly weathered serpentine	RFS-6-30	3	0.32	0.01	0.21
28						
29						
30	30' - 39' Medium to dark brown and light to medium orangish brown saprolite (?) intermixed with pulverized and fractured peridotite	RFS-6-34	4	0.50	0.02	0.21
31						
32						
33						
34						
35						
36		RFS-6-39	5	0.57	0.03	0.23
37						
38						
39	39' - 41' Medium to dark brown soil with pulverized and fractured rock chips	RFS-6-41	2	0.44	0.02	0.20
40						

RFS-6 was located just off a road near trench. Red oxidized surface soil with potentially some overburden from trench located approximately 10 feet to the east.

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-6

(Page 3 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/25/08
Date Completed : 9/25/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 41 + 20N
Grid Easting : 12 + 84E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40		RFS-6-41	2	0.44	0.02	0.20
41	41' - 42' Mottled coloring (medium brown, light bluish/greenish grey, and light to medium yellowish brown) saprolite and highly weathered serpentine	RFS-6-42	1	0.34	0.01	0.20
42	42' - 43' Light grey pulverized and fractured serpentine	RFS-6-43	1	0.31	0.01	0.23
43	43' - 44.5' Light to medium yellowish brown saprolite (?)	RFS-6-44.5	1.5	0.42	0.01	0.23
44						
45	44.5' - 45.5' Light to medium bluish/greenish grey highly weathered serpentine	RFS-6-45.5	1	0.27	0.01	0.17
46	45.5' - 47' Light grey to light orangish brown soil (possibly just pulverized rock) with rock chips	RFS-6-47	1.5	0.31	0.01	0.26
47	47' - 50' Medium yellowish brown soil with rock chips. Pieces of saprolite (?) with veins of light bluish/greenish grey highly weathered serpentine	RFS-6-50	3	0.33	0.01	0.20
48						
49						
50	50' - 53.5' Light grey pulverized and fractured serpentine and light orangish brown saprolite (?) with rock chips	RFS-6-53.5	3.5	0.22	0.01	0.18
51						
52						
53						
54	53.5' - 54.5' Light grey pulverized and fractured serpentine	RFS-6-54.5	1.5	0.23	0.01	0.20
55	54.5' - 56.5' Light grey to light greyish brown soil with some saprolite (?)	RFS-6-56.5	2	0.22	0.01	0.18
56						
57	56.5' - 58' Light orangish brown to light bluish/greenish grey (saprolite?)	RFS-6-58	1.5	0.20	0.01	0.18
58	58' - 63' Light to medium grey pulverized and fractured serpentine	RFS-6-63	5	0.23	0.01	0.20
59						
60						

RFS-6 was located just off a road near trench. Red oxidized surface soil with potentially some overburden from trench located approximately 10 feet to the east.

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-6

(Page 4 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/25/08
Date Completed : 9/25/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 41 + 20N
Grid Easting : 12 + 84E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60		RFS-6-63	5	0.23	0.01	0.20
61						
62						
63	63' - 66' Alternating layers of medium to dark brown soil/saprolite (?) with light bluish/greenish grey highly weathered serpentine	RFS-6-66	3	0.23	0.01	0.24
64						
65						
66	66' - 77' Light to dark grey (based on moisture content) pulverized and fractured serpentine. At 70' bgs there is a reddish gold colored mineral within the serpentine that has hexagonal or cubic shape	No Sample	11	NA	NA	NA
67						
68						
69						
70						
71						
72						
73						
74						
75						
76						
77						
78	End RFS-6 @ 77 feet bgs					
79						
80						

RFS-6 was located just off a road near trench. Red oxidized surface soil with potentially some overburden from trench located approximately 10 feet to the east.

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-7

(Page 1 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/18/08
Date Completed : 9/18/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 77N
Grid Easting : 11 + 30E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 0.5' Medium reddish brown, oxidized surface soil	RFS-7-0.5	0.5	0.97	0.01	0.21
1	0.5' - 8' Light grey pulverized and fractured serpentine	RFS-7-8	7.5	1.26	0.03	0.45
2						
3						
4						
5						
6						
7						
8	8' - 13' Medium yellowish brown, limonite with rock chips	RFS-7-13	5	0.78	0.02	0.24
9						
10						
11						
12						
13	13' - 17' Medium yellowish brown soil, not saturated like the limonite observed from 8' to 13' bgs. Lots of rock chips	RFS-7-17	4	1.14	0.03	0.67
14						
15						
16						
17	17' - 17.5' Light grey pulverized and fractured serpentine	RFS-7-17.5	0.5	0.28	0.01	0.19
18	17.5' - 27' Medium yellowish brown with rock chips, saprolite (?). Higher percentage of rock from 17.5' to 23' bgs	RFS-7-27	9.5	0.26	0.01	0.19
19						
20						

RFS_7 was located just off a road next to Tr-14A, mostly red, oxidized surface soil with rock. Located approximately 15' from old churn drilling location

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-7

(Page 2 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/18/08
Date Completed : 9/18/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 77N
Grid Easting : 11 + 30E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20						
21						
22						
23		RFS-7-27	9.5	0.26	0.01	0.19
24						
25						
26						
27	27' - 28.5' Medium to dark grey fractured serpentine (wet)	RFS-7-28.5	1.5	0.45	0.01	0.20
28						
29	28.5' - 31' Medium brown with reddish tint soil with rock chips	RFS-7-31	2.5	0.29	0.01	0.19
30						
31	31' - 32.5' Medium to dark brown with orangish yellow tint soil with large serpentine chips	RFS-7-32.5	1.5	0.23	0.01	0.15
32						
33	32.5' - 34.5' Medium to dark grey pulverized and fractured serpentine	RFS-7-34.5	2	0.24	0.01	0.17
34						
35	34.5' - 36' Medium brown with minor amounts of orangish yellow tint. Consolidated soil with rock chips	RFS-7-36	1.5	0.23	0.01	0.19
36						
37	36' - 38.5' Light to medium grey pulverized and fractured serpentine	RFS-7-38.5	2.5	0.21	0.01	0.14
38						
39	38.5' - 39.5' Medium to dark brownish grey with some reddish orange saprolite (?) with rock chips	RFS-7-39.5	1	0.22	0.01	0.15
40	39.5' - 40.5' Medium grey pulverized serpentine (wet)	RFS-7-40.5	1	0.25	0.01	0.17

RFS_7 was located just off a road next to Tr-14A, mostly red, oxidized surface soil with rock. Located approximately 15' from old churn drilling location

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-7

(Page 3 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/18/08
Date Completed : 9/18/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 77N
Grid Easting : 11 + 30E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40		RFS-7-40.5	1	0.25	0.01	0.17
41	40.5' - 41' Medium to dark brownish grey saprolite (?)	RFS-7-41	0.5	0.25	0.01	0.18
42	41' - 49' Light grey pulverized and fractured serpentine, with pieces of solid core					
43						
44						
45		RFS-7-49	8	0.23	0.01	0.16
46						
47						
48						
49	49' - 50' Brownish orange rind surrounding light to medium grey serpentine	RFS-7-50	1	0.24	0.01	0.21
50	50' - 52' Light grey pulverized and fractured serpentine					
51		RFS-7-52	2	0.23	0.01	0.16
52	52' - 54' Light grey to medium brown saprolite (?) with rock chips					
53		RFS-7-54	2	0.21	0.01	0.14
54	54' - 66' Light grey pulverized and fractured serpentine					
55						
56						
57		RFS-7-66	12	0.20	0.01	0.11
58						
59						
60						

RFS_7 was located just off a road next to Tr-14A, mostly red, oxidized surface
soil with rock. Located approximately 15' from old churn drilling location

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-7

(Page 4 of 4)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/18/08
Date Completed : 9/18/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 77 Feet
Logged By : Obie Strickler
Grid Northing : 52 + 77N
Grid Easting : 11 + 30E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%					
60		RFS-7-66	12	0.20	0.01	0.11					
61											
62											
63											
64											
65	66' - 67' Medium brown with orange tint saprolite (?) with rock chips	RFS-7-67	1	0.22	0.01	0.12					
66											
67							67' - 77' Light grey to medium brown cemented serpentine. An unusual light bluish green mineral observed at 70.5' bgs. Very soft No sample collected from this interval	No Sample	10	NA	NA
68											
69											
70											
71											
72	End RFS-7 @ 77 feet bgs										
73											
74											
75											
76											
77											
78											
79											
80											
RFS_7 was located just off a road next to Tr-14A, mostly red, oxidized surface soil with rock. Located approximately 15' from old churn drilling location											

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-8

(Page 1 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/17/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 92 Feet
Logged By : Obie Strickler
Grid Northing : 58 + 98N
Grid Easting : 8 + 65E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 1.5' Light to medium reddish brown, oxidized surface soil layer	RFS_8_1.5	1.5	0.23	0.01	0.14
1						
2	1.5' - 5' Light grey to medium dark grey pulverized and fractured serpentine	RFS_8_5	3.5	0.77	0.06	1.29
3						
4						
5	5' - 8' Medium brownish red soil with rock chips	RFS_8_8	3	0.28	0.01	0.09
6						
7						
8	8' - 11' Medium yellowish brown, limonite	RFS_8_11	3	0.40	0.02	0.04
9						
10						
11	11' - 13' Medium brown with yellowish tinge soil with rock chips, rock from 11.5' - 11.8'	RFS_8_13	2	0.61	0.02	0.31
12						
13	13' - 17' Light grey to medium brown, serpentine chips with minor amounts of soil	RFS_8_17	4	0.65	0.02	0.19
14						
15						
16						
17	17' - 22' Medium yellowish brown, limonite, areas of rock from 18' to 18.5' and from 19.8' to 20'.	RFS_8_22	5	0.44	0.01	0.15
18						
19						
20						

RFS_8 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-8 (Page 2 of 5)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/17/08 Date Completed : 9/17/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic		Sampling Method : Continuous Total Depth : 92 Feet Logged By : Obie Strickler Grid Northing : 58 + 98N Grid Easting : 8 + 65E		
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20						
21		RFS_8_22	5	0.44	0.01	0.15
22	22' - 22.5' Light to medium grey pulverized and fractured serpentine	RFS_8_22.5	.5	1.45	0.03	0.43
23	22.5' - 27' Medium yellowish brown, limonite. Sample from 22.5' to 27 feet, however only 1' of recovery in this section. Driller indicates lack of recovery in soft material due to blocking of core barrel from serpentine boulder from 22' to 22.5'					
24		RFS_8_27	4.5	0.62	0.12	1.16
25						
26						
27	27' - 33' Light grey pulverized and fractured serpentine with brown soil.					
28						
29						
30		RFS_8_33	6	0.42	0.02	0.16
31						
32						
33	33' - 40' Medium yellowish brown, limonite. Only 4 feet of core in box. Lack of core from barrel blockage by serpentine rock from 27' to 33'.					
34						
35						
36		RFS_8_40	7	1.31	0.05	0.26
37						
38						
39						
40						
RFS_8 was located just off a road, in an open area with good oxidized red surface soil layer						

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-8

(Page 3 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/17/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 92 Feet
Logged By : Obie Strickler
Grid Northing : 58 + 98N
Grid Easting : 8 + 65E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40	40' - 43' Light bluish/greenish grey, highly weathered serpentine. Yellowish brown material from 40' to 41' most likley cross-contamination from limonite above during transfer of material from core barrel to bag.	RFS_8_43	3	1.02	0.02	0.05
41						
42						
43	43' - 44.5' Light grey pulverized and fractured serpentine	RFS_8_44.5	1.5	0.94	0.01	0.04
44	44.5' - 46' Medium reddish brown saprolite (?)	RFS_8_46	1.5	0.78	0.01	0.05
45						
46	46' - 47' Light bluish/greenish grey, highly weathered serpentine	RFS_8_47	1	0.44	0.01	0.14
47	47' - 49' Medium brown soil with pulverized and fractured serpentine. Potentially wet pulverized serpentine but normally the wet pulverized serpentine is medium to dark grey.	RFS_8_49	2	0.33	0.01	0.17
48						
49	49' - 50' Medium brown to light bluish/greenish grey saprolite? (light bluish/greenish grey material most likely highly weathered serpentine)	RFS_8_50	1	0.30	0.01	0.16
50	50' - 56' Light grey pulverized and fractured serpentine	RFS_8_56	6	0.49	0.01	0.14
51						
52						
53						
54						
55						
56						
56	56' - 57' Light bluish/greenish grey highly weathered serpentine	RFS_8_57	1	0.52	0.01	0.14
57	57' - 59.5' Medium brown soil with pulverized and fractured serpentine, wet	RFS_8_59.5	2.5	0.28	0.01	0.10
58						
59						
60	59.5' - 67' Medium brown to light bluish/greenish grey material.	RFS_8_67	7.5	0.36	0.01	0.08
RFS_8 was located just off a road, in an open area with good oxidized red surface soil layer						

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-8

(Page 4 of 5)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/17/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 92 Feet
Logged By : Obie Strickler
Grid Northing : 58 + 98N
Grid Easting : 8 + 65E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60	Potentially a mixture of saprolite (medium brown material) and highly weathered serpentine (light bluish/greenish grey material)	RFS_8_67	7.5	0.36	0.01	0.08
61						
62						
63						
64						
65	67' - 67.5' Rock chips	RFS_8_67.5	.5	0.38	0.01	0.07
66						
67						
68						
69						
70	67.5' - 68' Medium brown and light bluish/greenish grey saprolite and highly weathered serpentine	RFS_8_68	.5	0.35	0.01	0.11
71	68' - 69' Light grey pulverized and fractured serpentine	RFS_8_69	1	0.04	0.01	0.02
72	69' - 71.5' Medium brown with orange and light bluish/greenish grey saprolite and highly weathered serpentine	RFS_8_71.5	2.5	0.26	0.01	0.16
73	71.5' - 72' Light grey pulverized and fractured serpentine	RFS_8_72	.5	0.03	0.01	0.01
74	72' - 73' Medium brown to light bluish/greenish grey material, large amounts of rock	RFS_8_73	1	0.18	0.01	0.12
75	73' - 76' No recovery	No Recovery	3	NA	NA	NA
76	76' - 86' Light grey pulverized and fractured serpentine	RFS_8_86	10	0.15	0.01	0.11
77						
78						
79						
80						

RFS_8 was located just off a road, in an open area with good oxidized red surface soil layer

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-8 (Page 5 of 5)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/17/08 Date Completed : 9/17/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic		Sampling Method : Continuous Total Depth : 92 Feet Logged By : Obie Strickler Grid Northing : 58 + 98N Grid Easting : 8 + 65E		
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
80		RFS_8_86	10	0.15	0.01	0.11
81						
82						
83						
84						
85	86' - 92' Light grey pulverized and fractured serpentine, some highly weathered serpentine	RFS_8_92	6	0.21	0.01	0.11
86						
87						
88						
89						
90						
91						
92						
93	End RFS-8 at 92' bgs					
94						
95						
96						
97						
98						
99						
100						
RFS_8 was located just off a road, in an open area with good oxidized red surface soil layer						

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 1 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 1' Medium reddish brown, oxidized surface layer	RFS-9-1	1	1.01	0.03	0.36
1	1' - 7' Medium yellowish brown soil with rock chips	RFS-9-7	6	0.63	0.02	0.19
2						
3						
4						
5						
6						
7	7' - 9' Light grey pulverized and fractured serpentine	RFS-9-9	2	0.25	0.01	0.15
8						
9	9' - 15' Medium orangish brown soil with saprolite (?) and rock chips	RFS-9-15	6	0.44	0.01	0.18
10						
11						
12						
13						
14						
15	15' - 16.5' Light grey pulverized and fractured serpentine	RFS-9-16.5	1.5	0.25	0.01	0.15
16						
17	16.5' - 17' Medium yellowish brown to dark brown soil with rock chips	RFS-9-17	0.5	0.23	0.01	0.16
18	17' - 18' Dark brown to black fractured serpentine	RFS-9-18	1	0.21	0.01	0.16
19	18' - 20.5' Medium yellowish brown to light bluish grey rock chips with soil	RFS-9-20.5	2.5	0.24	0.01	0.15
20						

RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 2 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20		RFS-9-20.5	2.5	0.24	0.01	0.15
21	20.5' - 21.5' Light grey pulverized and fractured serpentine	RFS-9-21.5	1	0.20	0.01	0.16
22	21.5' - 23' Medium brown soil with rock chips	RFS-9-23	1.5	0.38	0.01	0.16
23	23' - 24' Light grey pulverized and fractured serpentine	RFS-9-24	1	0.21	0.01	0.14
24	24' - 27' Medium yellowish brown soil, saprolite (?) and rock chips	RFS-9-27	3	0.20	0.01	0.14
25						
26						
27	27' - 27.5' Light grey pulverized and fractured serpentine	RFS-9-27.5	0.5	0.44	0.01	0.19
28	27.5' - 28' Medium brown with orange saprolite (?)	RFS-9-28	0.5	0.43	0.01	0.21
29	28' - 32' Medium yellowish brown soil, large amounts of rock	RFS-9-32	4	0.29	0.01	0.18
30						
31						
32	32' - 32.5' Light bluish/greenish grey highly weathered serpentine	RFS-9-32.5	0.5	0.19	0.01	0.15
33	32.5' - 33' Medium brown with orange soil and rock	RFS-9-33	0.5	0.20	0.01	0.15
34	33' - 35' Light grey pulverized and fractured serpentine	RFS-9-35	2	0.20	0.01	0.17
35	35' - 37' Medium to dark brown soil with rock chips	RFS-9-37	2	0.22	0.01	0.15
36						
37	37' - 42.5' Medium yellowish brown soil rind around fractured serpentine	RFS-9-42.5	5.5	0.23	0.01	0.15
38						
39						
40						

RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 3 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
40						
41		RFS-9-42.5	5.5	0.23	0.01	0.15
42						
43	42.5' - 47' Medium yellowish brown soil with rock chips					
44						
45		RFS-9-47	4.5	0.22	0.01	0.14
46						
47	47' - 48.5' Medium yellowish brown soil surrounding rock and light bluish/greenish grey highly weathered serpentine	RFS-9-48.5	1.5	0.20	0.01	0.15
48						
49	48.5' - 49' Medium bluish/greenish grey highly weathered serpentine	RFS-9-49	0.5	0.19	0.01	0.14
50	49' - 50' Medium to dark brown soil with large amounts of fractured rock	RFS-9-50	1	0.20	0.01	0.15
51	50' - 51' Medium yellowish brown soil with large amounts of fractured rock	RFS-9-51	1	0.21	0.01	0.16
52	51' - 53' Medium brown surface rind over light bluish/greenish grey highly weathered serpentine	RFS-9-53	2	0.18	0.01	0.15
53						
54	53' - 54' Medium brown soil/saprolite (?) with rock chips	RFS-9-54	1	0.21	0.01	0.16
55	54' - 55' Light grey pulverized and fractured serpentine	RFS-9-55	1	0.20	0.01	0.16
56	55' - 57' Light bluish/greenish grey highly weathered serpentine with rock chips	RFS-9-57	2	0.19	0.01	0.15
57						
58	57' - 60' Medium brown to dark grey and light orangish brown soil, saprolite (?) and rock chips	RFS-9-60	3	0.21	0.01	0.14
59						
60						

RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 4 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.net

Date Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : Sonic

Sampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
60	60' - 63' Medium brown saprolite (?) with small amount of fractured serpentine	RFS-9-63	3	0.21	0.01	0.14
61						
62						
63	63' - 65' Light grey pulverized and fractured serpentine	RFS-9-65	2	0.20	0.01	0.13
64						
65	65' - 66' Light bluish grey highly weathered serpentine	RFS-9-66	1	0.21	0.01	0.14
66	66' - 69' Medium brown to orangish yellow soil with rock chips	RFS-9-69	3	0.16	0.01	0.11
67						
68						
69	69' - 69.5' Light grey pulverized and fractured serpentine	RFS-9-69.5	0.5	0.02	0.01	0.02
70	69.5' - 70' Medium brown saprolite (?) with rock chips	RFS-9-70	0.5	0.02	0.01	0.02
71	70' - 73' Light grey pulverized and fractured serpentine	RFS-9-73	3	0.17	0.01	0.10
72						
73						
74	73' - 74.5' Medium to dark grey saturated soil with rock	RFS-9-74.5	1.5	0.02	0.01	0.02
75	74.5' - 76.5' Medium grey to light orangish yellow with very hard exterior, saprolite (?)	RFS-9-76.5	2	0.14	0.01	0.08
76						
77	76.5' - 78' Light grey to medium brown consolidated serpentine	RFS-9-78	1.5	0.21	0.01	0.15
78	78' - 84' Medium brown to medium dark grey saprolite (?) or possibly consolidated serpentine	RFS-9-84	6	0.20	0.01	0.12
79						
80						

RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 5 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
80						
81						
82		RFS-9-84	6	0.20	0.01	0.12
83						
84	84' - 86' Medium brown rind around light bluish/greenish grey highly weathered serpentine	RFS-9-86	2	0.22	0.01	0.17
85						
86	86' - 88' Medium brown soil with pulverized and fractured serpentine	RFS-9-88	2	0.23	0.01	0.19
87						
88	88' - 93' Medium brown with orange saprolite (?) and soil with rock chips. Light bluish/greenish grey highly weathered serpentine from 89' to 89.5' bgs	RFS-9-93	5	0.21	0.01	0.16
89						
90						
91						
92						
93	93' - 95.5' Light grey pulverized and fractured serpentine. Minor amounts of medium brown soil rind around rock	RFS-9-95.5	2.5	0.20	0.01	0.14
94						
95						
96	95.5' - 96.5' Medium brown saprolite (?) with fractured serpentine chips	RFS-9-96.5	1	0.20	0.01	0.12
97	96.5' - 99.5' Light grey pulverized serpentine (dry) and medium brownish grey pulverized and fractured serpentine (wet)	RFS-9-99.5	3	0.21	0.01	0.17
98						
99						
100	99.5' - 101' Medium brown with orange saprolite (?) with rock chips	RFS-9-101	1.5	0.20	0.01	0.14

RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-9

(Page 6 of 6)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/16/08
Date Completed : 9/17/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 117 Feet
Logged By : Obie Strickler
Grid Northing : 74 + 99N
Grid Easting : 6 + 07E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
100		RFS-9-101	1.5	0.20	0.01	0.14
101	101' - 104.5' Light grey pulverized and fractured serpentine					
102		RFS-9-104.5	3.5	0.21	0.01	0.13
103						
104						
105	104.5' - 105.5' Medium brown with orange saprolite (?) with rock chips	RFS-9-105.5	1	0.19	0.01	0.13
106	105.5' - 106' Medium brownish grey pulverized and fractured serpentine (wet)	RFS-9-106	0.5	0.20	0.01	0.14
107	106' - 106.5' Medium brown with orange saprolite (?) and fractured serpentine	RFS-9-106.5	0.5	0.19	0.01	0.13
108	106.5' - 111' Light grey to medium brown pulverized and fractured serpentine					
109		RFS-9-111	4.5	0.20	0.01	0.16
110						
111	111' - 111.5' Medium to dark brown saprolite (?) with fractured serpentine	RFS-9-111.5	0.5	0.19	0.01	0.15
112	111.5' - 117' Light grey to medium brown pulverized serpentine					
113		RFS-9-117	5.5	0.19	0.01	0.14
114						
115						
116						
117	End RFS-9 @ 117 feet bgs					
118						
119						
120						
RFS_9 was located just off a road with an equal mixture of red, oxidized surface soil and rock						

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-10 (Page 1 of 3)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/10/08 Date Completed : 9/10/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic	Sampling Method : Continuous Total Depth : 53 Feet Logged By : Obie Strickler Grid Northing : 32 + 40N Grid Easting : 28 + 09E			
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0 1 2 3 4	0' - 4' Medium reddish brown, oxidized surface layer	RFS_10_4	4	0.38	0.04	0.63
4 5 6 7 8 9 10 11 12	4' - 12' Light grey pulverized and fractured serpentine	RFS_10_12	8	0.25	0.01	0.17
12 13 14 15 16 17	12' - 17' Light brown, mixed soil and fractured serpentine	RFS_10_17	5	0.21	0.01	0.15
17 18 19 20	17' - 22' Light brown, mixed soil and fractured serpentine small boulder from 21' bgs to 21.3' bgs	RFS_10_22	5	0.21	0.01	0.12

RFS-10 was located just off a road with limited amounts of red, oxidized surface soil

Red Flat Nickel Corp. Red Flat Nickel Deposit Curry County, Oregon		LOG OF BORING RFS-10 (Page 2 of 3)				
LithoLogic Resources, LLC Michael D. Strickler, RG geomania@hughes.net		Date Started : 9/10/08 Date Completed : 9/10/08 Boring Diameter : 4" Drilling Contractor : Boart Longyear Drilling Method : Sonic		Sampling Method : Continuous Total Depth : 53 Feet Logged By : Obie Strickler Grid Northing : 32 + 40N Grid Easting : 28 + 09E		
Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
20						
21		RFS_10_22	5	0.21	0.01	0.12
22	22' - 27' Light brown mixed soil with fractured serpentine					
23						
24		RFS_10_27	5	0.28	0.01	0.16
25						
26						
27	27' - 32' Medium brown soil with fractured serpentine					
28						
29		RFS_10_32	5	0.41	0.01	0.18
30						
31						
32	32' - 35' Light grey pulverized and fractured serpentine with solid serpentine core					
33		RFS_10_35	3	0.19	0.01	0.15
34						
35	35' - 40' Light to medium brown soil with blue and black serpentine fragments					
36						
37		RFS_10_40	5	0.33	0.01	0.16
38						
39						
40						
RFS-10 was located just off a road with limited amounts of red, oxidized surface soil						

[illegible]

Red Flat Nickel Corp.

Red Flat Nickel Deposit
Curry County, Oregon

LOG OF BORING RFS-11

(Page 1 of 2)

LithoLogic Resources, LLC
Michael D. Strickler, RG
geomania@hughes.netDate Started : 9/23/08
Date Completed : 9/23/08
Boring Diameter : 4"
Drilling Contractor : Boart Longyear
Drilling Method : SonicSampling Method : Continuous
Total Depth : 27 Feet
Logged By : Obie Strickler
Grid Northing : 63 + 21N
Grid Easting : 6 + 96E

Depth in Feet	DESCRIPTION	Sample ID	Sample Interval (Feet)	Ni%	Co%	Cr%
0	0' - 2' Medium reddish brown to medium yellowish brown surface layer. Oxidized to approximately 1' bgs	Hold Sample				
1						
2	2' - 9' Light grey pulverized and fractured serpentine. Wet pulverized serpentine from drillers water from 7' to 8.5' bgs	Hold Sample				
3						
4						
5						
6						
7						
8						
9	9' - 10' Medium yellowish brown soil with fractured serpentine	Hold Sample				
10	10' - 27' Light grey (dry) to medium grey (wet) pulverized and fractured serpentine	Hold Sample				
11						
12						
13						
14						
15						
16						
17						
18						
19						
20						

Red Flat Nickel Corp.

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LOG OF BORING RFS-11

(Page 2 of 2)

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Logged By : Obie Strickler
Grid Northing : 63 + 21N
Grid Easting : 6 + 96E

Depth in Feet

DESCRIPTION

Sample ID

Sample Interval (Feet)

Ni%

Co%

Cr%

20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40

End boring @ 27' bgs

Hold Sample

Red Flat: Trench #1

Analytical Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_A_1_1	0.795	0.071	1.660	36.10	3.31	Surface/Oxidized Layer	SANDY CLAY (ML), medium to dark reddish brown, 75-80% fines, 15-20% fine sand, <10% gravel to cobble, dry, non-plastic, low density, organics.
RF_A_1_2	1.260	0.075	1.800	42.00	2.09	Limonite	GRAVELLY CLAY (ML), medium to dark reddish brown, 60-70% fines, 10-15% fine sand, 30-35% gravel and cobble >2", dry, non-plastic, low density.
RF_A_1_3	1.230	0.104	1.640	36.00	4.79	Limonite	GRAVELLY CLAY (ML), light to medium yellowish brown, 60-70% fines, <10% fine sand, 30-40% gravel and cobble >2", dry, non-plastic, low to medium density.
RF_A_1_4	1.150	0.062	0.864	24.90	9.88	Limonite	GRAVELLY CLAY (ML), light to medium yellowish brown, 60-70% fines, 10-15% fine sand, 30-35% gravel and cobble (serpentine) >2", dry to damp, low plasticity, medium density.
RF_A_1_5	1.060	0.046	0.695	22.80	10.95	Limonite	GRAVELLY CLAY (ML), medium yellowish brown, 60-70% fines, 10-15% fine sand, 30-35% gravel and cobble (serpentine) >2", damp, low plasticity, medium density.
RF_A_1_6	1.080	0.053	0.819	25.80	9.91	Limonite	GRAVELLY CLAY (ML), medium yellowish brown, 50-60% fines, <10% fine sand, 40-50% gravel and cobble >2", damp, low plasticity, medium density. Increase in weathered serpentine.
RF_A_1_7	1.140	0.047	0.958	21.80	11.20	Limonite/Rock	CLAYEY GRAVEL (GC), medium to dark brown, 40-50% fines, <10% fine sand, 50-60% gravel and cobble (serpentine), damp to wet, low plasticity, medium to high density.
RF_A_1_8	0.917	0.028	0.462	13.75	16.00	Limonite/Rock	CLAYEY GRAVEL (GC), medium to dark brown, 20-30% fines, <10% fine sand, 70-80% gravel and cobble (serpentine), damp to wet, low plasticity, high density.
RF_A_1_12	0.629	0.022	0.380	11.10	17.90	Limonite/Rock	SERPENTINE, dark green to black, <10% fines, >90% angular serpentine fragments. Fines most likely in-fall.
Average	1.029	0.056	1.031	26.03	9.56		

Corestone Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_CSR_1	0.776	0.024	0.411	12.00	16.75	Rind	Sample collected from ~ 9-12' bgs, not very thick <0.5", not completely weathered. No rind observed in upper portions of trench.
RF_CSC_1	0.276	0.011	0.131	5.72	22.00	Core	Composite sample from excavated rock, all serpentine.

Red Flat: Trench #2

Analytical Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_A_2_1	0.950	0.049	0.806	25.100	6.530	Surface/Oxidized Layer	CLAYEY GRAVEL (GC), medium to dark reddish brown, 35-40% fines, 60-65% gravel, dry, non-plastic, low to medium density.
RF_A_2_2	0.783	0.024	0.401	12.300	16.900	Limonite/Rock	CLAYEY GRAVEL (GC), medium to dark reddish brown, 20-30% fines, 70-80% gravel and boulder (serpentine), dry, non-plastic, low to medium density.
RF_A_2_3	0.853	0.020	0.296	11.900	16.850	Serpentine	SERPENTINE, 80-90% rock, 10-20% fines interspersed within the rock, highly fractured, very little weathering.
RF_A_2_4	0.457	0.024	0.410	14.600	12.750	Serpentine	SERPENTINE, 80-90% rock, 10-20% fines interspersed within the rock, highly fractured, very little weathering.
RF_A_2_5	0.605	0.017	0.244	9.830	16.100	Serpentine	SERPENTINE, >90% rock, <10% fines interspersed within the rock, highly fractured, medium weathering. Fines most likely in-fall.
RF_A_2_6	0.521	0.015	0.213	9.300	17.200	Serpentine	SERPENTINE, >90% rock, <10% fines interspersed within the rock, highly fractured, highly weathered. Fines most likely in-fall.
RF_A_2_7	0.288	0.014	0.206	8.790	16.750	Serpentine	SERPENTINE, >90% rock, <10% fines interspersed within the rock, highly fractured, highly weathered. Fines most likely in-fall.
RF_A_2_8	0.283	0.014	0.206	8.830	17.150	Serpentine	SERPENTINE, >90% rock, <10% fines interspersed within the rock, highly fractured, highly weathered. Fines most likely in-fall.
Average	0.593	0.022	0.348	12.581	15.029		

Corestone Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_CSR_2_6	0.446	0.018	0.266	11.900	14.100	Rind	Rind collected from partially weathered serpentine, very granular
RF_CSC_2	0.294	0.011	0.180	5.960	20.200	Core	Composite collected from soil stockpile

Red Flat: Trench #3

Analytical Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_A_3_1	0.270	0.038	1.210	28.60	2.99	Oxidized Surface Layer	SANDY SILT (ML), dark reddish brown, 65-75% fines, 15-20% fine sand, 5-15% gravel <0.1' diameter, dry, non-plastic, low density.
RF_A_3_2	0.745	0.029	1.840	46.40	1.09	Limonite	SANDY SILT (ML), medium yellowish brown, 80-90% fines, 10-20% fine sand, dry, low plasticity, low density.
RF_A_3_3	0.815	0.045	1.830	47.90	0.92	Limonite	SANDY CLAY (ML), medium yellowish brown, 80-90% fines, 10-20% fine sand, dry, low plasticity, low density.
RF_A_3_4	0.821	0.098	1.910	44.30	1.07	Limonite	SANDY CLAY (ML), medium yellowish brown, 85-90% fines, 10-15% fine sand, dry, low plasticity, low density.
RF_A_3_5	0.710	0.180	1.110	39.90	2.07	Limonite/ Saprolite	SANDY CLAY (ML), medium yellowish brown, 85-90% fines, 10-15% fine sand, dry, low plasticity, low density.
RF_A_3_6	0.782	0.199	1.070	40.00	2.17	Limonite/ Saprolite	SANDY CLAY (CL), medium brown, 85-90% fines, 10-15% fine sand, dry to damp, low to medium plasticity, low density.
RF_A_3_7	1.010	0.176	1.470	43.60	2.06	Saprolite	SANDY CLAY (CL), medium brown, 85-90% fines, 10-15% fine sand, dry to damp, low to medium plasticity, low density. Observable saprolitic structures.
RF_A_3_8	0.765	0.125	0.968	34.80	5.04	Saprolite	SANDY CLAY (CL), medium brown, 80-90% fines, 10-20% fine sand, dry to damp, low to medium plasticity, low density.
RF_A_3_9	0.736	0.128	0.870	30.90	5.48	Saprolite	SANDY CLAY (CL), medium brown, 80-90% fines, 10-20% fine sand, dry to damp, medium plasticity, low density.
RF_A_3_10	0.882	0.126	0.894	32.20	4.51	Saprolite	SANDY CLAY (CL), medium brown, 80-90% fines, 10-20% fine sand, damp, medium plasticity, low density.
RF_A_3_11	0.919	0.105	0.883	32.50	4.02	Saprolite	SANDY CLAY (CL), light to medium yellowish brown, 85-90% fines, 10-15% fine sand, damp, medium plasticity, low density.
RF_A_3_12	1.020	0.086	0.823	29.10	4.76	Saprolite	SANDY CLAY (CL), light to medium yellowish brown, 85-90% fines, 10-15% fine sand, damp to wet, medium plasticity, low density. Visible structure in saprolite increases.
RF_A_3_13	1.010	0.078	0.875	29.90	4.53	Saprolite	SANDY CLAY (CL), medium yellowish brown, 85-90% fines, 10-15% fine sand, damp to wet, medium plasticity, low density. Saprolitic structures with fractures and veins.
RF_A_3_14	0.979	0.086	0.820	29.00	6.29	Saprolite	SANDY CLAY (CL), medium to dark yellowish brown, 85-90% fines, 10-15% fine sand, damp to wet, medium plasticity, low density.
RF_A_3_15	1.020	0.075	1.050	27.20	7.00	Saprolite	SANDY CLAY (CL), light to medium yellowish brown, 85-90% fines, 10-15% fine sand, wet, medium plasticity, low density.

Red Flat: Trench #3

Analytical Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_A_3_21	1.440	0.066	0.628	24.80	7.08	Saprolite	SANDY CLAY (CL), light to medium yellowish brown, 70-80% fines, 10-20% fine sand, 10-20% gravel, wet, medium to high plasticity, low to medium density. Composite sample collected from 15 to 21'; large rock content increases significantly below 18'.
Average	0.870	0.103	1.141	35.07	3.82		

Corestone Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_CSR_3_12	1.650	0.042	0.329	12.900	12.850	Rind	Yellowish rind observed around serpentine boulder.
RF_CSC_3	0.821	0.018	0.194	7.110	19.550	Core	Composite corestone sample from trench stockpile.

Red Flat: Trench #4

Analytical Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_A_4_1	1.030	0.086	2.820	>50	0.640	Oxidized/Surface Layer	SANDY CLAY (ML), medium reddish brown, 85-90% fines, 10-15% fine sand, dry, non-plastic, medium dense.
RF_A_4_2	1.250	0.220	2.070	39.900	4.530	Limonite	SANDY CLAY (ML), medium reddish brown, 85-90% fines, 10-15% fine sand, dry, non-plastic, medium dense.
RF_A_4_3	1.570	0.187	0.749	28.100	7.080	Limonite	SANDY CLAY (ML), medium yellowish brown, 80-90% fines, 10-15% fine sand, gravel <5%, damp, low plasticity, low to medium density.
RF_A_4_4	1.750	0.166	0.795	28.400	6.790	Limonite	SANDY CLAY (ML), medium to dark reddish brown, 85-90% fines, 10-15% fine sand, <5% gravel (fragments from larger rocks), damp, low plasticity, low density.
RF_A_4_5	1.320	0.150	0.610	20.800	11.800	Saprolite	SANDY CLAY (CL), medium yellowish/reddish brown, 85-90% fines, 10-15% fine sand, <5% gravel, damp, low to medium plasticity, low to medium density. Visible saprolitic structures.
RF_A_4_6	1.660	0.179	1.030	29.500	7.190	Saprolite	SANDY CLAY (CL), medium yellowish brown, 85-90% fines, 10-15% fine sand, damp to wet, medium plasticity, low density.
RF_A_4_7	1.480	0.156	0.825	20.700	11.350	Saprolite	SANDY CLAY (CL), medium yellowish brown, 80-90% fines, 10-20% fine sand, wet, medium plasticity, low density.
RF_A_4_11	0.387	0.011	0.147	5.030	22.300	Bedrock	Serpentine bedrock, composite sample collected from 8 to 11' bgs. Bedrock encountered at ~ 7.5' bgs, 2 more holes excavated both encounter bedrock at ~ 7.5' bgs.
Average	1.306	0.144	1.131	24.633	8.960		

Corestone Samples	Ni%	Co%	Cr%	Fe%	Mg%	Horizon	Description
RF_CSR_4	1.580	0.200	0.421	15.600	13.050	Rind	Composite rind sample from rock within trench.
RF_CSC_4	1.375	0.081	0.150	6.270	20.000	Core	Composite core sample from excavated rock and rock in trench.

ADDITIONAL PHOTOGRAPHS



Density sample – trench no. 1, 4 ft



Density sample – trench no. 1, 9 ft (the sand is used to measure the volume)



Excavator digging – trench no. 1



Limonitic horizon – trench no. 1



Trench no. 1 outline



Saproplitic horizon –trench no. 1



Rocks and soils –trench no. 2



Rock pile at trench no.2



Trench no.2 outline



Density sample –trench no.3, 7ft



Density sample –trench no. 3, 16 ft



Channel sample – trench no.3



Typical saprolite – trench no. 3



Trench no. 3 outline



Density sample location – trench no. 4



Density sample – trench no. 4, 4 ft



Typical saprolite horizon –trench no. 4



Excavated soil and rocks from trench no.4



Soil profile in trench no. 4

APPENDIX C
KRIGING BLOCK RESULTS

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3890136	273758	0.38	0.0119	6.3
3890143	274058	0.44	0.0194	6.99
3890150	274358	0.5	0.0259	7.39
3890157	274657	0.55	0.0293	7.64
3890164	274957	0.57	0.0309	7.81
3890170	275257	0.56	0.0316	7.6
3890177	275557	0.55	0.0322	7.67
3890184	275857	0.56	0.0331	7.57
3890436	273751	0.37	0.0116	6.85
3890443	274051	0.42	0.0189	7.29
3890450	274351	0.49	0.0257	7.59
3890457	274651	0.54	0.0293	7.78
3890463	274951	0.57	0.0303	7.91
3890470	275250	0.57	0.0303	8
3890477	275550	0.56	0.0316	7.73
3890484	275850	0.55	0.0322	7.78
3890736	273744	0.44	0.0127	7.41
3890743	274044	0.45	0.0195	7.68
3890750	274344	0.5	0.0259	7.86
3890757	274644	0.54	0.0294	7.98
3890763	274944	0.57	0.0303	8.05
3890770	275244	0.57	0.0303	8.11
3890777	275544	0.57	0.0303	8.15
3890784	275844	0.56	0.0316	7.83
3891036	273737	0.54	0.0122	7.86
3891043	274037	0.51	0.0192	8.06
3891050	274337	0.52	0.0258	8.15
3891056	274637	0.55	0.0294	8.19
3891063	274937	0.57	0.0303	8.21
3891070	275237	0.57	0.0303	8.23
3891077	275537	0.57	0.0303	8.24
3891084	275837	0.59	0.0296	7.83
3891336	273730	0.61	0.0102	8.48
3891343	274030	0.56	0.0180	8.49
3891350	274330	0.55	0.0253	8.43
3891356	274630	0.55	0.0293	8.39
3891363	274930	0.57	0.0303	8.36
3891370	275230	0.59	0.0301	8.65
3891377	275530	0.6	0.0295	8.22
3891384	275830	0.6	0.0295	8.21
3891636	273724	0.66	0.0098	9.33
3891643	274024	0.6	0.0174	9.11
3891650	274324	0.57	0.0249	8.99
3891656	274623	0.57	0.0291	8.95
3891663	274923	0.61	0.0297	8.87
3891670	275223	0.61	0.0298	8.85
3891677	275523	0.6	0.0297	8.33
3891684	275823	0.58	0.0290	8.54
3891936	273717	0.69	0.0101	9.29
3891943	274017	0.63	0.0174	9.23
3891949	274317	0.6	0.0251	9.15

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3891956	274617	0.66	0.0291	9.15
3891963	274917	0.63	0.0299	8.95
3891970	275216	0.64	0.0300	9.01
3891977	275516	0.62	0.0295	8.47
3891983	275816	0.63	0.0287	8.63
3891990	276116	0.65	0.0287	9.48
3891997	276416	0.67	0.0305	10.42
3892004	276716	0.66	0.0309	10.7
3892011	277016	0.75	0.0311	10.38
3892017	277316	0.75	0.0314	10.01
3892236	273710	0.68	0.0104	9.33
3892243	274010	0.66	0.0177	9.36
3892249	274310	0.64	0.0250	8.95
3892256	274610	0.63	0.0293	8.86
3892263	274910	0.6	0.0300	8.64
3892270	275210	0.59	0.0301	8.64
3892277	275510	0.61	0.0292	8.56
3892283	275810	0.67	0.0292	8.97
3892290	276109	0.68	0.0304	9.8
3892297	276409	0.67	0.0305	10.44
3892304	276709	0.7	0.0317	10.94
3892311	277009	0.75	0.0311	10.39
3892317	277309	0.75	0.0314	10.01
3892536	273703	0.64	0.0114	9.41
3892542	274003	0.64	0.0179	9.16
3892549	274303	0.64	0.0247	9.04
3892556	274603	0.61	0.0289	8.7
3892563	274903	0.61	0.0305	8.62
3892570	275203	0.59	0.0298	8.45
3892577	275503	0.67	0.0299	8.75
3892583	275803	0.68	0.0307	9.32
3892590	276103	0.68	0.0307	10.35
3892597	276403	0.67	0.0305	10.48
3892604	276702	0.7	0.0317	10.95
3892611	277002	0.77	0.0317	10.52
3892617	277302	0.75	0.0314	10.01
3892836	273696	0.61	0.0110	8.93
3892842	273996	0.62	0.0163	8.63
3892849	274296	0.64	0.0223	8.34
3892856	274596	0.62	0.0267	8.25
3892863	274896	0.63	0.0291	7.92
3892870	275196	0.59	0.0300	8.15
3892876	275496	0.69	0.0310	8.82
3892883	275796	0.72	0.0312	9.68
3892890	276096	0.69	0.0308	10.51
3892897	276396	0.66	0.0311	10.79
3892904	276696	0.7	0.0317	10.97
3892910	276996	0.77	0.0317	10.54
3892917	277296	0.78	0.0314	10.65
3893136	273690	0.58	0.0090	8.49
3893142	273990	0.59	0.0118	8.51

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3893149	274289	0.61	0.0169	8.27
3893156	274589	0.62	0.0214	7.99
3893163	274889	0.62	0.0255	8.05
3893170	275189	0.62	0.0287	8.51
3893176	275489	0.68	0.0302	8.79
3893183	275789	0.71	0.0305	9.73
3893190	276089	0.69	0.0302	10.57
3893197	276389	0.69	0.0310	11.2
3893204	276689	0.7	0.0309	11.01
3893210	276989	0.76	0.0309	10.57
3893217	277289	0.75	0.0305	10.62
3893224	277589	0.75	0.0307	10
3893231	277889	0.65	0.0304	9.29
3893238	278188	0.63	0.0303	9.32
3893244	278488	0.62	0.0298	8.96
3893251	278788	0.63	0.0284	9.12
3893258	279088	0.65	0.0282	8.94
3893265	279388	0.67	0.0277	8.74
3893272	279688	0.68	0.0254	8.83
3893278	279988	0.75	0.0208	8.49
3893285	280288	0.83	0.0160	7.29
3893435	273683	0.58	0.0083	8.46
3893442	273983	0.6	0.0084	8.57
3893449	274283	0.63	0.0106	7.69
3893456	274583	0.64	0.0134	7.67
3893463	274883	0.63	0.0186	7.92
3893469	275182	0.61	0.0233	8.25
3893476	275482	0.66	0.0260	8.94
3893483	275782	0.69	0.0271	9.84
3893490	276082	0.69	0.0277	11.1
3893497	276382	0.75	0.0281	11.93
3893503	276682	0.72	0.0280	11.73
3893510	276982	0.71	0.0278	10.76
3893517	277282	0.75	0.0277	10.37
3893524	277582	0.64	0.0272	9.74
3893531	277882	0.65	0.0268	9.73
3893538	278182	0.63	0.0255	9.25
3893544	278482	0.68	0.0241	9.34
3893551	278782	0.64	0.0233	9.2
3893558	279081	0.66	0.0223	9.15
3893565	279381	0.68	0.0226	9.08
3893572	279681	0.71	0.0216	8.62
3893578	279981	0.76	0.0179	8.38
3893585	280281	0.79	0.0134	7.8
3893735	273676	0.6	0.0088	8.65
3893742	273976	0.63	0.0080	7.92
3893749	274276	0.66	0.0077	7.87
3893756	274576	0.66	0.0085	7.76
3893763	274876	0.62	0.0115	8.03
3893769	275176	0.58	0.0163	8.51
3893776	275476	0.62	0.0190	9.26

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3893783	275775	0.66	0.0202	10.53
3893790	276075	0.74	0.0205	11.5
3893797	276375	0.8	0.0203	12.02
3893803	276675	0.77	0.0201	11.85
3893810	276975	0.71	0.0198	10.83
3893817	277275	0.68	0.0196	10.24
3893824	277575	0.61	0.0192	9.66
3893831	277875	0.64	0.0187	9.63
3893837	278175	0.66	0.0173	9.25
3893844	278475	0.68	0.0147	9.43
3893851	278775	0.65	0.0140	9.29
3893858	279075	0.62	0.0135	9.17
3893865	279375	0.64	0.0150	9.19
3893871	279674	0.67	0.0162	8.73
3893878	279974	0.7	0.0158	8.67
3893885	280274	0.73	0.0139	8.61
3893960	283573	0.38	0.0138	4.03
3893967	283873	0.3	0.0097	3.97
3893974	284173	0.26	0.0085	4.87
3893980	284473	0.23	0.0091	4.89
3893987	284773	0.21	0.0120	4.95
3893994	285073	0.22	0.0131	4.77
3894001	285373	0.22	0.0101	4.63
3894008	285673	0.17	0.0092	4.9
3894014	285973	0.12	0.0081	5.61
3894021	286273	0.1	0.0096	5.58
3894035	273669	0.65	0.0094	8.83
3894042	273969	0.68	0.0090	8.23
3894049	274269	0.73	0.0078	8.6
3894056	274569	0.73	0.0074	8.2
3894063	274869	0.67	0.0080	8.26
3894069	275169	0.6	0.0099	8.28
3894076	275469	0.59	0.0111	9.38
3894083	275769	0.65	0.0113	10.15
3894090	276069	0.76	0.0112	10.96
3894097	276369	0.88	0.0110	12.46
3894103	276668	0.84	0.0109	12.22
3894110	276968	0.73	0.0107	11.61
3894117	277268	0.61	0.0106	9.21
3894124	277568	0.6	0.0104	9.64
3894131	277868	0.65	0.0101	9.11
3894137	278168	0.71	0.0095	8.89
3894144	278468	0.68	0.0083	11
3894151	278768	0.65	0.0081	9.56
3894158	279068	0.64	0.0079	10
3894165	279368	0.64	0.0086	9.01
3894171	279668	0.63	0.0100	8.59
3894178	279968	0.65	0.0123	9.01
3894185	280268	0.68	0.0121	9.17
3894219	268564	0.49	0.0206	9.06
3894226	268864	0.46	0.0122	6.27

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate Ni (%)	Variance Ni (%) ²	the block (ft)
3894233	269164	0.44	0.0106	8.81
3894240	269463	0.48	0.0147	8.42
3894247	269763	0.51	0.0155	10.2
3894254	270063	0.56	0.0116	11.65
3894260	283567	0.4	0.0099	3.8
3894260	270363	0.64	0.0111	11.2
3894267	283867	0.33	0.0081	4.06
3894267	270663	0.71	0.0091	10.46
3894273	284167	0.27	0.0075	4.47
3894274	270963	0.81	0.0082	10.77
3894280	284466	0.23	0.0076	5.13
3894281	271263	0.9	0.0081	10.7
3894287	284766	0.22	0.0083	5.32
3894288	271563	0.93	0.0080	10.98
3894294	285066	0.25	0.0099	4.75
3894294	271863	0.87	0.0073	11.55
3894301	285366	0.26	0.0094	4.61
3894301	272163	0.85	0.0072	11.4
3894308	285666	0.22	0.0084	4.65
3894308	272463	0.76	0.0078	10.49
3894314	285966	0.14	0.0085	5.77
3894315	272763	0.67	0.0079	10.32
3894321	286266	0.09	0.0091	6.12
3894322	273063	0.6	0.0080	9.65
3894328	273362	0.63	0.0088	9.69
3894335	273662	0.67	0.0083	9.45
3894342	273962	0.74	0.0086	9.28
3894349	274262	0.79	0.0077	9.37
3894356	274562	0.81	0.0073	8.62
3894362	274862	0.76	0.0073	8.33
3894369	275162	0.68	0.0075	8.22
3894376	275462	0.65	0.0076	9.42
3894383	275762	0.68	0.0076	10.72
3894390	276062	0.8	0.0076	11.72
3894396	276362	0.93	0.0075	13.36
3894403	276662	0.89	0.0075	12.37
3894410	276962	0.78	0.0075	10.69
3894417	277261	0.63	0.0075	10.34
3894424	277561	0.63	0.0074	8.96
3894430	277861	0.72	0.0074	9.18
3894437	278161	0.76	0.0074	8.57
3894444	278461	0.69	0.0073	8.74
3894451	278761	0.61	0.0072	9.8
3894458	279061	0.61	0.0072	10.46
3894465	279361	0.62	0.0073	9.9
3894471	279661	0.62	0.0076	9.15
3894478	279961	0.66	0.0083	8.49
3894485	280261	0.68	0.0084	10.68
3894492	280561	0.73	0.0076	11.95
3894499	280861	0.73	0.0073	11.89
3894505	281160	0.67	0.0089	10.79

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3894512	281460	0.66	0.0167	9.71
3894519	281760	0.67	0.0260	9.5
3894519	268557	0.47	0.0194	9.49
3894526	282060	0.63	0.0290	8.41
3894526	268857	0.45	0.0105	8.28
3894533	282360	0.55	0.0288	6.43
3894533	269157	0.48	0.0086	9.76
3894539	282660	0.46	0.0263	4.75
3894540	269457	0.51	0.0118	9.3
3894546	282960	0.42	0.0210	3.87
3894547	269757	0.55	0.0119	9.6
3894553	283260	0.43	0.0137	3.77
3894553	270057	0.61	0.0089	10
3894560	283560	0.39	0.0104	3.75
3894560	270356	0.67	0.0074	11.32
3894567	283860	0.34	0.0091	4.21
3894567	270656	0.72	0.0066	13.04
3894573	284160	0.3	0.0089	4.17
3894574	270956	0.76	0.0059	14.68
3894580	284460	0.28	0.0086	4.75
3894581	271256	0.92	0.0061	14.31
3894587	284760	0.25	0.0080	5.05
3894587	271556	1.05	0.0061	12.17
3894594	285059	0.27	0.0085	5.03
3894594	271856	0.96	0.0064	11.87
3894601	285359	0.28	0.0101	4.78
3894601	272156	0.92	0.0069	11.34
3894607	285659	0.25	0.0087	4.9
3894608	272456	0.84	0.0071	8.87
3894614	285959	0.15	0.0090	5.85
3894615	272756	0.7	0.0067	8.62
3894621	286259	0.08	0.0091	6.63
3894622	273056	0.61	0.0070	8.83
3894628	273356	0.63	0.0074	8.94
3894635	273656	0.7	0.0075	10.03
3894642	273956	0.78	0.0075	9.35
3894649	274255	0.81	0.0074	9.78
3894656	274555	0.84	0.0073	8.59
3894662	274855	0.82	0.0073	8.34
3894669	275155	0.78	0.0073	8.28
3894676	275455	0.74	0.0073	9.69
3894683	275755	0.73	0.0073	10.58
3894690	276055	0.79	0.0073	12.82
3894696	276355	0.86	0.0073	13.73
3894703	276655	0.85	0.0073	12.48
3894710	276955	0.76	0.0072	10.62
3894717	277255	0.65	0.0072	8.9
3894724	277555	0.68	0.0071	9.12
3894730	277855	0.76	0.0072	10.38
3894737	278154	0.81	0.0072	9.9
3894744	278454	0.79	0.0072	9.02

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3894751	278754	0.72	0.0071	9.49
3894758	279054	0.66	0.0072	10.05
3894764	279354	0.68	0.0073	9.15
3894771	279654	0.69	0.0071	9.21
3894778	279954	0.7	0.0070	9.02
3894785	280254	0.76	0.0071	8.15
3894792	280554	0.75	0.0063	8.99
3894798	280854	0.75	0.0069	9.05
3894805	281154	0.7	0.0085	8.12
3894812	281454	0.67	0.0160	9.02
3894819	281754	0.67	0.0256	9.29
3894819	268550	0.47	0.0200	10.42
3894826	282053	0.6	0.0285	7.76
3894826	268850	0.45	0.0112	7.71
3894833	282353	0.54	0.0288	5.72
3894833	269150	0.51	0.0083	9.03
3894839	282653	0.47	0.0259	4.39
3894840	269450	0.61	0.0099	10.58
3894846	282953	0.43	0.0197	3.93
3894847	269750	0.67	0.0089	9.23
3894853	283253	0.42	0.0110	3.72
3894853	270050	0.71	0.0075	11.08
3894860	283553	0.37	0.0084	3.64
3894860	270350	0.73	0.0068	12.63
3894867	283853	0.35	0.0095	3.9
3894867	270650	0.78	0.0059	15.25
3894873	284153	0.33	0.0102	4.18
3894874	270949	0.78	0.0049	14.67
3894880	284453	0.31	0.0101	4.96
3894881	271249	0.92	0.0048	18.99
3894887	284753	0.29	0.0097	4.84
3894887	271549	1.06	0.0043	13.07
3894894	285053	0.28	0.0100	5.18
3894894	271849	0.96	0.0060	11.69
3894901	285353	0.29	0.0101	4.81
3894901	272149	0.91	0.0070	10.3
3894907	285653	0.23	0.0086	5.08
3894908	272449	0.86	0.0071	9.43
3894914	285952	0.15	0.0091	6.01
3894915	272749	0.77	0.0065	9.19
3894921	286252	0.08	0.0099	6.81
3894921	273049	0.68	0.0068	8.42
3894928	273349	0.67	0.0073	8.5
3894935	273649	0.71	0.0074	9.33
3894942	273949	0.8	0.0074	9.56
3894949	274249	0.84	0.0073	9.25
3894955	274549	0.85	0.0073	8.9
3894962	274848	0.85	0.0073	9.27
3894969	275148	0.85	0.0073	9.32
3894976	275448	0.81	0.0073	9.89
3894983	275748	0.76	0.0073	11.18

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3894989	276048	0.72	0.0073	12.24
3894996	276348	0.75	0.0073	12.76
3895003	276648	0.76	0.0072	11.68
3895010	276948	0.71	0.0072	9.39
3895017	277248	0.67	0.0072	8.27
3895024	277548	0.68	0.0072	8.42
3895030	277848	0.75	0.0073	9.69
3895037	278148	0.89	0.0075	9.63
3895044	278448	0.97	0.0073	9.1
3895051	278747	0.94	0.0064	8.74
3895058	279047	0.82	0.0069	8.4
3895064	279347	0.73	0.0072	8
3895071	279647	0.72	0.0069	8.66
3895078	279947	0.74	0.0063	8.71
3895085	280247	0.73	0.0070	10.87
3895092	280547	0.72	0.0066	9.77
3895098	280847	0.73	0.0069	9.31
3895105	281147	0.7	0.0087	7.1
3895112	281447	0.69	0.0163	8.57
3895119	281747	0.68	0.0260	9.08
3895119	268543	0.52	0.0204	11.86
3895126	282047	0.61	0.0288	8.21
3895126	268843	0.51	0.0126	12.76
3895132	282347	0.55	0.0288	6.02
3895133	269143	0.58	0.0081	11.46
3895139	282646	0.49	0.0257	4.22
3895140	269443	0.73	0.0070	12.52
3895146	282946	0.42	0.0191	4.06
3895146	269743	0.85	0.0065	11.26
3895153	283246	0.41	0.0103	4.52
3895153	270043	0.88	0.0063	10.94
3895160	283546	0.36	0.0077	4.05
3895160	270343	0.86	0.0064	12.57
3895166	283846	0.36	0.0079	3.79
3895167	270643	0.89	0.0054	14.61
3895173	284146	0.37	0.0086	3.85
3895174	270943	0.89	0.0049	18.26
3895180	284446	0.34	0.0091	5.28
3895181	271243	0.87	0.0051	19.03
3895187	284746	0.31	0.0121	5.04
3895187	271543	0.9	0.0051	14.16
3895194	285046	0.29	0.0133	4.85
3895194	271842	0.88	0.0058	13.74
3895200	285346	0.29	0.0109	4.36
3895201	272142	0.87	0.0066	11.04
3895207	285646	0.22	0.0087	4.68
3895208	272442	0.82	0.0072	10.63
3895214	285946	0.16	0.0096	5.57
3895215	272742	0.81	0.0069	9.98
3895221	286246	0.1	0.0113	6.01
3895221	273042	0.76	0.0064	8.59

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3895228	286545	0.07	0.0103	6.43
3895228	273342	0.7	0.0074	8.57
3895235	286845	0.08	0.0086	5.02
3895235	273642	0.72	0.0084	8.36
3895241	287145	0.12	0.0086	4.73
3895242	273942	0.78	0.0078	9.05
3895248	287445	0.17	0.0078	4.59
3895249	274242	0.86	0.0073	9.08
3895255	287745	0.19	0.0086	5.08
3895255	274542	0.89	0.0073	9.24
3895262	274842	0.91	0.0073	10.32
3895269	275142	0.87	0.0073	9.97
3895276	275442	0.83	0.0073	10.55
3895283	275741	0.73	0.0073	10.43
3895289	276041	0.68	0.0073	12.03
3895296	276341	0.69	0.0072	11.88
3895303	276641	0.71	0.0072	11.06
3895310	276941	0.72	0.0072	10.31
3895317	277241	0.73	0.0071	10.27
3895323	277541	0.74	0.0073	9.76
3895330	277841	0.81	0.0076	11.21
3895337	278141	0.94	0.0089	9.95
3895344	278441	1.08	0.0081	8.95
3895351	278741	1.08	0.0071	9.09
3895357	279041	0.94	0.0077	9.02
3895364	279341	0.85	0.0084	8.56
3895371	279640	0.81	0.0086	9.4
3895378	279940	0.76	0.0085	9.11
3895385	280240	0.71	0.0087	8.26
3895392	280540	0.7	0.0079	9.85
3895398	280840	0.72	0.0083	9.64
3895405	281140	0.72	0.0111	8.21
3895412	281440	0.7	0.0188	8.6
3895419	281740	0.71	0.0272	8.87
3895419	268536	0.6	0.0202	13.72
3895426	282040	0.61	0.0292	8.16
3895426	268836	0.59	0.0109	14.99
3895432	282340	0.52	0.0291	5.6
3895433	269136	0.67	0.0070	13.98
3895439	282640	0.47	0.0260	4.12
3895440	269436	0.84	0.0048	15.59
3895446	282940	0.39	0.0198	4.1
3895446	269736	0.99	0.0047	8.76
3895453	283240	0.38	0.0111	4.29
3895453	270036	0.97	0.0058	10.38
3895460	283539	0.38	0.0085	3.75
3895460	270336	0.96	0.0052	11.56
3895466	283839	0.38	0.0080	3.85
3895467	270636	1.04	0.0051	12.27
3895473	284139	0.36	0.0088	4.24
3895474	270936	0.94	0.0057	16.26

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3895480	284439	0.32	0.0088	4.34
3895480	271236	0.81	0.0062	17.18
3895487	284739	0.28	0.0121	4.69
3895487	271536	0.8	0.0059	14.58
3895494	285039	0.26	0.0138	4.73
3895494	271836	0.79	0.0058	13.84
3895500	285339	0.25	0.0117	4.33
3895501	272136	0.84	0.0057	11.98
3895507	285639	0.23	0.0097	4.32
3895508	272435	0.82	0.0067	11.02
3895514	285939	0.19	0.0088	5.19
3895514	272735	0.79	0.0070	10.67
3895521	286239	0.15	0.0097	5.42
3895521	273035	0.78	0.0070	8.71
3895528	286539	0.13	0.0099	5.33
3895528	273335	0.71	0.0086	8.44
3895534	286839	0.15	0.0093	4.41
3895535	273635	0.67	0.0092	7.77
3895541	287139	0.2	0.0082	4.21
3895542	273935	0.73	0.0080	8.21
3895548	287438	0.25	0.0076	4.13
3895549	274235	0.84	0.0074	8.51
3895555	287738	0.25	0.0085	4.77
3895555	274535	0.96	0.0073	10.1
3895562	274835	0.97	0.0073	10.58
3895569	275135	0.91	0.0073	10.39
3895576	275435	0.82	0.0073	9.95
3895583	275735	0.7	0.0073	9.57
3895589	276035	0.64	0.0073	11.21
3895596	276334	0.67	0.0072	10.55
3895603	276634	0.73	0.0072	11.3
3895610	276934	0.77	0.0070	9.87
3895617	277234	0.83	0.0065	10.49
3895623	277534	0.82	0.0072	10.04
3895630	277834	0.85	0.0075	10.15
3895637	278134	0.92	0.0082	9.64
3895644	278434	1	0.0093	8.76
3895651	278734	0.99	0.0091	8.88
3895719	268530	0.67	0.0188	15.63
3895726	268830	0.73	0.0096	14.87
3895733	269130	0.78	0.0056	15.44
3895740	269429	0.87	0.0051	15.74
3895746	269729	0.96	0.0049	11.63
3895753	270029	0.98	0.0053	10.87
3895759	283533	0.38	0.0124	3.94
3895760	270329	0.95	0.0049	8.49
3895766	283833	0.38	0.0093	4.28
3895767	270629	1.02	0.0050	10.84
3895773	284132	0.33	0.0079	4.34
3895774	270929	0.96	0.0055	14.48
3895780	284432	0.29	0.0081	4.29

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3895780	271229	0.86	0.0063	15.34
3895787	284732	0.24	0.0101	4.87
3895787	271529	0.75	0.0064	16.91
3895794	285032	0.23	0.0110	4.39
3895794	271829	0.77	0.0063	12.64
3895800	285332	0.24	0.0097	4.27
3895801	272129	0.86	0.0061	11.32
3895807	285632	0.25	0.0106	4.18
3895808	272429	0.86	0.0067	10.17
3895814	285932	0.22	0.0098	4.3
3895814	272729	0.8	0.0076	8.51
3895821	286232	0.19	0.0083	4.78
3895821	273029	0.74	0.0086	7.78
3895828	286532	0.18	0.0080	4.81
3895828	273328	0.71	0.0095	7.54
3895834	286832	0.21	0.0089	4.34
3895835	273628	0.62	0.0096	6.89
3895841	287132	0.26	0.0091	4.29
3895842	273928	0.66	0.0083	7.5
3895848	287432	0.27	0.0082	4.6
3895848	274228	0.77	0.0076	8.1
3895855	287732	0.27	0.0087	4.7
3895855	274528	0.96	0.0074	9.97
3895862	274828	1.02	0.0073	10.71
3895869	275128	0.96	0.0073	10.05
3895876	275428	0.86	0.0073	9.8
3895882	275728	0.73	0.0073	10.29
3895889	276028	0.62	0.0073	10.64
3895896	276328	0.67	0.0072	11.1
3895903	276628	0.75	0.0069	10.38
3895910	276928	0.81	0.0068	10.2
3895916	277227	0.8	0.0084	10.56
3895923	277527	0.77	0.0092	10.1
3895930	277827	0.76	0.0080	8.38
3895937	278127	0.76	0.0075	8.08
3895944	278427	0.78	0.0083	7.4
3895951	278727	0.77	0.0108	7.62
3896019	268523	0.7	0.0168	14.32
3896026	268823	0.79	0.0087	16.45
3896033	269123	0.87	0.0063	14.49
3896039	269423	0.91	0.0056	16.3
3896046	269723	0.97	0.0053	12.56
3896053	270022	0.97	0.0055	10.41
3896059	283526	0.37	0.0187	3.97
3896060	270322	0.93	0.0057	10.28
3896066	283826	0.35	0.0134	4.01
3896067	270622	0.9	0.0053	9.97
3896073	284126	0.33	0.0107	4.14
3896073	270922	0.86	0.0060	11.06
3896080	284426	0.26	0.0095	4.53
3896080	271222	0.82	0.0067	12.84

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3896087	284726	0.21	0.0084	5.08
3896087	271522	0.75	0.0083	13.85
3896093	285025	0.21	0.0081	4.31
3896094	271822	0.77	0.0073	12.81
3896100	285325	0.26	0.0088	4.24
3896101	272122	0.87	0.0070	11.6
3896107	285625	0.27	0.0100	4.17
3896108	272422	0.88	0.0075	9.4
3896114	285925	0.26	0.0099	4.45
3896114	272722	0.8	0.0086	7.36
3896121	286225	0.25	0.0083	4.39
3896121	273022	0.74	0.0094	7.51
3896127	286525	0.22	0.0075	4.28
3896128	273322	0.7	0.0089	7.23
3896134	286825	0.24	0.0077	4.24
3896135	273622	0.62	0.0102	6.92
3896141	287125	0.25	0.0089	5.2
3896142	273921	0.59	0.0092	6.58
3896148	287425	0.25	0.0095	5.19
3896148	274221	0.68	0.0089	7.68
3896155	287725	0.24	0.0098	5.4
3896155	274521	0.84	0.0081	9.34
3896162	274821	0.95	0.0074	9.9
3896169	275121	0.93	0.0073	9.69
3896176	275421	0.89	0.0073	10.26
3896182	275721	0.78	0.0073	11.2
3896189	276021	0.65	0.0073	11.76
3896196	276321	0.64	0.0072	10.72
3896203	276621	0.72	0.0069	9.71
3896210	276921	0.77	0.0066	10.31
3896216	277221	0.71	0.0083	10.25
3896223	277521	0.66	0.0088	10.54
3896230	277820	0.64	0.0080	7.76
3896237	278120	0.62	0.0074	6.76
3896244	278420	0.6	0.0078	6.62
3896250	278720	0.6	0.0097	6.54
3896319	268516	0.67	0.0148	13.52
3896326	268816	0.76	0.0111	13.46
3896333	269116	0.89	0.0097	13.97
3896339	269416	1.01	0.0075	12.59
3896346	269716	1.1	0.0067	12.14
3896353	270016	1.06	0.0058	10.48
3896360	270316	1.01	0.0057	11.69
3896367	270616	0.89	0.0064	9.43
3896373	270915	0.86	0.0067	9.54
3896380	271215	0.8	0.0065	16.58
3896387	271515	0.75	0.0091	12.73
3896393	285019	0.27	0.0077	4.15
3896394	271815	0.78	0.0086	11.83
3896400	285319	0.31	0.0086	4.02
3896401	272115	0.85	0.0075	10.2

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3896407	285618	0.33	0.0085	3.87
3896407	272415	0.85	0.0078	8.68
3896414	285918	0.34	0.0090	4.16
3896414	272715	0.78	0.0099	8
3896421	286218	0.31	0.0090	3.97
3896421	273015	0.7	0.0090	7.35
3896427	286518	0.28	0.0080	4.24
3896428	273315	0.67	0.0083	7.35
3896434	286818	0.27	0.0074	4.12
3896435	273615	0.61	0.0106	6.85
3896441	287118	0.26	0.0080	4.92
3896441	273915	0.56	0.0104	6.41
3896448	287418	0.26	0.0103	5.06
3896448	274215	0.61	0.0110	7.28
3896455	287718	0.23	0.0120	5.49
3896455	274515	0.69	0.0093	8.17
3896462	274814	0.78	0.0077	8.46
3896469	275114	0.81	0.0073	8.39
3896475	275414	0.82	0.0073	9.6
3896482	275714	0.78	0.0073	10.37
3896489	276014	0.67	0.0075	10.18
3896496	276314	0.59	0.0074	9.71
3896503	276614	0.61	0.0072	9.4
3896510	276914	0.62	0.0074	9.1
3896516	277214	0.6	0.0090	9.72
3896523	277514	0.57	0.0098	9.15
3896530	277814	0.59	0.0082	7.5
3896537	278114	0.55	0.0075	6.3
3896544	278414	0.52	0.0090	6.03
3896550	278713	0.51	0.0102	6.1
3896619	268509	0.6	0.0110	12.34
3896626	268809	0.73	0.0099	12.2
3896632	269109	0.9	0.0088	10.34
3896639	269409	1.14	0.0076	11.7
3896646	269709	1.21	0.0071	11.5
3896653	270009	1.16	0.0067	10.95
3896660	270309	1	0.0066	10.18
3896667	270609	0.87	0.0070	8.96
3896673	270909	0.81	0.0071	8.89
3896680	271209	0.76	0.0073	9.82
3896687	271508	0.76	0.0093	10.69
3896693	285012	0.34	0.0077	4.02
3896694	271808	0.76	0.0095	10.28
3896700	285312	0.39	0.0075	3.72
3896701	272108	0.83	0.0082	9.34
3896707	285612	0.41	0.0077	3.81
3896707	272408	0.82	0.0079	8.32
3896714	285912	0.38	0.0088	3.78
3896714	272708	0.77	0.0101	7.7
3896721	286212	0.33	0.0093	3.82
3896721	273008	0.73	0.0092	7.77

STATE PLANE		Block Estimate Ni (%)	Estimation Variance Ni (%) ²	Depth of the block (ft)
X	Y			
3896727	286511	0.29	0.0082	3.81
3896728	273308	0.67	0.0086	7.39
3896734	286811	0.28	0.0075	3.96
3896735	273608	0.61	0.0120	7
3896741	287111	0.29	0.0076	4.26
3896741	273908	0.58	0.0138	6.5
3896748	287411	0.27	0.0090	4.69
3896748	274208	0.58	0.0141	6.71
3896755	287711	0.25	0.0110	4.69
3896755	274508	0.61	0.0117	7
3896762	274808	0.64	0.0085	7.48
3896769	275108	0.66	0.0077	7.13
3896775	275407	0.72	0.0079	8.22
3896782	275707	0.72	0.0083	8.82
3896789	276007	0.64	0.0094	9.13
3896796	276307	0.54	0.0084	8.42
3896803	276607	0.51	0.0074	9.05
3896809	276907	0.53	0.0074	8.61
3896816	277207	0.56	0.0081	9.38
3896823	277507	0.58	0.0084	8.58
3896830	277807	0.6	0.0078	7.22
3896837	278107	0.55	0.0076	6.82
3896843	278407	0.5	0.0090	5.84
3896850	278707	0.47	0.0127	5.4
3896919	268502	0.56	0.0074	10.07
3896926	268802	0.72	0.0074	10.84
3896932	269102	0.89	0.0076	11.08
3896939	269402	1.1	0.0073	11.1
3896946	269702	1.2	0.0073	10.61
3896953	270002	1.07	0.0072	10.01
3896960	270302	0.9	0.0072	9.89
3896966	270602	0.8	0.0072	9.12
3896973	270902	0.8	0.0074	8.47
3896980	271202	0.8	0.0083	8.7
3896987	271502	0.78	0.0097	9.77
3896993	285005	0.38	0.0092	3.78
3896994	271802	0.81	0.0112	9.34
3897000	285305	0.44	0.0078	3.87
3897000	272102	0.86	0.0091	8.67
3897007	285605	0.41	0.0077	3.8
3897007	272401	0.88	0.0080	8.76
3897014	285905	0.35	0.0079	3.62
3897014	272701	0.83	0.0103	8.28
3897020	286205	0.31	0.0083	3.64
3897021	273001	0.78	0.0101	7.98
3897027	286505	0.25	0.0092	3.49
3897028	273301	0.7	0.0112	7.19
3897034	286805	0.24	0.0087	3.62
3897035	273601	0.63	0.0160	6.77
3897041	287104	0.26	0.0080	4.06
3897041	273901	0.58	0.0193	6.65

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3897048	287404	0.27	0.0082	4.47
3897048	274201	0.57	0.0185	6.45
3897054	287704	0.23	0.0096	4.62
3897055	274501	0.59	0.0137	6.86
3897062	274801	0.59	0.0099	6.96
3897069	275101	0.62	0.0106	7.31
3897075	275401	0.68	0.0127	7.32
3897082	275701	0.65	0.0136	7.99
3897089	276001	0.62	0.0140	8.79
3897096	276300	0.53	0.0108	7.55
3897103	276600	0.5	0.0086	8.07
3897109	276900	0.5	0.0081	7.91
3897116	277200	0.56	0.0080	8.34
3897123	277500	0.6	0.0077	8.49
3897130	277800	0.57	0.0075	6.99
3897137	278100	0.5	0.0080	6.16
3897143	278400	0.47	0.0106	5.74
3897150	278700	0.46	0.0142	5.28
3897185	266996	0.51	0.0296	7.27
3897191	267296	0.52	0.0255	7.77
3897198	267596	0.54	0.0188	8.08
3897205	267896	0.54	0.0123	8.24
3897212	268196	0.58	0.0105	9.65
3897219	268496	0.64	0.0080	11.91
3897226	268796	0.78	0.0072	11.4
3897232	269095	0.91	0.0073	11.89
3897239	269395	1.02	0.0073	10.57
3897246	269695	1.04	0.0073	9.51
3897253	269995	0.95	0.0073	8.48
3897260	270295	0.84	0.0073	9.08
3897266	270595	0.83	0.0073	9.35
3897273	270895	0.9	0.0075	8.37
3897280	271195	0.89	0.0089	8.1
3897287	271495	0.84	0.0105	8.28
3897293	284998	0.39	0.0147	3.95
3897294	271795	0.83	0.0117	8.48
3897300	285298	0.43	0.0119	4.28
3897300	272095	0.9	0.0095	9.16
3897307	285598	0.38	0.0115	4.01
3897307	272395	0.95	0.0082	9.06
3897314	285898	0.3	0.0117	3.69
3897314	272695	0.91	0.0111	8.5
3897320	286198	0.27	0.0125	3.48
3897327	286498	0.23	0.0143	3.48
3897334	286798	0.22	0.0139	3.61
3897341	287098	0.23	0.0128	3.91
3897348	287398	0.24	0.0129	4.27
3897354	287698	0.23	0.0144	4.67
3897423	277493	0.6	0.0092	7.49
3897430	277793	0.54	0.0085	7.81
3897437	278093	0.46	0.0098	6.65

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3897443	278393	0.44	0.0115	5.67
3897450	278693	0.46	0.0119	4.88
3897485	266989	0.53	0.0286	7.02
3897491	267289	0.5	0.0216	6.89
3897498	267589	0.52	0.0130	6.99
3897505	267889	0.57	0.0087	7.96
3897512	268189	0.65	0.0095	8.54
3897519	268489	0.76	0.0088	9.93
3897525	268789	0.84	0.0075	11.12
3897532	269089	0.9	0.0073	9.97
3897539	269389	0.92	0.0073	8.53
3897546	269689	0.9	0.0075	7.54
3897553	269988	0.85	0.0079	7.64
3897559	270288	0.84	0.0077	8.77
3897566	270588	0.93	0.0074	9.51
3897573	270888	1.03	0.0073	9.04
3897580	271188	0.98	0.0076	8.2
3897587	271488	0.85	0.0083	8.29
3897594	271788	0.83	0.0105	8.47
3897600	272088	0.89	0.0094	8.78
3897607	272388	0.95	0.0083	8.76
3897614	272688	0.92	0.0124	8.57
3897723	277487	0.61	0.0130	6.77
3897730	277786	0.54	0.0132	6.91
3897736	278086	0.47	0.0117	5.74
3897743	278386	0.44	0.0107	5.14
3897750	278686	0.46	0.0110	4.85
3897785	266982	0.51	0.0256	6.96
3897791	267282	0.5	0.0176	6.8
3897798	267582	0.52	0.0103	6.81
3897805	267882	0.6	0.0073	7.42
3897812	268182	0.7	0.0081	8.61
3897819	268482	0.77	0.0086	10.38
3897825	268782	0.77	0.0075	9.95
3897832	269082	0.8	0.0074	8.82
3897839	269382	0.84	0.0081	8.05
3897846	269682	0.85	0.0087	7.06
3897853	269982	0.86	0.0092	7.56
3897859	270282	0.85	0.0083	8.03
3897866	270581	0.92	0.0074	8.79
3897873	270881	0.98	0.0073	8.45
3897880	271181	0.92	0.0073	8.24
3897887	271481	0.79	0.0078	7.78
3897893	271781	0.76	0.0101	8.17
3897900	272081	0.81	0.0097	8.17
3897907	272381	0.87	0.0089	8.26
3897914	272681	0.88	0.0140	8.52
3898084	266976	0.52	0.0222	7.15
3898091	267276	0.52	0.0131	6.43
3898098	267575	0.57	0.0082	6.99
3898105	267875	0.65	0.0067	8.99

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3898112	268175	0.71	0.0075	10.12
3898118	268475	0.7	0.0078	11.1
3898125	268775	0.66	0.0073	10.1
3898132	269075	0.66	0.0078	9.28
3898139	269375	0.75	0.0098	7.57
3898146	269675	0.81	0.0108	7.74
3898153	269975	0.85	0.0090	8.5
3898159	270275	0.82	0.0076	8.51
3898166	270575	0.79	0.0073	8.12
3898173	270875	0.77	0.0073	7.75
3898180	271175	0.74	0.0073	8.13
3898187	271474	0.7	0.0080	8.28
3898193	271774	0.71	0.0111	8.36
3898200	272074	0.77	0.0126	8.05
3898207	272374	0.82	0.0131	8.02
3898214	272674	0.82	0.0178	8.23
3898384	266969	0.54	0.0188	7.94
3898391	267269	0.56	0.0108	7.59
3898398	267569	0.65	0.0073	7.93
3898405	267869	0.75	0.0063	12.72
3898412	268169	0.73	0.0073	11.31
3898418	268468	0.69	0.0069	14.26
3898425	268768	0.65	0.0066	11.63
3898432	269068	0.63	0.0083	9.66
3898439	269368	0.72	0.0107	8.89
3898446	269668	0.82	0.0101	8.91
3898452	269968	0.83	0.0080	8.64
3898459	270268	0.8	0.0073	8.41
3898466	270568	0.7	0.0073	7.39
3898473	270868	0.62	0.0073	7.02
3898480	271168	0.62	0.0076	7.49
3898684	266962	0.57	0.0155	7.77
3898691	267262	0.6	0.0092	7.57
3898698	267562	0.72	0.0074	8.31
3898705	267862	0.78	0.0074	9.23
3898712	268162	0.79	0.0090	11.11
3898718	268462	0.76	0.0085	11.97
3898725	268762	0.73	0.0069	11.68
3898732	269061	0.73	0.0095	10.53
3898739	269361	0.77	0.0113	9.51
3898746	269661	0.87	0.0094	9.49
3898752	269961	0.9	0.0076	9.56
3898759	270261	0.84	0.0073	8.62
3898766	270561	0.71	0.0074	7.12
3898773	270861	0.61	0.0077	6.7
3898780	271161	0.59	0.0095	7.37
3898984	266955	0.62	0.0155	8.44
3898991	267255	0.69	0.0094	8.62
3898998	267555	0.77	0.0075	9.27
3899005	267855	0.82	0.0077	9.1
3899011	268155	0.79	0.0096	10.38

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3899018	268455	0.78	0.0094	11.16
3899025	268755	0.76	0.0080	11.03
3899032	269055	0.75	0.0099	10.39
3899039	269355	0.79	0.0102	9.27
3899045	269655	0.85	0.0082	9.28
3899052	269954	0.88	0.0073	9.52
3899059	270254	0.85	0.0075	8.5
3899066	270554	0.76	0.0086	7.14
3899073	270854	0.65	0.0107	6.9
3899080	271154	0.63	0.0150	7.57
3899284	266948	0.66	0.0142	9.86
3899291	267248	0.75	0.0085	10.18
3899298	267548	0.85	0.0074	9.38
3899305	267848	0.87	0.0077	8.73
3899311	268148	0.83	0.0097	9.07
3899318	268448	0.79	0.0098	10.06
3899325	268748	0.75	0.0088	10.31
3899332	269048	0.76	0.0108	10.17
3899339	269348	0.8	0.0102	9.33
3899345	269648	0.81	0.0078	9.14
3899352	269948	0.82	0.0076	9.11
3899359	270248	0.84	0.0091	8.68
3899366	270547	0.78	0.0131	7.97
3899373	270847	0.7	0.0182	7.31
3899379	271147	0.66	0.0227	7.41
3899584	266942	0.69	0.0146	9.14
3899591	267242	0.78	0.0088	9.26
3899598	267541	0.88	0.0074	8.88
3899604	267841	0.9	0.0077	8.2
3899611	268141	0.82	0.0096	8.24
3899618	268441	0.76	0.0102	8.99
3899625	268741	0.72	0.0106	9.56
3899632	269041	0.7	0.0131	9.33
3899639	269341	0.7	0.0110	8.97
3899645	269641	0.69	0.0088	8.8
3899884	266935	0.67	0.0166	9.09
3899891	267235	0.74	0.0106	8.84
3899898	267535	0.81	0.0075	8.54
3899904	267835	0.85	0.0074	8.43
3899911	268134	0.78	0.0093	8.22
3899918	268434	0.72	0.0106	8.69
3899925	268734	0.66	0.0118	8.8
3899932	269034	0.66	0.0149	8.86
3899938	269334	0.64	0.0124	8.8
3899945	269634	0.64	0.0117	8.61
3900150	265428	0.49	0.0257	8.54
3900157	265728	0.49	0.0219	8.81
3900164	266028	0.53	0.0195	9.1
3900170	266328	0.56	0.0197	9.27
3900177	266628	0.58	0.0196	9.06
3900184	266928	0.62	0.0160	8.74

STATE PLANE		Block	Estimation	Depth of
X	Y	Estimate	Variance	the block
		Ni (%)	Ni (%) ²	(ft)
3900191	267228	0.65	0.0107	8.35
3900198	267528	0.67	0.0074	8.44
3900204	267828	0.7	0.0065	7.59
3900211	268128	0.68	0.0092	8.27
3900450	265422	0.48	0.0232	8.39
3900457	265721	0.48	0.0161	8.57
3900463	266021	0.49	0.0114	8.65
3900470	266321	0.53	0.0129	8.63
3900477	266621	0.56	0.0154	9
3900484	266921	0.59	0.0129	8.34
3900491	267221	0.61	0.0093	8.2
3900497	267521	0.62	0.0074	8.55
3900504	267821	0.64	0.0073	8.47
3900511	268121	0.64	0.0103	8.62
3900750	265415	0.48	0.0220	8.42
3900757	265715	0.48	0.0138	8.7
3900763	266015	0.49	0.0087	9.27
3900770	266315	0.51	0.0102	9.88
3900777	266614	0.54	0.0125	9.08
3900784	266914	0.56	0.0115	8.66
3900791	267214	0.59	0.0100	8.17
3900797	267514	0.62	0.0076	7.99
3900804	267814	0.63	0.0077	7.95
3900811	268114	0.62	0.0114	8.58
3901050	265408	0.47	0.0214	8.17
3901056	265708	0.48	0.0134	8.89
3901063	266008	0.5	0.0083	9.54
3901070	266308	0.53	0.0097	8.8
3901077	266608	0.54	0.0126	8.72
3901084	266908	0.56	0.0127	8.2
3901090	267207	0.58	0.0109	7.87
3901097	267507	0.6	0.0081	7.56
3901104	267807	0.6	0.0086	7.54
3901111	268107	0.59	0.0134	7.27
3901350	265401	0.44	0.0205	7.74
3901356	265701	0.44	0.0133	7.65
3901363	266001	0.46	0.0084	7.38
3901370	266301	0.51	0.0096	8
3901377	266601	0.53	0.0117	8.29
3901384	266901	0.54	0.0116	8.24
3901390	267201	0.55	0.0122	7.87
3901397	267501	0.53	0.0103	7.61
3901404	267801	0.53	0.0125	6.97
3901411	268100	0.55	0.0190	7.46
3901650	265394	0.41	0.0187	7.09
3901656	265694	0.4	0.0140	6.9
3901663	265994	0.4	0.0100	6.47
3901670	266294	0.45	0.0112	7.01
3901677	266594	0.48	0.0132	8.04
3901684	266894	0.5	0.0136	8.32
3901690	267194	0.52	0.0169	7.75

STATE PLANE		Block Estimate Ni (%)	Estimation Variance Ni (%) ²	Depth of the block (ft)
X	Y			
3901697	267494	0.5	0.0180	7.63
3901704	267794	0.52	0.0205	7.47
3901711	268094	0.53	0.0251	7.67

APPENDIX D
PETROGRAPHIC REPORT

REPORT ON THE PETROGRAPHIC ANALYSIS OF ROCK SAMPLES POLISH SECTIONS (Translated from French by AJR)

The present report include the petrographic analysis of 2 polish sections made from two rock samples collected by AJR during the site visit. The analysis were done using a polarizing microscope with transmitted light for the observation of the silicates and in reflected light for the observation of oxides and sulphurs. Also the reports present photographs that illustrate minerals and observed textures.

Sample R1

Mineralogical assemblage

Silicates minerals

Altered olivine	65%
Serpentine	10%
Chlorite	5%
Talc	5%

Dark minerals

Oxides:	
Magnetite	10 %
Hématite	5 %

Name of the rock:

Peridotite, without pyroxene the rock would be called a dunite, but intense mineralogical alteration as made this call difficult.

Description of minerals

Olivine – $(Mg, Fe)_2SiO_4$

Olivine highly altered in serpentine and oxides. It is dirty brown and is replaced by serpentine, magnetite and hematite. This alteration is the result of fluid circulation and presents a metamorphism of the upper greenschist and the lower amphibolite facies. The observation revealed that the olivine is a intermediary composition between the forsterite and the fayalite.

Serpentine - $Mg_3Si_2O_5(OH)_4$

Serpentine is a phyllosilicate that can be observed in several mineral species: lizardite, antigorite and chrysotile. Nickeliferous serpentine are named garnierite, pecoraite, nepouite, etc. The section analysed present mainly the antigorite serpentine variety, with a typical knitted structure and with some chrysotile veinlets.

Talc - $Mg_6Si_8O_{20}(OH)_4$

Talc is a phyllosilicate that can be observed within magnesium rich serpentine. In the section, talc veinlets cutting across serpentine. The veinlets are micro-folded which would lead to assume a large silica injection thru a metasomatic process that have transformed the serpentine into talc and magnesite.

Chlorite ferromagnesian and magnesian - $(Mg, Fe^{2+}, Fe^{3+}, Mn, Al)_{12}(Si, Al)_8O_{20}(OH)_{16}$

Chlorite indicates that the ultramafic rocks are rich in aluminium and magnesium. The chlorite is also a phyllosilicate resulting in the olivine alteration. The chlorite is in veinlets cutting all the other minerals, including the micro-folded talc veinlets, revealing a secondary and late nature.

Dark minerals

Oxides

Magnetite (Fe_3O_4 with often significant quantities of Mg, Mn, Al, Cr et Ti)

Magnetite is in contact with the chlorite veinlets inside the larger olivine crystals. It is the result of the iron rich olivine and pyroxene alteration.

Hematite (Fe_2O_3)

Hematite is found inside the larger olivine crystals. It is the result of the iron rich olivine and pyroxene alteration.

Sample R2

Mineralogical assemblage

Silicates minerals

Chlorite	33%
Talc	30%
Quartz	15%
Zirconium	9%
Rutile	6%
Amphibole	2%

Dark minerals

Oxide:	
Magnetite	5%

Name of the rock:

Peridotite ? So intensely altered that it is difficult to tell the initial rock name

Description of minerals

Chlorite ferromagnesian and magnesian - $(Mg, Fe^{2+}, Fe^{3+}, Mn, Al)_{12} (Si, Al)_8 O_{20} (OH)_{16}$

Chlorite is observed with a micro-sheeting structure and is forming a very fine grain assemblage with talc, quartz and magnetite. This is the result of the total alteration of the former minerals composing the protolite. There is no signs of primary minerals and the section is composed in secondary minerals that make the bowlingite, a type of olivine alteration.

Talc - $Mg_3 Si_2 O_5 (OH)_2$

Talc is a phyllosilicate that can be observed within magnesium rich serpentine. In the section, it present in two forms:

1. micro-cristaline within a chlorite, quartz and magnetite fine grain matrix;
2. with the typical fibrous form in late veins of quartz and talc cutting across the fine grain matrix.

Quartz (SiO_2)

Like the talc, quartz is present in the section in two forms:

3. micro-crystalline within a chlorite, quartz and magnetite fine grain matrix, some quartz eyes are remnants of old olivine completely replaced by quartz, chlorite and magnetite;
4. with the fibrous talc in late veins of quartz and talc cutting across the fine grain matrix.

Zircon $Zr(SiO_4)$

It is observed in small sub-rounded prisms included into chlorite. The sub-rounded shape is indicative of metasomatic hydrothermal process.

Rutile TiO_2

It is in fine needles in the quartz/talc veins. Its presence signifies high temperature hydrothermal process.

Amphibole $Ca_2(Mg, Fe)_5Si_8O_{22}(OH)_2$

It is part of the actinote family and forms prismatic shapes. Its composition lies between tremolite and ferrotremolite.

Dark minerals

Oxides

Magnetite (Fe_3O_4 with often significant quantities of Mg, Mn, Al, Cr et Ti)

Magnetite is present in fine grains within the matrix in association with the alteration that forms the bowlingite. It is the result of the iron rich olivine.

Montréal, le 17 janvier 2008.

Objet : rapport final sur l'analyse pétrographique de lames minces polies.

Ce rapport final contient les analyses pétrographiques détaillées des 4 lames minces polies effectuées à partir de 4 échantillons de roches. Les informations sur la localisation exacte et la géologie locale et régionale de ces échantillons n'ont pas été données au pétrographe afin de préserver la confidentialité totale du site actuellement exploré. Ces analyses ont été effectuées au microscope polarisant en lumière transmise pour l'observation des silicates et en lumière réfléchie pour l'observation des oxydes et des sulfures.

Ce rapport contient des photos en couleur pour illustrer les minéraux et les textures observés afin de faciliter la compréhension de la lecture des descriptions.

Numéro de l'échantillon : R1

Numéro de la lame mince polie : R1

Assemblage minéralogique

Minéraux silicatés

Olivine altérée : 65%

Serpentine : 10%

Chlorite : 5%

Talc : 5%

Nom de la roche :

Péridotite. S'il y avait des pyroxènes, ils ont été complètement altérés et il est difficile de les retracer. Sans pyroxène, cette roche pourrait être appelée dunite.

Minéraux opaques

Oxides :

Magnétite : 10%

Hématite : 5%

Description des minéraux

Olivine – $(Mg, Fe)_2SiO_4$

L'olivine est très altérée en serpentine et oxides. Elle a donc un aspect brun sâle en lumière naturelle. Elle est remplacée par de la serpentine, de la magnétite, de l'hématite. La serpentinisation de l'olivine résulte de la circulation de fluides hydrothermaux. La transition du faciès des schistes verts à celui des amphibolites s'accompagne d'une grande quantité de fluides métamorphiques. On observe alors la réaction :
Olivine → serpentine + brucite.

La transformation de l'olivine en serpentine et oxides révèle une composition intermédiaire entre la forstérite et la fayalite.

Serpentine - $Mg_3Si_2O_5(OH)_4$

La serpentine est un phyllosilicate qui se présente sous plusieurs espèces minérales : la lizardite, l'antigorite et le chrysotile sont les plus importantes. Comme mentionné plus haut, le contexte des échantillons analysés ici laisse sous-entendre que cette serpentine est une variété nickélifère (le Ni remplace le Mg dans la structure du minéral).

La variété de serpentine la plus répandue dans cette lame est l'antigorite. En effet, on observe nettement la structure maillée du minéral avec des veinules de chrysotile qui

traversent cette structure. Elle montre une couleur jaunâtre en lumière naturelle et une biréfringence grise bleutée en nicols croisés.

Elle caractérise un faciès métamorphique aux schistes verts supérieur – amphibolite inférieur.

Talc - $Mg_6Si_8O_{20}(OH)_4$

Le talc est un phyllosilicate présent dans les serpentinites magnésiennes. Il est normalement, totalement incolore en lumière naturelle et se présente en sections allongées comme les micas. Il est parfois fibreux.

Dans la lame observée, il se retrouve en veinules qui recoupent la serpentine. On le reconnaît facilement en nicols croisés avec ses couleurs de biréfringence très vives dans les bleu-violet-orange de la fin du 2^e au début du 3^e ordre. Ces veinules sont plissotées.

Avec un métasomatisme accompagné d'une forte addition de silice, la serpentine se transforme selon la réaction :

Serpentine → talc + magnésite.

La lame R1 ne contient pas de quartz. Cependant, la lame R2 contient des veinules de quartz tardif qui pourrait caractériser ce métasomatisme. Cette observation n'est qu'une supposition car l'auteur ignore si ces deux lames proviennent de la même lithologie.

Chlorite ferromagnésienne et magnésienne - $(Mg, Fe^{2+}, Fe^{3+}, Mn, Al)_{12}(Si, Al)_8O_{20}(OH)_{16}$

La présence de chlorite dans cette lame montre que cette roche ultrabasique contient de l'aluminium.

En lumière naturelle, la chlorite montre un pléochroïsme vert pâle car elle contient du fer. La couleur verte caractérise la présence de fer dans sa structure. Sa couleur pâle montre qu'elle contient également du magnésium. Elle résulte de l'altération des minéraux ferromagnésiens tels que l'olivine.

En nicols croisés, elle montre une biréfringence faible avec des teintes de polarisation dans les gris du début du 1^{er} ordre et une extinction irrégulière.

La chlorite s'observe sous forme de veinules qui recoupent tous les minéraux. Cela reflète sa nature tardive. Elle recoupe également des veinules de talc plissées.

Minéraux opaques

Les oxydes

Magnétite (Fe_3O_4 avec souvent des quantités significatives de Mg, Mn, Al, Cr et Ti)

Elle montre une couleur grise bleutée en lumière naturelle. Elle est isotrope en nicols croisés. Elle se retrouve en contact des veinules de chlorite et à l'intérieur des cristaux d'olivine altérée.

Hématite (Fe_2O_3)

De couleur brun-rouge en lumière naturelle, elle montre une anisotropie en nicols croisés. Elle se retrouve comme produit de remplacement dans les cristaux d'olivine.

Numéro de l'échantillon : R2
 Numéro de la lame mince polie : R2

Assemblage minéralogique

Minéraux silicatés

Chlorite : 33%
 Talc : 30%
 Quartz : 15%

Zircon : 9%
 Rutile : 6%
 Amphibole : 2%

Nom de la roche :

Ancienne péridotite? L'altération est intense et il est difficile de retracer le protolite.

Minéraux opaques

Oxides :
 Magnétite : 5%

Description des minéraux

Chlorite ferromagnésienne et magnésienne - $(Mg, Fe^{2+}, Fe^{3+}, Mn, Al)_{12}(Si, Al)_8O_{20}(OH)_{16}$

La chlorite se présente en feuillets microcristallins et forme une matrice à grains très fins avec du talc, du quartz, et de la magnétite. Ces produits résultent de l'altération totale des minéraux ferromagnésiens qui constituaient cette roche. Il ne reste aucune trace de ces minéraux primaires et la lame est constituée essentiellement de ces produits secondaires qui composent la bowlingite, altération typique de l'olivine.

En lumière naturelle, la chlorite est incolore à légèrement verdâtre. Elle contient donc essentiellement du magnésium et un peu de fer. En nicols croisés, elle montre une biréfringence faible avec des teintes de polarisation dans les gris du début du 1^{er} ordre et une extinction irrégulière.

Talc - $Mg_3Si_2O_5(OH)_2$

Le talc est un phyllosilicate présent dans les serpentinites magnésiennes. Il est, normalement, totalement incolore en lumière naturelle et se présente en sections allongées comme les micas. Il est parfois fibreux.

Dans la lame observée, il se retrouve sous deux formes :

- sous une forme microcristalline dans la matrice et il se mélange à de la chlorite, du quartz et de la magnétite. Il résulte de l'altération de minéraux très magnésiens comme l'olivine et le pyroxène;

- sous forme fibreuse dans des veinules tardives composées de quartz limpide et de talc. Le talc forme des `cheveux`ondulants à l'intérieur de ces veinules qui semblent recouper les produits d'altération de la matrice. Ce talc résulte d'un métasomatisme accompagné d'une forte addition de silice, caractérisé par la présence de quartz limpide à rutile.

Cette lame semble donc représenter donc une roche ultrabasique entièrement recristallisée. Des processus métamorphiques, accompagnés d'un métasomatisme important ayant permis la circulation de fluides hydrothermaux, ont entraîné la recristallisation totale de la roche. La texture microcristalline témoigne de cette recristallisation.

Quartz (SiO_2)

Comme le talc, le quartz se présente sous deux formes :

- sous forme microcristalline dans la matrice où il se mélange aux produits d'altération dans la bowlingite. Des `yeux`de quartz retracent d'anciennes olivines complètement remplacées par du quartz, de la chlorite et de la magnétite.

- sous forme limpide dans les veinules tardives avec du talc fibreux. Il contient alors des aiguilles de rutile qui caractérisent sa nature primaire. Il provient alors de fluides hydrothermaux riches en silice ayant lessivé la roche.

Zircon $\text{Zr}(\text{SiO}_4)$

Il se présente en petits prismes sub-arrondis à arrondis en inclusions dans la chlorite. En lumière naturelle, ils présentent un fort relief. En nicols croisés, ils ont des couleurs vives de biréfringence.

Leur forme arrondie témoigne de leur corrosion par des processus métasomatiques. La circulation des fluides hydrothermaux, retracés par la présence des veinules de quartz limpide, est responsable de cette altération des grains.

Rutile TiO_2

Il se présente en fines aiguilles à fort relief dans le quartz limpide où il forme des cheveux fibreux.

Sa présence caractérise le lessivage de la roche par des fluides de haute température. En effet, le rutile représente le polymorphe de haute température d'oxyde de titane.

Amphibole $\text{Ca}_2(\text{Mg, Fe})_5\text{Si}_8\text{O}_{22}(\text{OH})_2$

Cette amphibole fait partie de la famille des actinotes dont les deux membres purs sont : la trémolite (Mg) et la ferrotrémolite (Fe).

Elle se présente sous une forme prismatique avec un faible pléochroïsme vert pâle témoignant de sa teneur en fer. Cette amphibole est donc ferro-magnésienne et possède une composition intermédiaire entre la trémolite et la ferrotrémolite.

En nicols croisés, elle montre des teintes orange-grise.

Sa présence témoigne d'un métamorphisme au faciès des amphibolites. La présence de chlorite témoigne d'un faciès amphibolite inférieur. La quantité de fluides hydrothermaux est importante à ce faciès. Cela concorde avec la présence des veinules de quartz limpide à inclusions de rutile, à la corrosion des grains de zircon par des processus metasomatiques et au remplacement total des minéraux primaires comme l'olivine et les pyroxènes. La roche primaire a donc entièrement recristallisé et aucune structure ni minéraux primaires syn-magmatiques ne subsistent.

Minéraux opaques

Les oxides

Magnétite (Fe_3O_4 avec souvent des quantités significatives de Mg, Mn, Al, Cr et Ti)

Elle se présente en petits grains dans la matrice où elle est associée aux produits d'altération formant la bowlingite. Elle résulte donc de l'altération de l'olivine ferrière.

Fait le 21 janvier 2008 à Montréal par :

A handwritten signature in dark ink, appearing to read 'S. CADERON', with a long horizontal flourish extending to the right.

Sandrine CADERON, Geo., Ph.D.
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Tél : (450) 926-0409
Courriel : alexandrine_geo@yahoo.ca



Photo 18 : LM R1. LN – X10. Ol + Serp + Tlc + Chlo + Mag. *Haut gauche* : l’olivine est progressivement remplacée par des oxides. On observe des veinules de chlorite et de talc. La chlorite montre un pléochroïsme vert pâle. Le talc et la serpentine sont de couleur jaunâtre. Les veinules de chlorite semblent tardives par rapport au talc, à la serpentine et à l’altération de l’olivine.

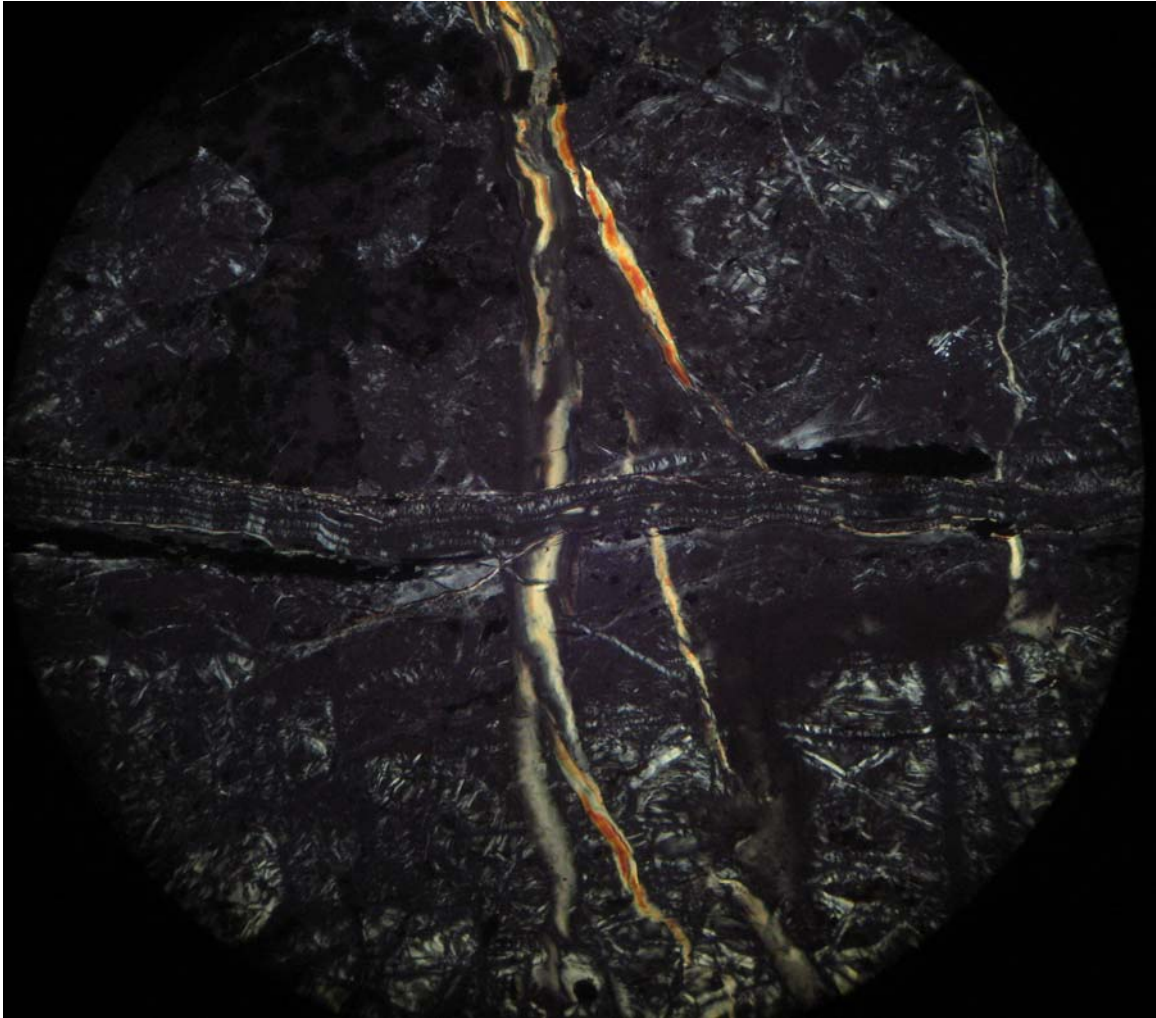


Photo 19 : LM R1. LP – X10. Ol + Serp + Tlc + Chlo + Mag. Idem que la photo 18 en LP. On observe nettement le recoupement des veinules chlorite-talc : la chlorite (grise bleutée) est tardive et recoupe le talc (biréfringence élevée dans les orange-rose). La serpentine forme des mailles typiques de l'antigorite.

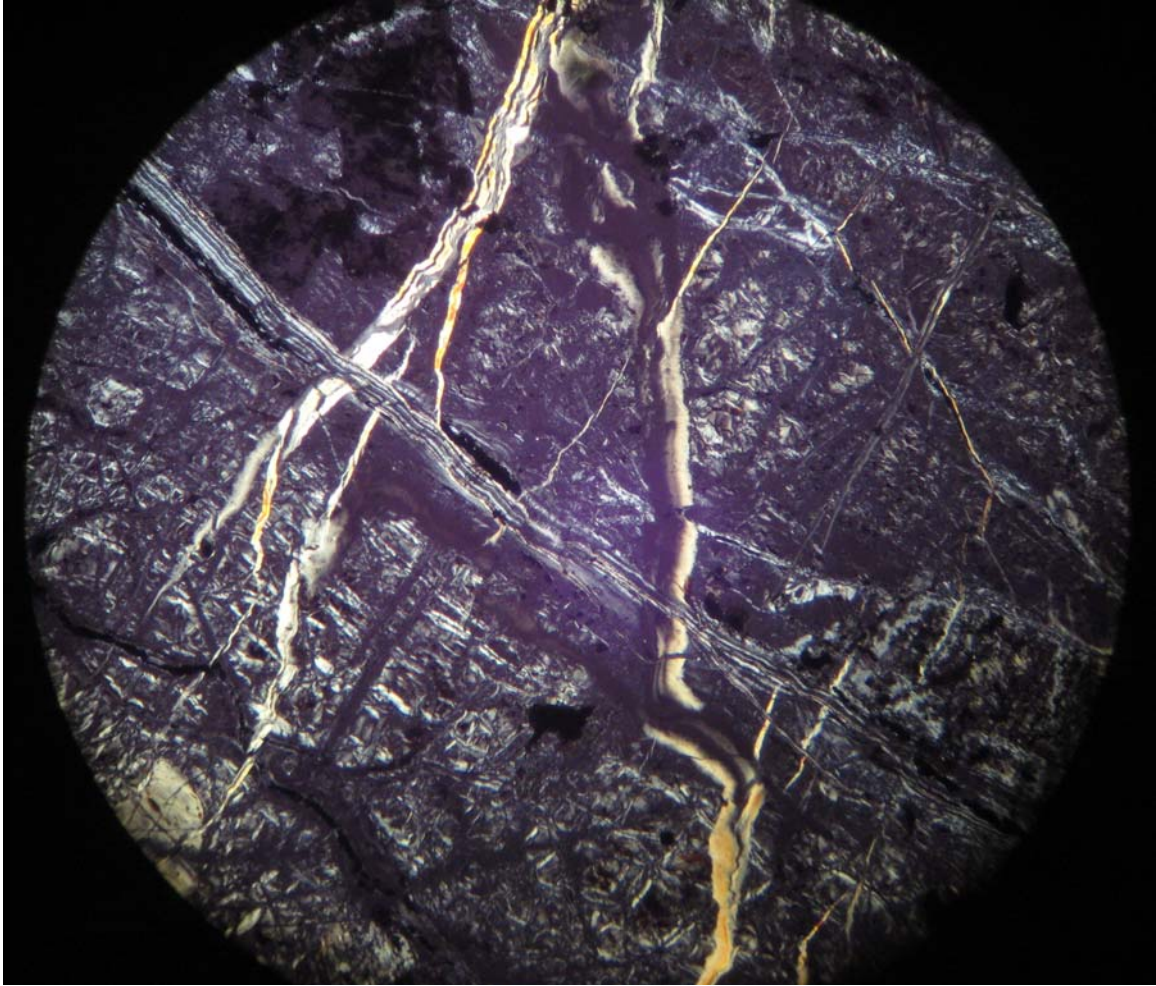


Photo 20: LM R1. LP – X5. Serp + Tlc + Chlo + Mag. Si on retrace l'évolution des minéraux : (1)- serpentinisation de l'olivine avec formation de serpentine de magnétite; (2)- mise en place des veinules de talc; (3) plissement des veinules de talc; (4) mise en place des veinules de chlorite.



Photo 21 : LM R1. LN – X5. Ol + Serp + Chlo + Mag + Hém. Serpentinisation de l'olivine avec exsolutions d'oxides (Mag + Hém). La serpentine montre une couleur jaunâtre.

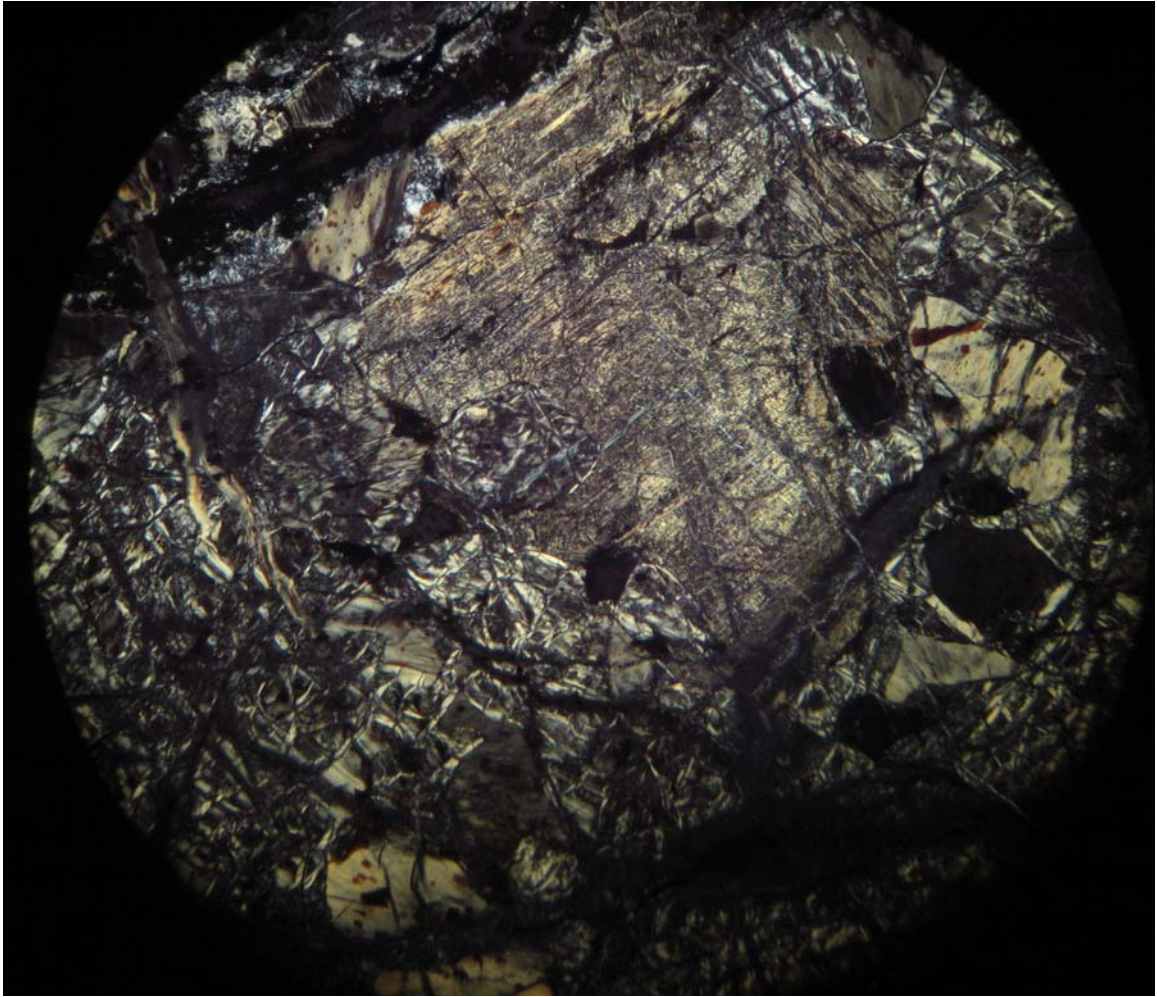


Photo 22 : LM R1. LP – X5. Idem que la photo 21 en LP.

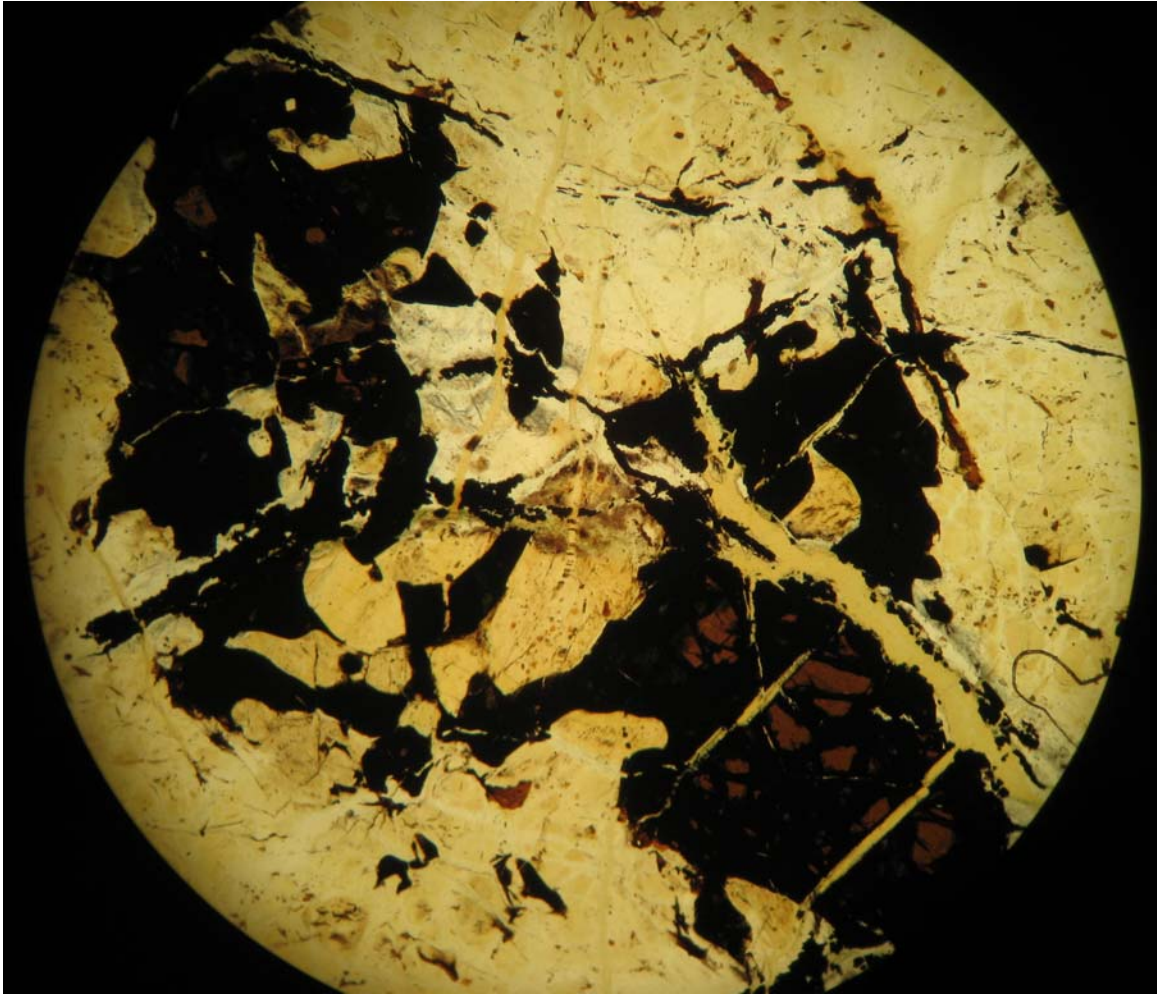


Photo 23 : LM R1. LN – X5. Ol + Serp + Tlc + Chlo + Mag + Hém. Remplacement de l'olivine par de la serpentine et des oxides. L'olivine a une composition intermédiaire entre la forstérite et la fayalite. Son altération entraîne donc la formation de minéraux ferro-magnésiens et d'oxides.

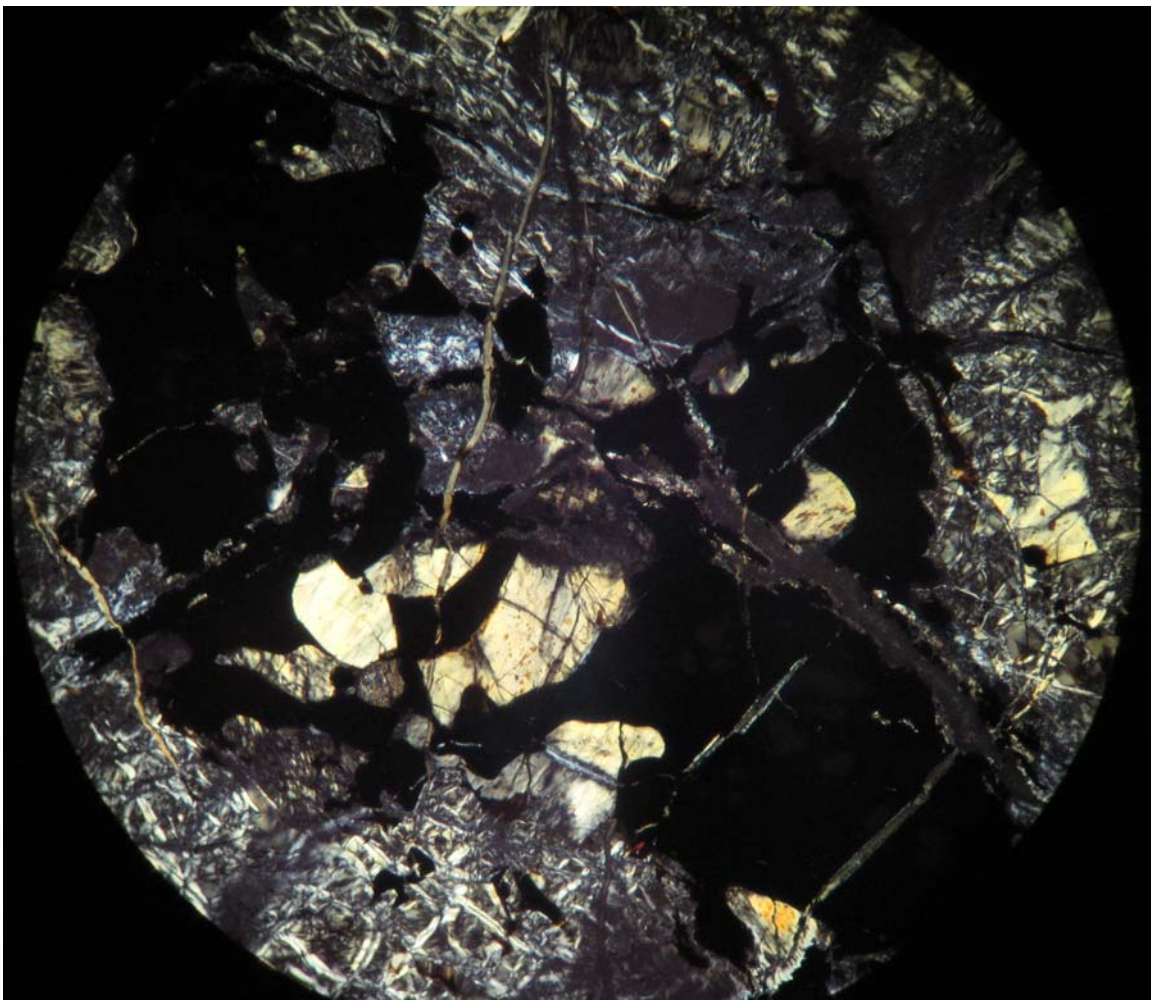


Photo 24 : LM R1. LP – X5. Idem que la photo 23 en LP.



Photo 25 : LM R1. LN – X5. Serp + Chlo + Hém + Mag. Exsolutions d'oxides à travers la serpentine. Il ne reste plus rien de l'olivine. La serpentine montre sa couleur jaunâtre caractéristique.

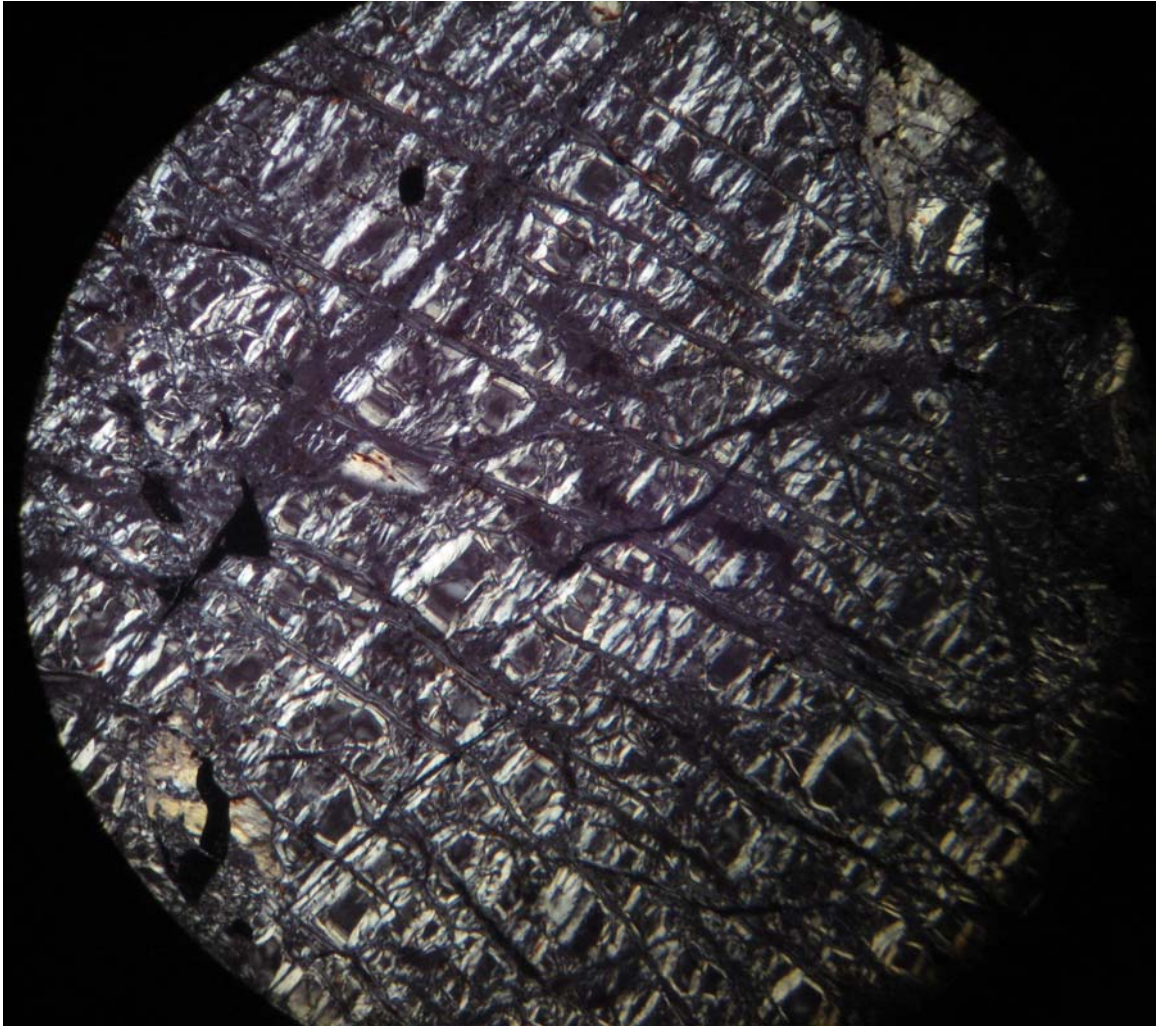


Photo 26 : LM R1. LP – X5. Idem que la photo 25 en LP. On observe nettement la structure maillée de la serpentine. Des filonnets de chrysotile fibreux traversent les mailles de l’antigorite.

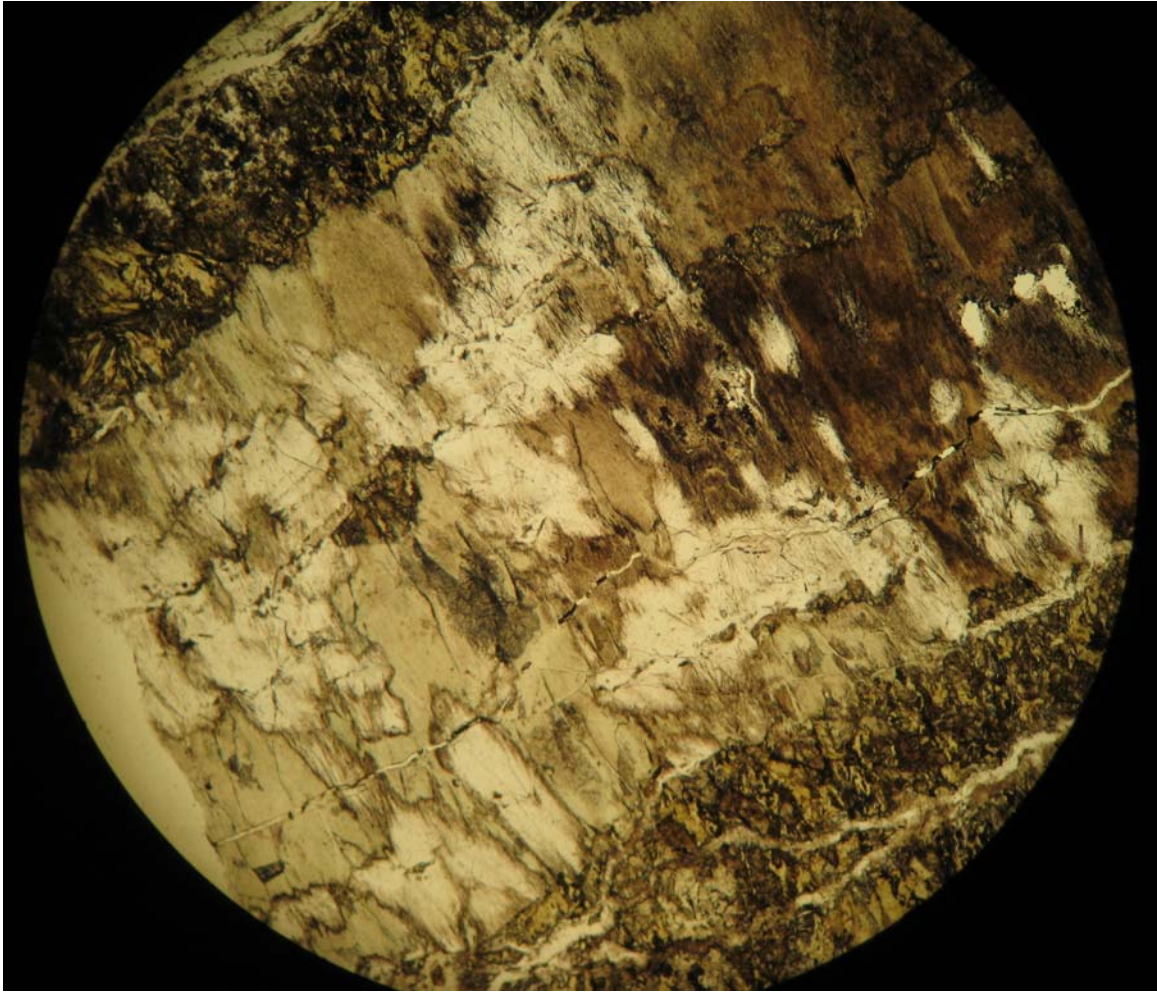


Photo 27 : LM R2. LN – X5. Tlc + Qtz + Rut + Bow. Veinules à talc + quartz. Le talc se présente sous sa forme fibreuse comme des `cheveux`ondulants. On observe des aiguilles très fines de rutile dans le quartz. La bowlingite compose la matrice microcristalline et contient un mélange de talc + quartz + chlorite.

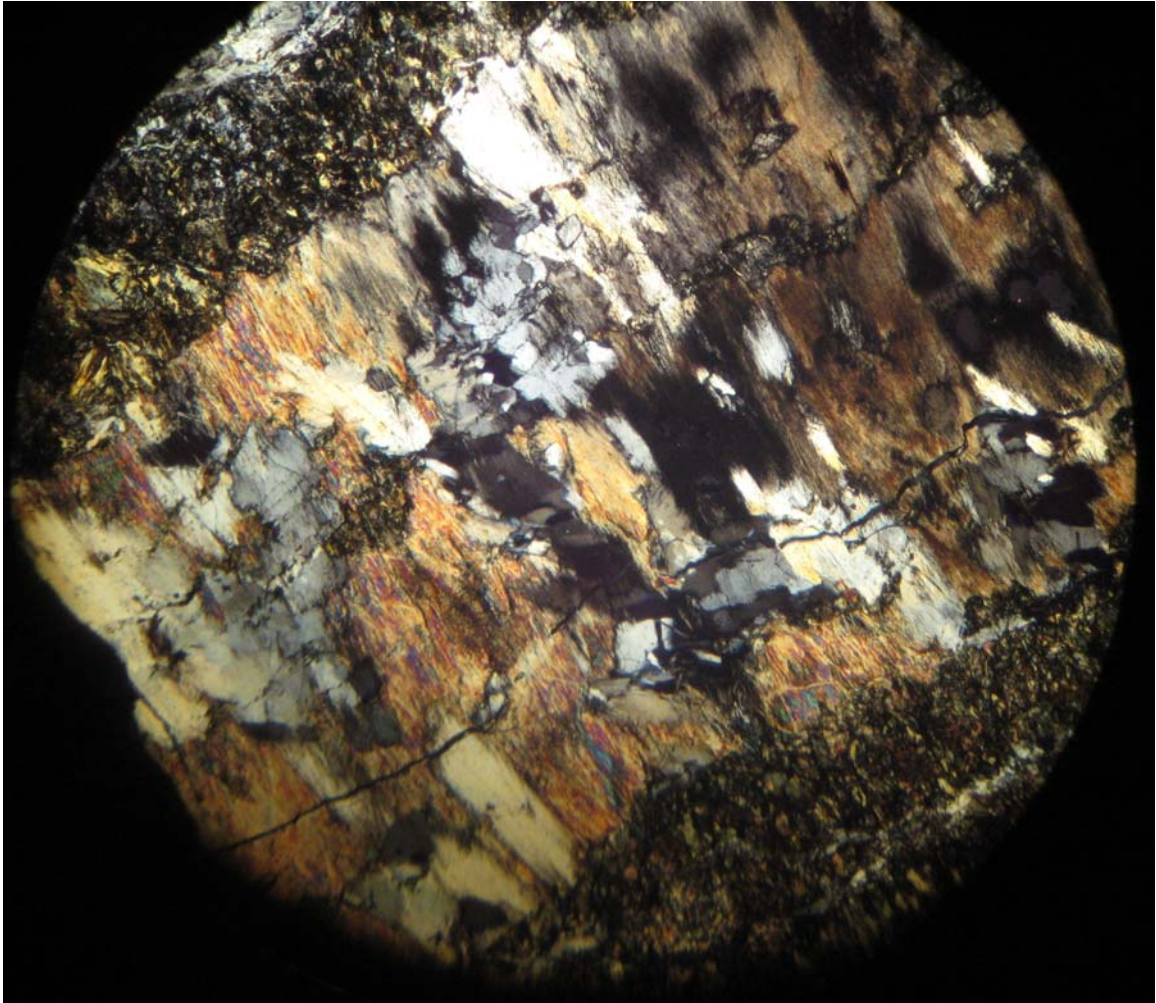


Photo 28 : LM R2. LP – X5. Idem que la photo 27 en LP. Le talc montre des couleurs très vives de biréfringence. Le quartz est limpide. Les veinules recoupent l'altération à bowlingite et semblent donc tardives.

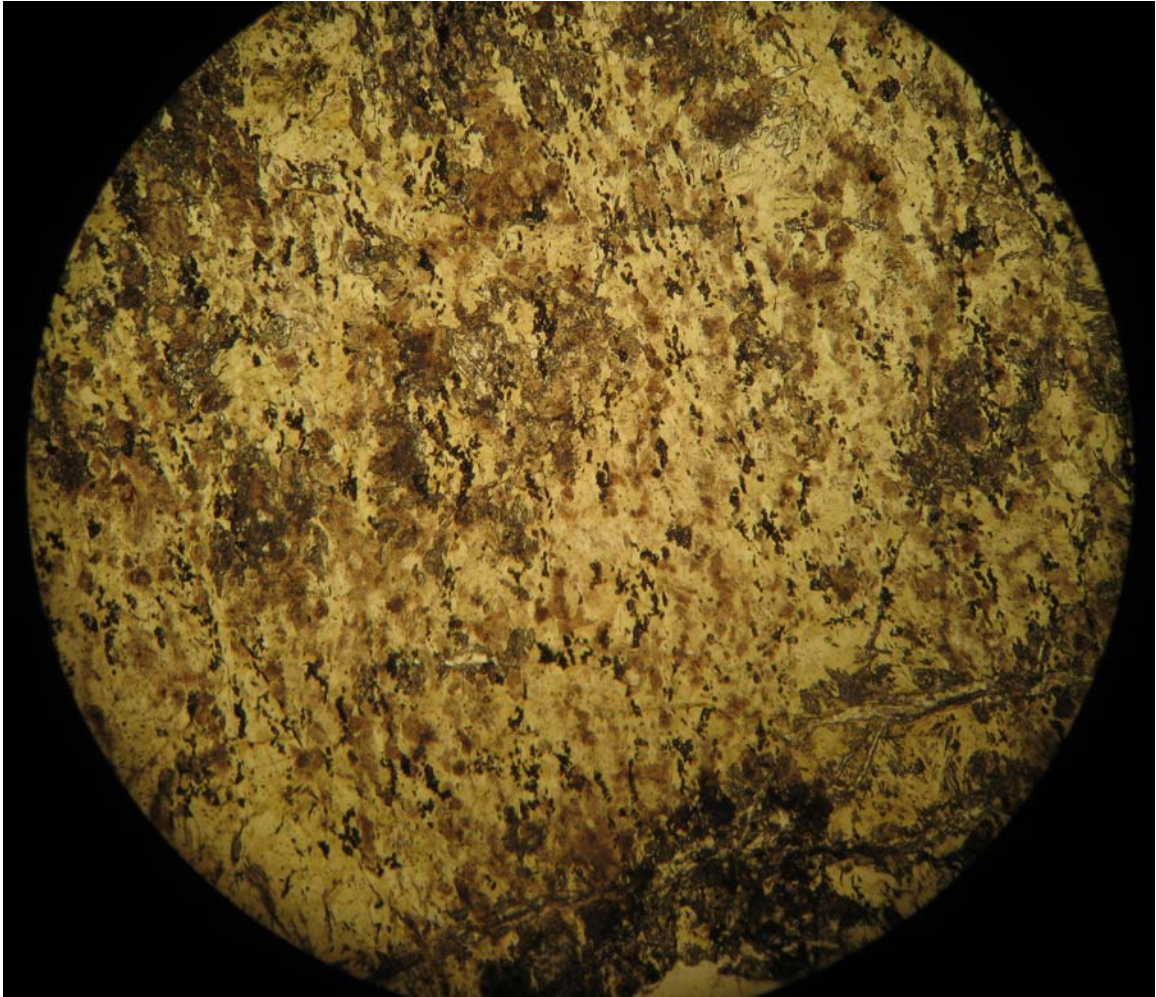


Photo 29 : LM R2. LN – X5. Mélange de Chlo + Tlc + Qtz + Hém + Mag formant de la bowlingite. Les cristaux sont microcristallins et proviennent de l'altération d'une roche riche en olivine et pyroxènes. Aucun minéral primaire ne subsiste.

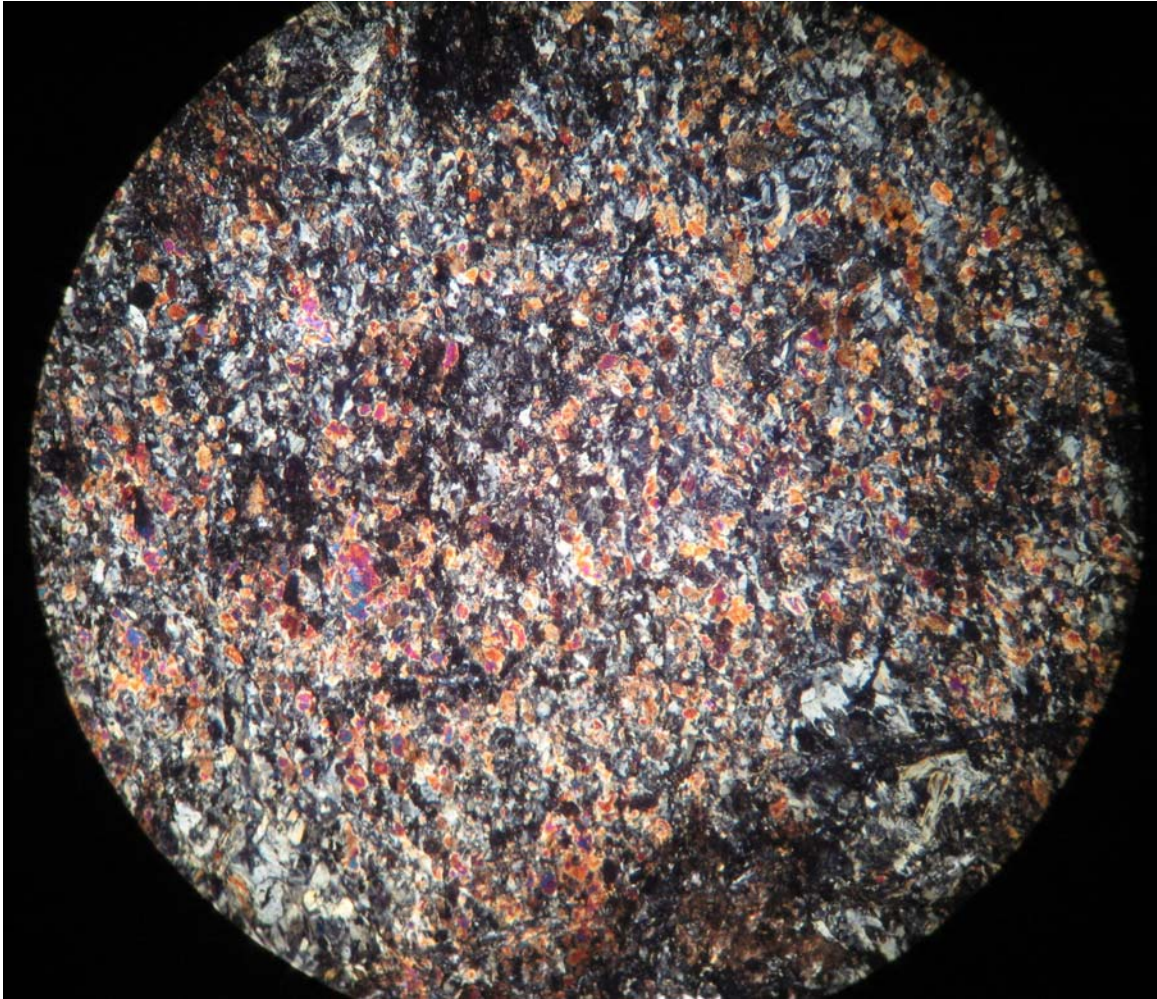


Photo 30 : LM R2. LP – X5. Idem que la photo 29 en LP. Le talc, en cristaux microcristallins, montre une forte biréfringence (bleu-rose-orange). Ces minéraux microcristallins ont recristallisé à partir de minéraux primaires dont ils résultent par altération.

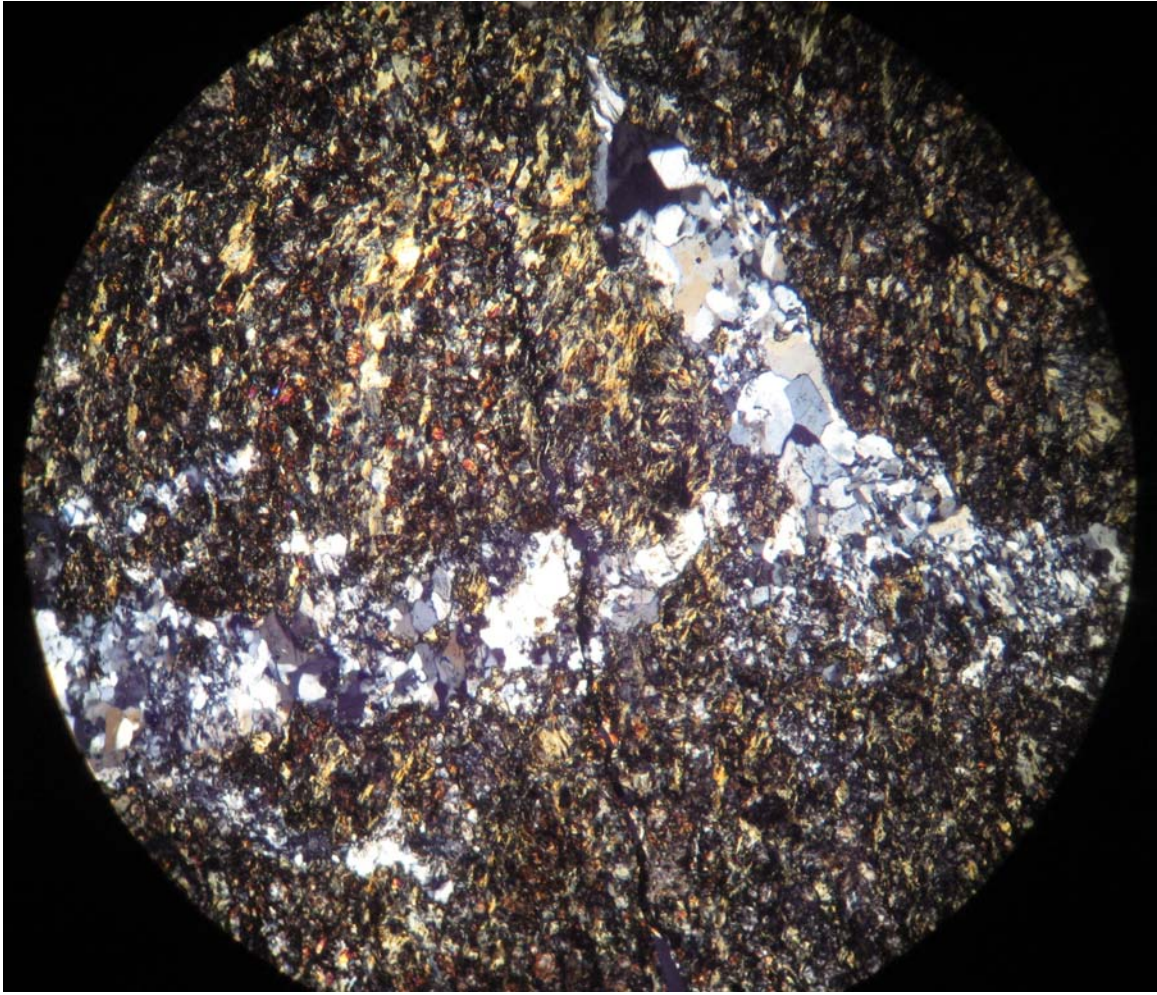


Photo 31 : LM R2. LP – X5. Veinules tardives à quartz microcristallin recoupant la matrice microcristalline à chlo + Tlc + Qtz + Mag. La présence de ce quartz témoigne d’une circulation importante de fluides dans la roche. Ces fluides ont entraîné une altération intense avec une disparition des minéraux primaires.

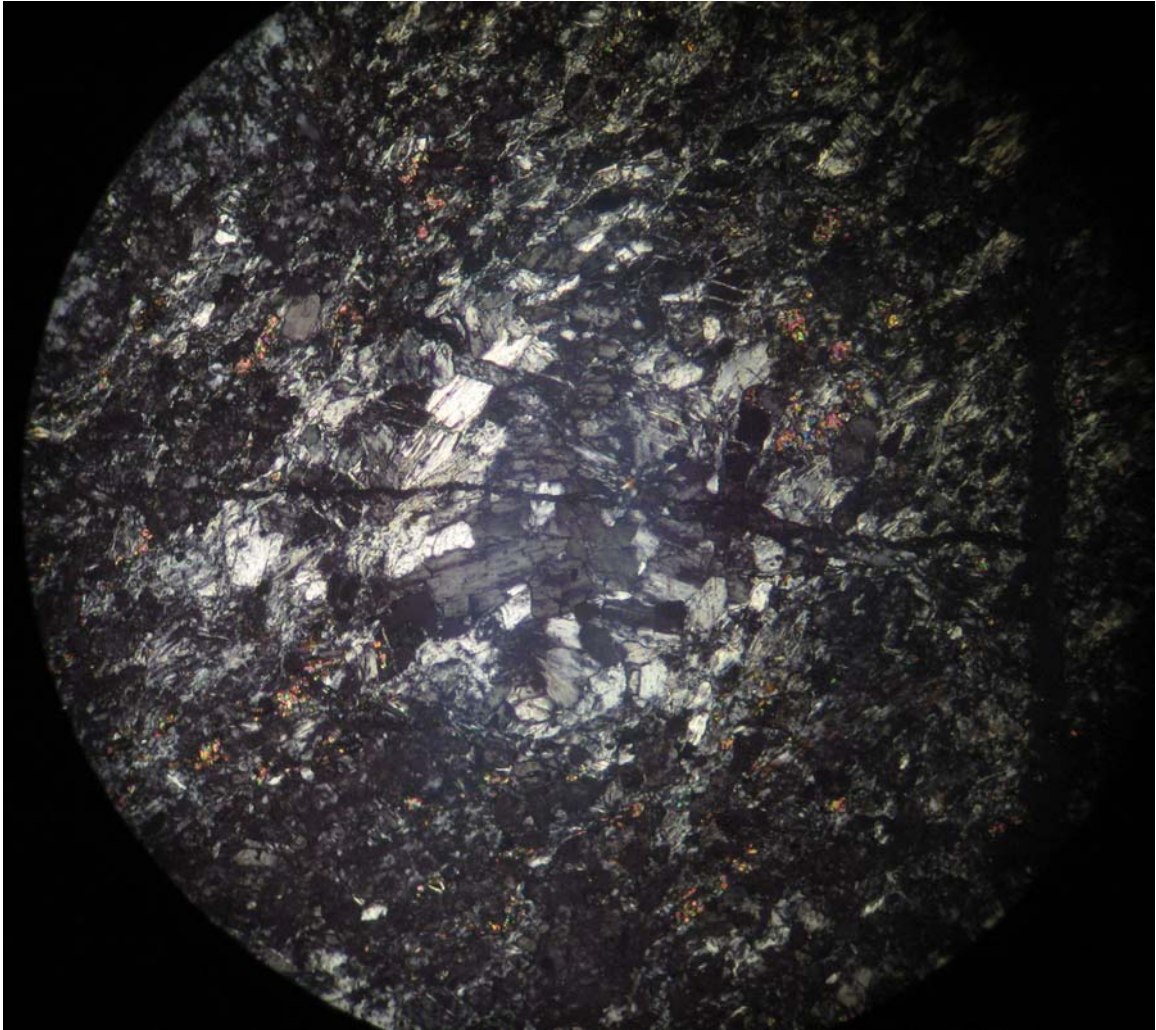


Photo 32 : LM R2. LP – X10. *Centre:* fantôme d'olivine entièrement remplacée par du quartz, de la chlorite et de la magnétite. On observe également des petits cristaux de zircon à très forte biréfringence dans la matrice microcristalline.

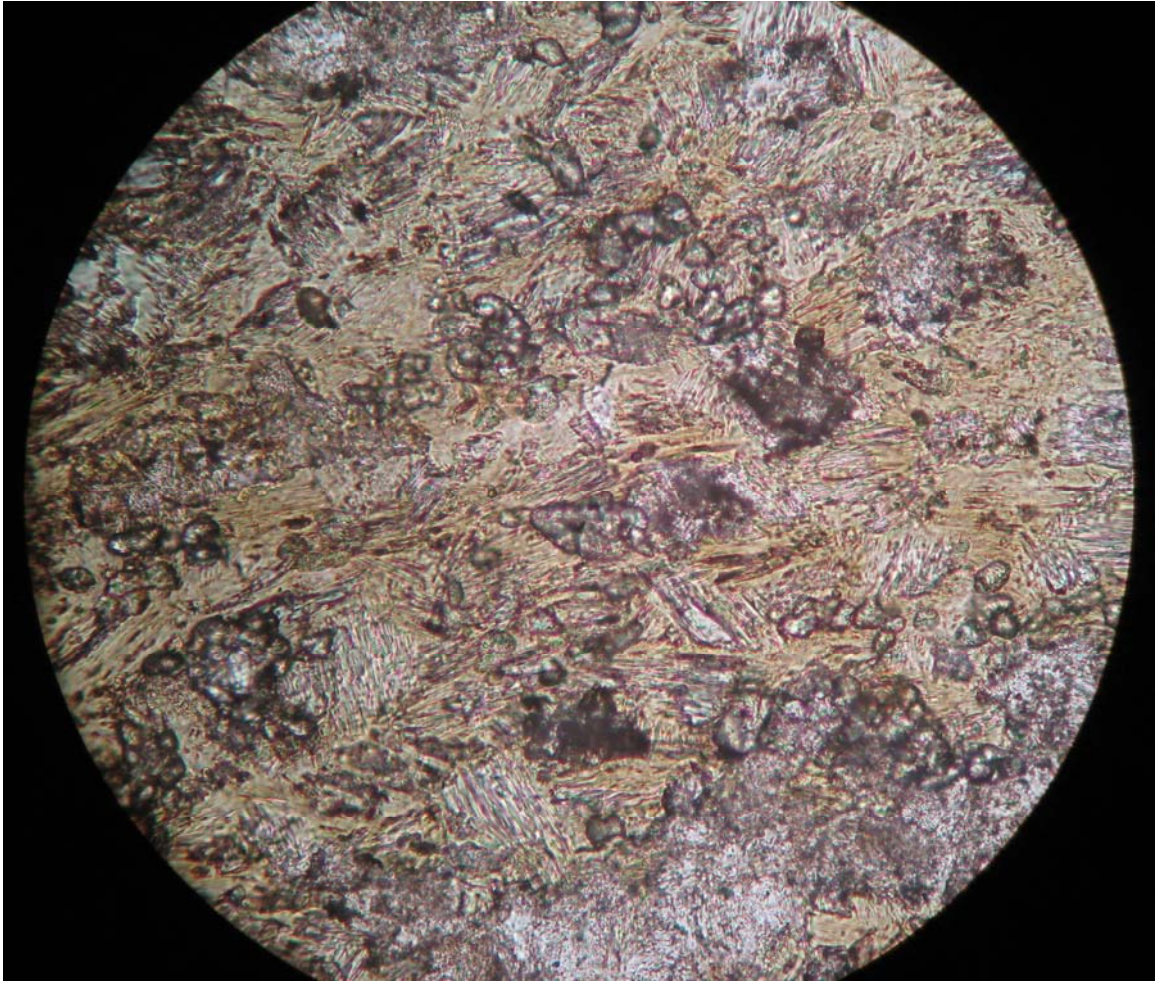


Photo 33 : LM R2. LN – X40. Cristaux de zircon dans des feuillets de chlorite. Les grains arrondis témoignent de la corrosion des cristaux par du métasomatisme.

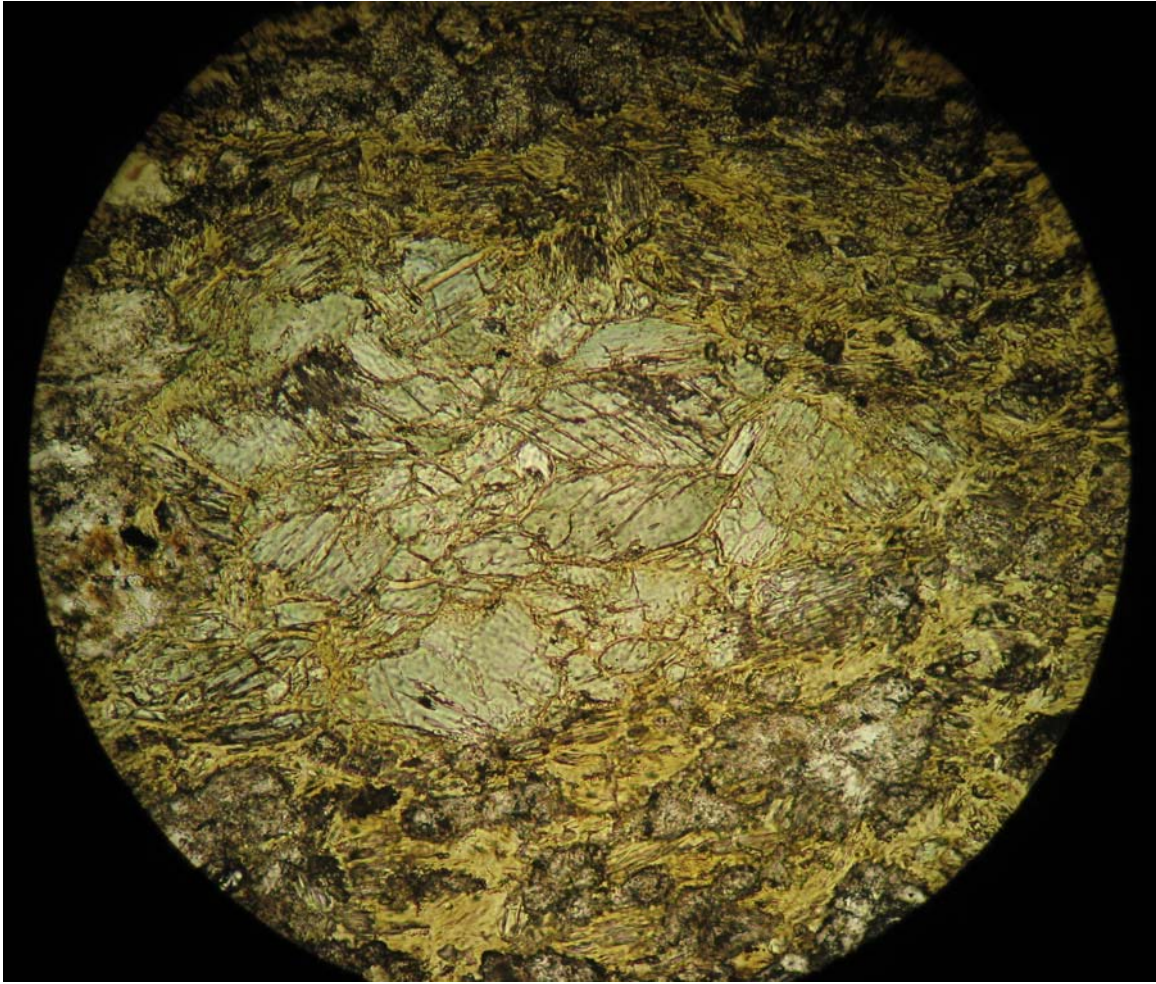


Photo 34 : LM R2. LN – X20. Amp + Tlc + Bow. On observe les cristaux losangiques de l'amphibole avec un pléochroïsme vert pâle. La bowlingite a un aspect jaune-verdâtre.

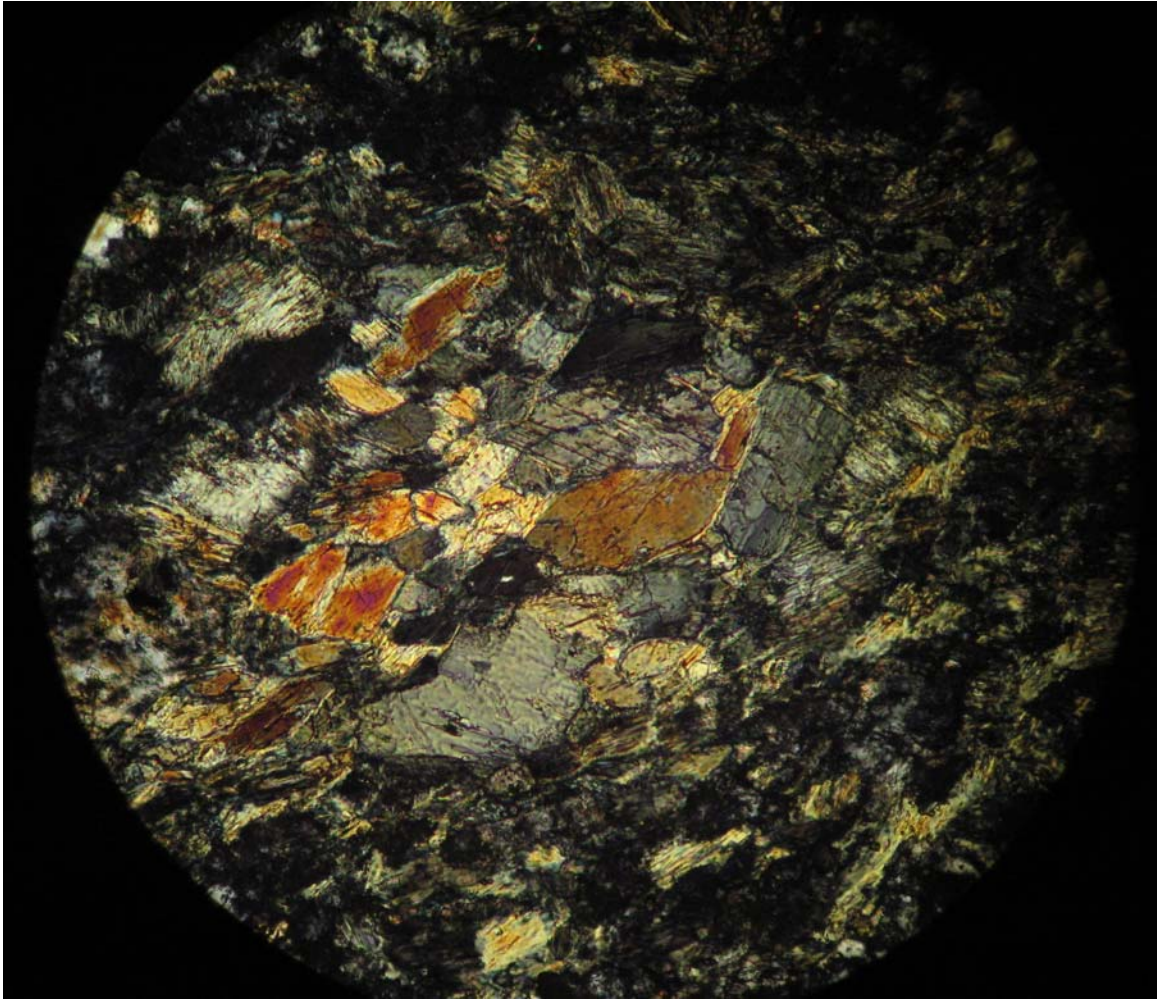


Photo 35 : LM R2. LP – X20. Idem que la photo 34 en LP. L'amphibole montre des couleurs de biréfringence gris et orange, tandis que le talc montre des couleurs irrégulières orange-rose violacé. La matrice est un mélange de chlorite, de quartz, de talc et d'oxides.

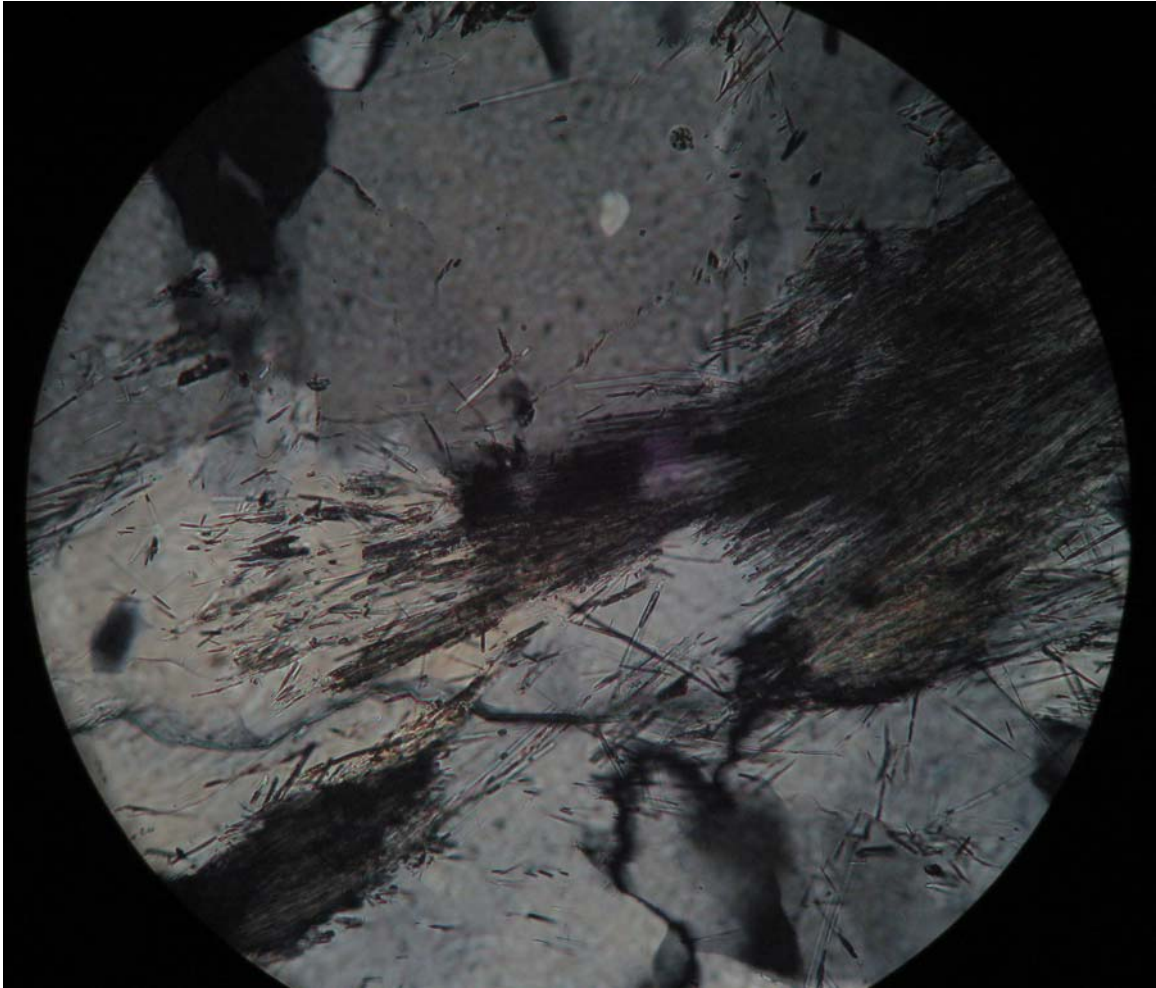


Photo 36 : LM R2. LP – X40. Aiguilles de rutile dans le quartz des veinules à Tlc + Qtz. Ce rutile nous témoigne de l'origine hydrothermale du quartz. Des fluides riches en silice ont circulé dans la roche tardivement. Les veinules semblent recouper les produits d'altération.

APPENDIX E

LIST OF CLAIMS AND DEED

United States Department of the Interior
Bureau of Land Management
 DIV OF MANAGEMENT SERVICES
 P.O. BOX 2965
 PORTLAND, OR 97208
 Phone: (503) 808-6008

Receipt

No: 1638879

Transaction #: 1692717	
Date of Transaction: 01/16/2008	
CUSTOMER:	BULLIVANT/HOUSER/BAILEY PC 300 PIONEER TOWER 888 SW FIFTH AVENUE PORTLAND, OR 97204

LINE #	QTY	DESCRIPTION	REMARKS	UNIT PRICE	TOTAL
1	1.00	LOCATABLE MINERALS / MINING CLAIMS- NOT NEW-UNADJUD, ONE AUTH NO. ONLY / MINING CLAIM MONEY RECEIVED (455) CASES: ORMC161516/\$2510.00		- n/a -	2510.00
TOTAL:					\$2,510.00

PAYMENT INFORMATION							
1	AMOUNT:	\$2,510.00	POSTMARKED:	N/A			
	TYPE:	CHECK	RECEIVED:	01/16/2008			
	CHECK NO:	171415					
	NAME:	BULLIVANT/HOUSER/BAILEY PC 300 PIONEER TOWER 888 SW FIFTH AVENUE PORTLAND OR 97204					

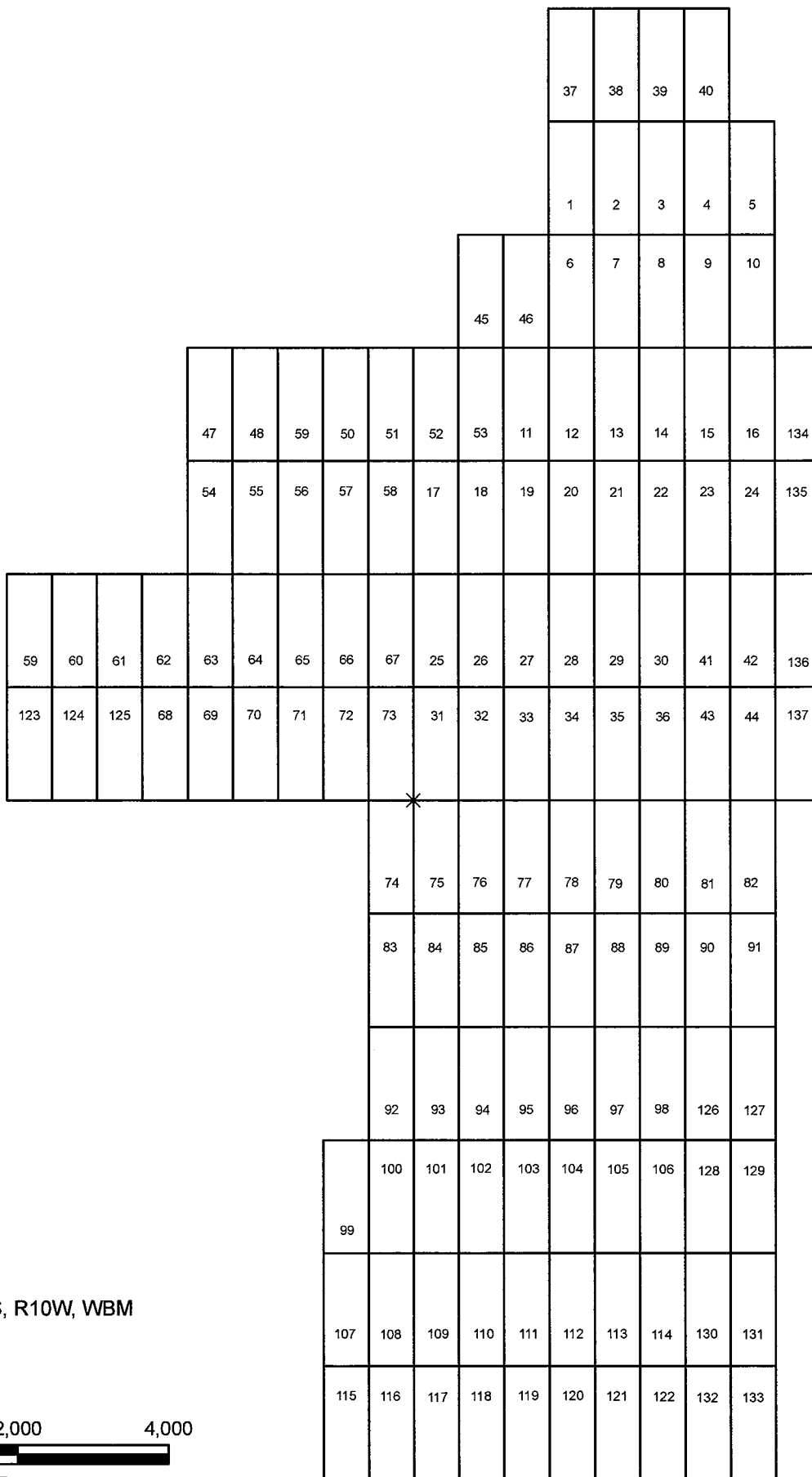
REMARKS
<i>Paid in full for 251 claims - Quit claim - P. R. Kerckhoff</i>

This receipt was generated by the automated BLM Collections and Billing System and is a paper representation of a portion of the official electronic record contained therein.

BUREAU OF LAND MGMT.

2008 JAN 25 PM 3:38

OREGON STATE OFFICE
PORTLAND, OR



Legend

20 Cleo Mining Claim

X SE Corner, Sec. 6, T41S, R10W, WBM

2,000 1,000 0 2,000 4,000



SCALE IN FEET

Prepared for Red Flat Nickel Corp., Inc.
by LithoLogic Resources, LLC

Michael D. Strickler, R.G.
www.LithoLogic.com

DATE 5/29/07
DWN JOS
APP
REV 1/7/08

**CLEOPATRA
CLEO MINING CLAIMS**
Curry County, Oregon
January, 2008

BUREAU OF LAND MGMT.

2008 JAN 25 PM 3:38

OREGON STATE OFFICE
PORTLAND, OR



Legend

- 91 RF Mining Claim
- Discovery Monument
- X SE Corner, Sec. 24, T37S, R14W, WBM

0 750 1,500 3,000 4,500 6,000

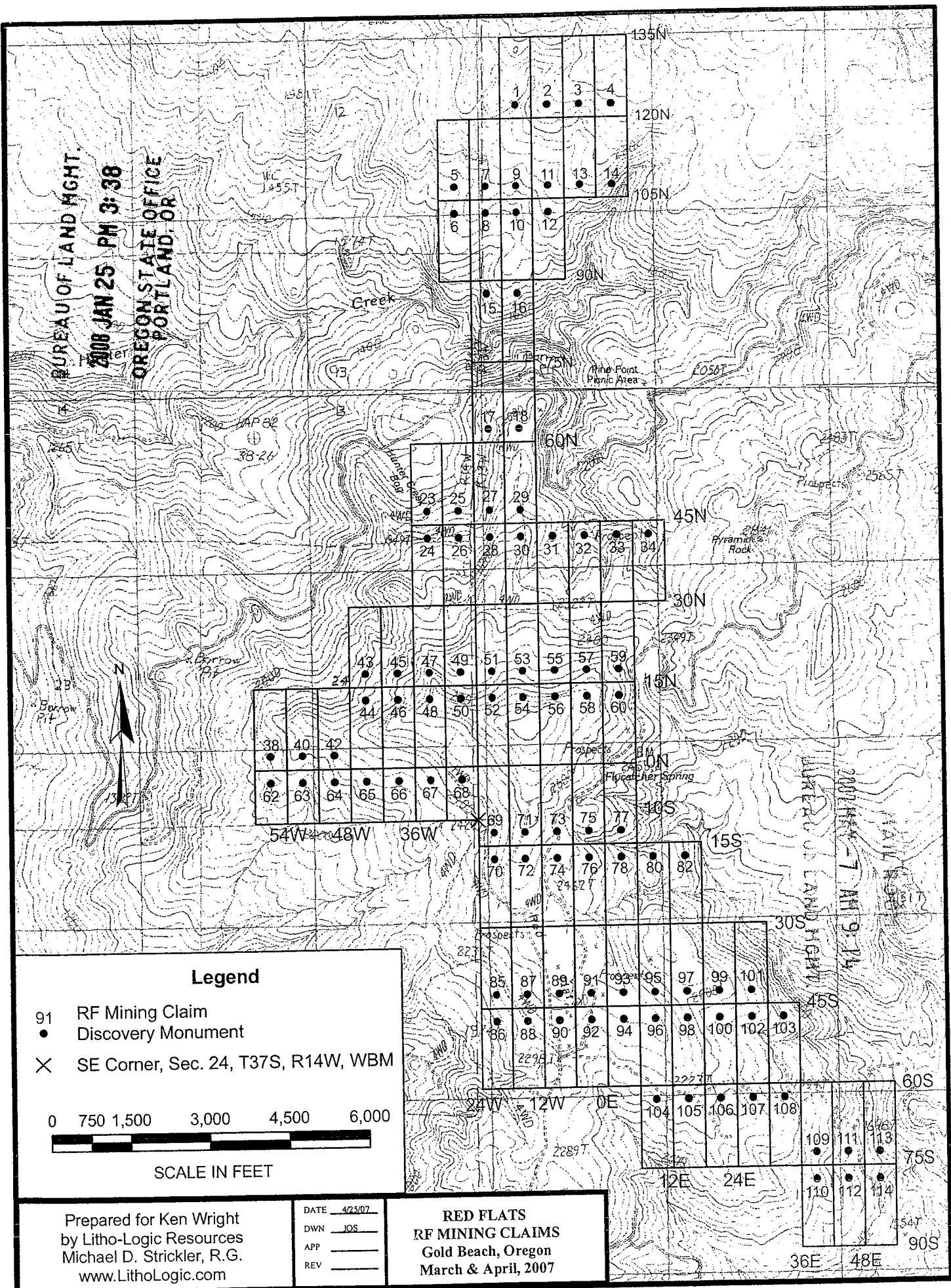


SCALE IN FEET

Prepared for Ken Wright
by Litho-Logic Resources
Michael D. Strickler, R.G.
www.LithoLogic.com

DATE 4/23/07
DWN JOS
APP _____
REV _____

RED FLATS
RF MINING CLAIMS
Gold Beach, Oregon
March & April, 2007



**Recording requested by, and
after recording return to:**
John A. Magliana, Esq.
Bullivant Houser Bailey PC
888 S.W. Fifth Avenue, Suite 300
Portland, Oregon 97204

CURRY COUNTY, OREGON
LAND-DEQC
Cnt=1 Pgs=3 RECC
\$15.00 \$11.00 \$10.00
2007-6768
12/21/2007 02:22 PM
\$36.00



00004483200700067680030031

I Renee' Kolen, County Clerk, certify that the
within document was received and duly recorded
in the official records of Curry County.

Renee' Kolen

Renee' Kolen - Curry County Clerk



**Until a change is requested,
all tax statements shall be sent
to the following address:**
No Change.

STATUTORY QUITCLAIM DEED

KEN WRIGHT, Grantor, releases and quitclaims to RED FLAT NICKEL CORP., INC., a Nevada corporation, Grantee, all right, title and interest in and to the "RF" and "Cleo" groups of unpatented lode mining claims situated in Curry County, Oregon, as further described on Exhibit A attached hereto and by this reference incorporated herein.

TOGETHER WITH all and singular tenements, hereditaments and appurtenances thereunto belonging, or in any way appertaining, and the reversion and reversions, remainder and remainders, rents issues and profits thereof.

TOGETHER WITH all minerals and all veins and lodes of mineral-bearing rock therein and all dips, spurs and angels thereof.

The true consideration for this conveyance is value given other than money.

BEFORE SIGNING OR ACCEPTING THIS INSTRUMENT, THE PERSON TRANSFERRING FEE TITLE SHOULD INQUIRE ABOUT THE PERSON'S RIGHTS, IF ANY, UNDER ORS 197.352. THIS INSTRUMENT DOES NOT ALLOW USE OF THE PROPERTY DESCRIBED IN THIS INSTRUMENT IN VIOLATION OF APPLICABLE LAND USE LAWS AND REGULATIONS. BEFORE SIGNING OR ACCEPTING THIS INSTRUMENT, THE PERSON ACQUIRING FEE TITLE TO THE PROPERTY SHOULD CHECK WITH THE APPROPRIATE CITY OR COUNTY PLANNING DEPARTMENT TO VERIFY APPROVED USES, TO DETERMINE ANY LIMITS ON LAWSUITS AGAINST FARMING OR FOREST PRACTICES AS DEFINED IN ORS 30.930 AND TO INQUIRE ABOUT THE RIGHTS OF NEIGHBORING PROPERTY OWNERS, IF ANY, UNDER ORS 197.352.

DATED this 14 day of December, 2007.

Ken Wright
Name: Ken Wright

OREGON STATE DEPT OF LAND
BUREAU OF LAND MGMT.
2008 JAN 25 PM 3:38
PORTLAND, OR

STATE OF OREGON)
) ss.
County of Lane)

This instrument was acknowledged before me on December 14, 2007 by
Ken Wright.



Jennifer E. Allen
Notary Public of Oregon
My Commission Expires: 9/17/11

OREGON STATE OFFICE
PORTLAND, OR
2008 JAN 25 PM 3:38
BUREAU OF LAND MGMT.

EXHIBIT A

RED FLATS NICKEL CORP.

<u>Claim Number</u>	<u>Instrument Number</u>
RF 34	2007-3955
RF 89	2007-3956

CLEO

<u>Claim Number</u>	<u>Instrument Number</u>
Cleo 38 through Cleo 40	2007-3957 through 2007-3959
Cleo 134 through Cleo 137	2007-5517 through 2007-5520

BUREAU OF LAND MGMT.
2008 JAN 25 PM 3:39
OREGON STATE OFFICE
PORTLAND, OR

Claim List: Cleopatra Claim Block

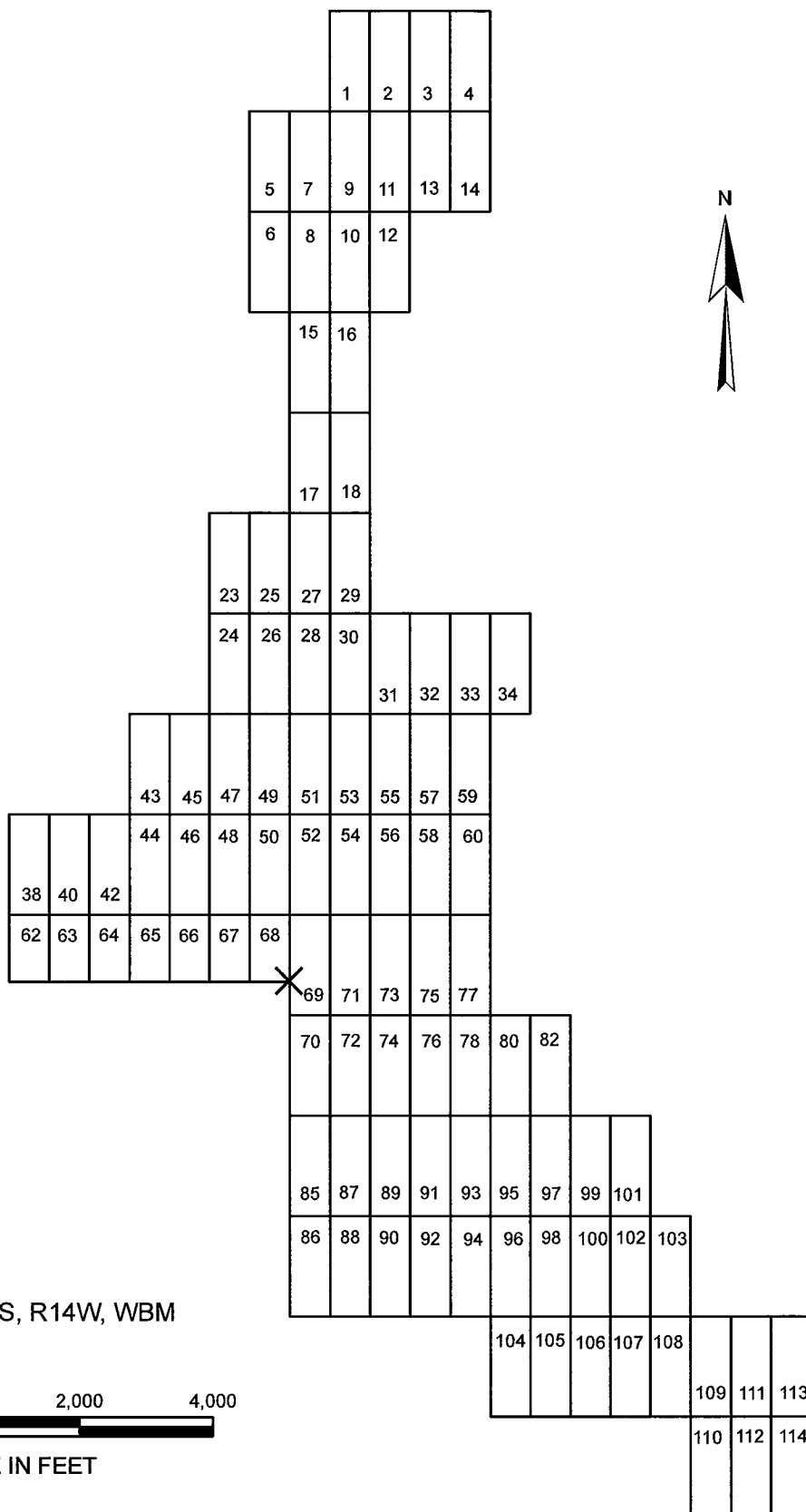
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Cleo # 3	161518	Cleo # 48	161775	Cleo # 93	161820
Cleo # 4	161519	Cleo # 49	161776	Cleo # 94	161821
Cleo # 5	161520	Cleo # 50	161777	Cleo # 95	161822
Cleo # 6	161521	Cleo # 51	161778	Cleo # 96	161823
Cleo # 7	161522	Cleo # 52	161779	Cleo # 97	161824
Cleo # 8	161523	Cleo # 53	161780	Cleo # 98	161825
Cleo # 9	161524	Cleo # 54	161781	Cleo # 99	161826
Cleo # 10	161525	Cleo # 55	161782	Cleo # 100	161827
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Cleo # 14	161529	Cleo # 59	161786	Cleo # 104	161831
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Cleo # 16	161531	Cleo # 61	161788	Cleo # 106	161833
Cleo # 17	161532	Cleo # 62	161789	Cleo # 107	161834
Cleo # 18	161533	Cleo # 63	161790	Cleo # 108	161835
Cleo # 19	161534	Cleo # 64	161791	Cleo # 109	161836
Cleo # 20	161535	Cleo # 65	161792	Cleo # 110	161837
Cleo # 21	161536	Cleo # 66	161793	Cleo # 111	161838
Cleo # 22	161537	Cleo # 67	161794	Cleo # 112	161839
Cleo # 23	161538	Cleo # 68	161795	Cleo # 113	161840
Cleo # 24	161539	Cleo # 69	161796	Cleo # 114	161841
Cleo # 25	161540	Cleo # 70	161797	Cleo # 115	161842
Cleo # 26	161541	Cleo # 71	161798	Cleo # 116	161843
Cleo # 27	161542	Cleo # 72	161799	Cleo # 117	161844
Cleo # 28	161543	Cleo # 73	161800	Cleo # 118	161845
Cleo # 29	161544	Cleo # 74	161801	Cleo # 119	161846
Cleo # 30	161545	Cleo # 75	161802	Cleo # 120	161847
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Cleo # 32	161547	Cleo # 77	161804	Cleo # 122	161849
Cleo # 33	161548	Cleo # 78	161805	Cleo # 123	161850
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Cleo # 36	161551	Cleo # 81	161808	Cleo # 126	161853
Cleo # 37	161764	Cleo # 82	161809	Cleo # 127	161854
Cleo # 38	161765	Cleo # 83	161810	Cleo # 128	161855
Cleo # 39	161766	Cleo # 84	161811	Cleo # 129	161856
Cleo # 40	161767	Cleo # 85	161812	Cleo # 130	161857
Cleo # 41	161768	Cleo # 86	161813	Cleo # 131	161858
Cleo # 42	161769	Cleo # 87	161814	Cleo # 132	161859
Cleo # 43	161770	Cleo # 88	161815	Cleo # 133	161860
Cleo # 44	161771	Cleo # 89	161816	Cleo # 134	162421
Cleo # 45	161772	Cleo # 90	161817	Cleo # 135	162422
				Cleo # 136	162423
				Cleo # 137	162424

Claim List: RF Claim Block					
Claim	ORMC #		Claim	ORMC #	
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RF # 4	161338		RF # 64	161388	
RF # 5	161339		RF # 65	161389	
RF # 6	161340		RF # 66	161390	
RF # 7	161341		RF # 67	161391	
RF # 8	161342		RF # 68	161392	
RF # 9	161343		RF # 69	161393	
RF # 10	161344		RF # 70	161394	
RF # 11	161345		RF # 71	161395	
RF # 12	161346		RF # 72	161396	
RF # 13	161347		RF # 73	161397	
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RF # 15	161349		RF # 75	161399	
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RF # 17	161351		RF # 77	161401	
RF # 18	161352		RF # 78	161402	
RF # 23	161353		RF # 80	161403	
RF # 24	161354		RF # 82	161404	
RF # 25	161355		RF # 85	161405	
RF # 26	161356		RF # 86	161406	
RF # 27	161357		RF # 87	161407	
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RF # 54	161379		RF # 109	161429	
RF # 55	161380		RF # 110	161430	
RF # 56	161381		RF # 111	161431	
RF # 57	161382		RF # 112	161432	
RF # 58	161383		RF # 113	161433	
RF # 59	161384		RF # 114	161434	

BUREAU OF LAND MGMT.

2008 JAN 25 PM 3:40

OREGON STATE OFFICE
PORTLAND, OR



Prepared for Red Flat Nickel Corp., Inc.
by LithoLogic Resources, LLC

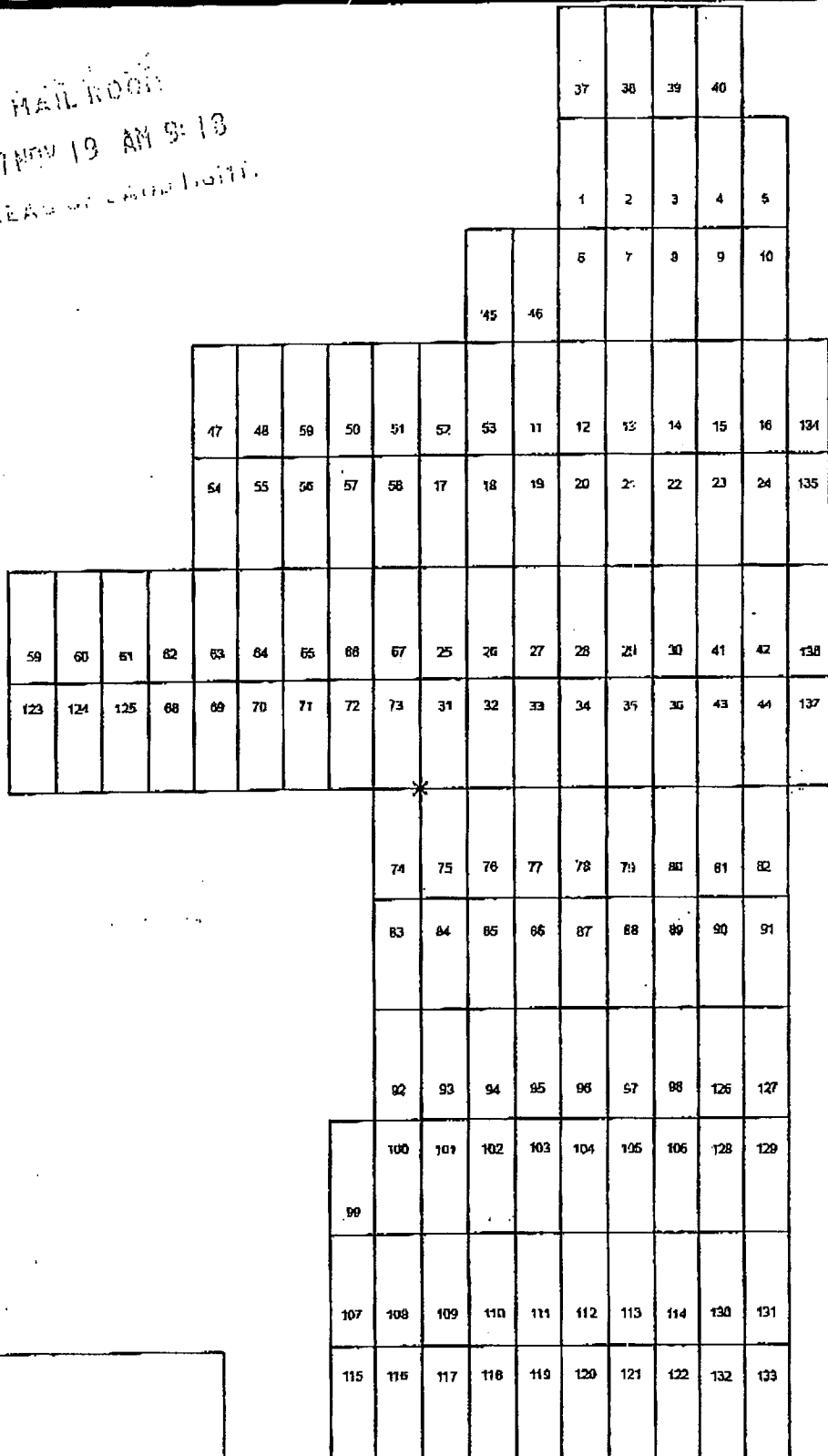
Michael D. Strickler, R.G.
www.LithoLogic.com

DATE 1/7/08
DWN JOS
APP _____
REV _____

**RED FLAT
RF MINING CLAIMS**
Curry County, Oregon
January 7, 2008

MAIL ROOM
2007 NOV 19 AM 9:13
BUREAU OF LAND MGMT.

BUREAU OF LAND MGMT.
2008 JAN 25 PM 3:40
OREGON STATE OFFICE
PORTLAND, OR



Legend

- Cleo Mining Claim
- 20 Discovery Monument
- X SE Corner, Sec. 6, T41S, R10W, WBM

2,000 1,000 0 2,000 4,000
SCALE IN FEET

Prepared for Ken Wright
by LithoLogic Resources, LLC
Michael D. Strickler, R.G.
www.LithoLogic.com

DATE 2/29/07
DWN KE
APP
REV 10/23/07

CLEOPATRA
CLEO MINING CLAIMS
Curry County, Oregon
October, 2007

**Recording requested by, and
after recording return to:**
John A. Magliana, Esq.
Bullivant Houser Bailey PC
888 S.W. Fifth Avenue, Suite 300
Portland, Oregon 97204

**Until a change is requested,
all tax statements shall be sent
to the following address:**
No Change.

CURRY COUNTY, OREGON
LAND-DEQC
Cnt=1 Pgs=3 RECC
\$15.00 \$11.00 \$10.00
2007-5762
10/24/2007 02:03 PM
\$36.00



00003287200700057620030035

I, Renee' Kolen, County Clerk, certify that the
within document was received and duly recorded
in the official records of Curry County.

Renee' Kolen
Renee' Kolen - Curry County Clerk



STATUTORY QUITCLAIM DEED

KEN WRIGHT, Grantor, releases and quitclaims to RED FLAT NICKEL CORP., INC., a Nevada corporation, Grantee, all right, title and interest in and to the "RF" and "Cleo" groups of unpatented lode mining claims situated in Curry County, Oregon, as further described on Exhibit A attached hereto and by this reference incorporated herein.

TOGETHER WITH all and singular tenements, hereditaments and appurtenances thereunto belonging, or in any way appertaining, and the reversion and reversions, remainder and remainders, rents issues and profits thereof.

TOGETHER WITH all minerals and all veins and lodes of mineral-bearing rock therein and all dips, spurs and angels thereof.

The true consideration for this conveyance is value given other than money.

BEFORE SIGNING OR ACCEPTING THIS INSTRUMENT, THE PERSON TRANSFERRING FEE TITLE SHOULD INQUIRE ABOUT THE PERSON'S RIGHTS, IF ANY, UNDER ORS 197.352. THIS INSTRUMENT DOES NOT ALLOW USE OF THE PROPERTY DESCRIBED IN THIS INSTRUMENT IN VIOLATION OF APPLICABLE LAND USE LAWS AND REGULATIONS. BEFORE SIGNING OR ACCEPTING THIS INSTRUMENT, THE PERSON ACQUIRING FEE TITLE TO THE PROPERTY SHOULD CHECK WITH THE APPROPRIATE CITY OR COUNTY PLANNING DEPARTMENT TO VERIFY APPROVED USES, TO DETERMINE ANY LIMITS ON LAWSUITS AGAINST FARMING OR FOREST PRACTICES AS DEFINED IN ORS 30.930 AND TO INQUIRE ABOUT THE RIGHTS OF NEIGHBORING PROPERTY OWNERS, IF ANY, UNDER ORS 197.352.

DATED this 17th day of October, 2007.

OREGON STATE OFFICE
PORTLAND, OR

2008 JAN 25 PM 3:40

BUREAU OF LAND MGMT.

Ken Wright
Name: Ken Wright

STATE OF OREGON)
) ss.
County of Multnomah)

This instrument was acknowledged before me on October 17, 2007 by Ken Wright.



Linda Jones
Notary Public of Oregon
My Commission Expires: 10/9/2009

OREGON STATE OFFICE
PORTLAND, OR
2008 JAN 25 PM 3:41
BUREAU OF LAND MGMT.

EXHIBIT A

RED FLATS NICKEL CORP.

<u>Claim Number</u>	<u>Instrument Number</u>
RF 1 through 16	2007-2372 through 2007-2387
RF 17 through 18	2007-2166 through 2007-2167
RF 23 through 30	2007-1923 through 2007-1930
RF 31 through 34	2007-2168 through 2007-2171
RF 38	2007-2388
RF 40	2007-2389
RF 42	2007-2390
RF 43 through 50	2007-1931 through 2007-1938
RF 51 through RF 60	2007-1683 through 2007-1692
RF 62 through RF 64	2007-2391 through 2007-2393
RF 65 through 68	2007-1939 through 2007-1942
RF 69 through 78	2007-1693 through 2007-1702
RF 80	2007-2394
RF 82	2007-2395
RF 85 through 108	2007-1703 through 2007-1726
RF 109 through 114	2007-1943 through 2007-1948

CLEO

<u>Claim Number</u>	<u>Instrument Number</u>
Cleo 1 through 36	2007-2909 through 2007-2944
Cleo 37	2007-4187
Cleo 38 through 40	2007-3957 through 2007-3959
Cleo 41 through 57	2007-4188 through 2007-4204
Cleo 58	2007-4280
Cleo 59 through 133	2007-4205 through 2007-4279

BUREAU OF LAND MGMT.
2008 JAN 25 PM 3:41
OREGON STATE OFFICE
PORTLAND, OR

Claim List: Cleopatra Claim Block

Claim	ORMC #	Claim	ORMC #	Claim	ORMC #
Cleo # 1	161516	Cleo # 46	161773	Cleo # 91	161818
Cleo # 2	161517	Cleo # 47	161774	Cleo # 92	161819
Cleo # 3	161518	Cleo # 48	161775	Cleo # 93	161820
Cleo # 4	161519	Cleo # 49	161776	Cleo # 94	161821
Cleo # 5	161520	Cleo # 50	161777	Cleo # 95	161822
Cleo # 6	161521	Cleo # 51	161778	Cleo # 96	161823
Cleo # 7	161522	Cleo # 52	161779	Cleo # 97	161824
Cleo # 8	161523	Cleo # 53	161780	Cleo # 98	161825
Cleo # 9	161524	Cleo # 54	161781	Cleo # 99	161826
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Cleo # 11	161526	Cleo # 56	161783	Cleo # 101	161828
Cleo # 12	161527	Cleo # 57	161784	Cleo # 102	161829
Cleo # 13	161528	Cleo # 58	161785	Cleo # 103	161830
Cleo # 14	161529	Cleo # 59	161786	Cleo # 104	161831
Cleo # 15	161530	Cleo # 60	161787	Cleo # 105	161832
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Cleo # 17	161532	Cleo # 62	161789	Cleo # 107	161834
Cleo # 18	161533	Cleo # 63	161790	Cleo # 108	161835
Cleo # 19	161534	Cleo # 64	161791	Cleo # 109	161836
Cleo # 20	161535	Cleo # 65	161792	Cleo # 110	161837
Cleo # 21	161536	Cleo # 66	161793	Cleo # 111	161838
Cleo # 22	161537	Cleo # 67	161794	Cleo # 112	161839
Cleo # 23	161538	Cleo # 68	161795	Cleo # 113	161840
Cleo # 24	161539	Cleo # 69	161796	Cleo # 114	161841
Cleo # 25	161540	Cleo # 70	161797	Cleo # 115	161842
Cleo # 26	161541	Cleo # 71	161798	Cleo # 116	161843
Cleo # 27	161542	Cleo # 72	161799	Cleo # 117	161844
Cleo # 28	161543	Cleo # 73	161800	Cleo # 118	161845
Cleo # 29	161544	Cleo # 74	161801	Cleo # 119	161846
Cleo # 30	161545	Cleo # 75	161802	Cleo # 120	161847
Cleo # 31	161546	Cleo # 76	161803	Cleo # 121	161848
Cleo # 32	161547	Cleo # 77	161804	Cleo # 122	161849
Cleo # 33	161548	Cleo # 78	161805	Cleo # 123	161850
Cleo # 34	161549	Cleo # 79	161806	Cleo # 124	161851
Cleo # 35	161550	Cleo # 80	161807	Cleo # 125	161852
Cleo # 36	161551	Cleo # 81	161808	Cleo # 126	161853
Cleo # 37	161764	Cleo # 82	161809	Cleo # 127	161854
Cleo # 38	161765	Cleo # 83	161810	Cleo # 128	161855
Cleo # 39	161766	Cleo # 84	161811	Cleo # 129	161856
Cleo # 40	161767	Cleo # 85	161812	Cleo # 130	161857
Cleo # 41	161768	Cleo # 86	161813	Cleo # 131	161858
Cleo # 42	161769	Cleo # 87	161814	Cleo # 132	161859
Cleo # 43	161770	Cleo # 88	161815	Cleo # 133	161860
Cleo # 44	161771	Cleo # 89	161816	Cleo # 134	162421
Cleo # 45	161772	Cleo # 90	161817	Cleo # 135	162422
				Cleo # 136	162423
				Cleo # 137	162424

Claim List: RF Claim Block

Claim	ORMC #	Claim	ORMC #
RF # 1	161335	RF # 60	161385
RF # 2	161336	RF # 62	161386
RF # 3	161337	RF # 63	161387
RF # 4	161338	RF # 64	161388
RF # 5	161339	RF # 65	161389
RF # 6	161340	RF # 66	161390
RF # 7	161341	RF # 67	161391
RF # 8	161342	RF # 68	161392
RF # 9	161343	RF # 69	161393
RF # 10	161344	RF # 70	161394
RF # 11	161345	RF # 71	161395
RF # 12	161346	RF # 72	161396
RF # 13	161347	RF # 73	161397
RF # 14	161348	RF # 74	161398
RF # 15	161349	RF # 75	161399
RF # 16	161350	RF # 76	161400
RF # 17	161351	RF # 77	161401
RF # 18	161352	RF # 78	161402
RF # 23	161353	RF # 80	161403
RF # 24	161354	RF # 82	161404
RF # 25	161355	RF # 85	161405
RF # 26	161356	RF # 86	161406
RF # 27	161357	RF # 87	161407
RF # 28	161358	RF # 88	161408
RF # 29	161359	RF # 89	161409
RF # 30	161360	RF # 90	161410
RF # 31	161361	RF # 91	161411
RF # 32	161362	RF # 92	161412
RF # 33	161363	RF # 93	161413
RF # 34	161364	RF # 94	161414
RF # 38	161365	RF # 95	161415
RF # 40	161366	RF # 96	161416
RF # 42	161367	RF # 97	161417
RF # 43	161368	RF # 98	161418
RF # 44	161369	RF # 99	161419
RF # 45	161370	RF # 100	161420
RF # 46	161371	RF # 101	161421
RF # 47	161372	RF # 102	161422
RF # 48	161373	RF # 103	161423
RF # 49	161374	RF # 104	161424
RF # 50	161375	RF # 105	161425
RF # 51	161376	RF # 106	161426
RF # 52	161377	RF # 107	161427
RF # 53	161378	RF # 108	161428
RF # 54	161379	RF # 109	161429
RF # 55	161380	RF # 110	161430
RF # 56	161381	RF # 111	161431
RF # 57	161382	RF # 112	161432
RF # 58	161383	RF # 113	161433
RF # 59	161384	RF # 114	161434

APPENDIX F
NOTICE OF EXPLORATION



File Code: 2810

Date: June 24, 2009

Litho Logic Resources, LLC
Agent for Red Flat Nickel Corporation
Litho Logic Resources, LLC
P. O. Box 369
Selma, Oregon 97538

**CERTIFIED MAIL – RETURN
RECEIPT REQUESTED
NUMBER: 7007 1490 0000 7370 3431**

RE: Red Flat (RF) placer mining

Dear Strickler:

I received and review your 2009 notice of intent (NOI). Your proposal states that you and your company wishes to continue exploration on your unpatented mining claims that are located in the Rogue River/Siskiyou National Forest, Gold Beach Ranger District, near Curry County. The legal location has been established as Township 37 south, Range 13 west, sections 7, 18, 19, 29, 30, 31 and 32, Willamette Meridian.

Based on the information you provided in your NOI and in a pre-season inspection it is my understanding that your proposed operations are as followed:

1. Operations are proposed to begin in late June of 2009 and will be completed by November 30, 2009 (Weather permitting).
2. Access to the site will be on existing roads and trails and that there will be no new roads constructed. Access route will be Forest Service road 3680 to Forest Service road 1703.
3. The proposed exploratory activity will take place on Lobes A & B, Red Flat mining claims, as identified on map.
4. You're proposing to continue your exploration of lateritic materials. You're your crew will use an excavator to dig four to five test holes. Each test hole will be approximately 8 feet wide x 6 feet long to bedrock (approximant average depth is 10 feet deep).
5. Five cubic feet of material will be removed and processed off site. The remaining material will be placed back into the original test site and reclaimed. Individual test site will not exceed 20 cubic yards this season.
 - *Note: Exploratory test areas are within existing bulldozer trenches and in other previous disturbed areas from the USBM and DOGSML programs that occurred in 1960s and 1970s.*
6. No chemicals will be used.
7. Projection of timeframes for each individual test site is 2 to 3 days.
8. Equipment and crew are as followed:



- Sub-surface testing will be accomplished track-mounted excavator.
 - equipment operator (for excavator)
 - Spatial control will be established utilizing a hand-held GPS unit.
 - A geologist to oversee sampling and provide oversight of the process four geo-technicians.
9. No work will take place within 200 feet of any active bogs, streams or seeps. The project will stay 300 feet away from Hunter Creek.
 10. Minimal to no brush will be removed at selected test sites.
 11. No structures will be constructed.

Even though your claims are outside of the POC stands I am requesting that you wash your equipment to help minimize the spread of *Phytophthora lateralis* root disease to uninfected stands of Port-Orford-ceda. All vehicles or ground equipment should be cleared prior to such equipment being moved onto the National Forest and the project area. Cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated and agreed to by a Forest Service representative to avoid runoff into other water sources and to avoid movement of the root disease prior to leaving a main access road onto closed spur roads. Additional wet weather measures include:

- Additional cleaning of personal gear such as boots and hand tools if soil movement on such gear is occurring;
- Vehicle/equipment travel will occur under dry like conditions behind gated roads (cessation of vehicle travel will occur when indicators such as puddles in the roadway or water running in roadside ditches occur in more than isolated locations.);
- Four-wheeler equipment may be washed and left behind gates. Rewashing would be necessary if removed and used on un-gated areas;
- All four-wheelers or track equipment are required to stay on existing roads or skid roads;
- All vehicle, four-wheeler, or track equipment use will cease during significant rain events when movement of soil is likely on both gated or un-gated roads/skid roads;
- Travel routes into the proposed treatment areas will be agreed to;
- Re-washing may be necessary if Forest Service contracting representative determines vehicles/equipment are being used in areas where *P.lateralis* root disease exists and can be transferred back into the project area due to wet weather conditions. If rewashing is necessary within the Project Area due to a change in condition, cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be

designated by a Forest Service representative to avoid runoff into other water sources.

- Only ATV or small tracked vehicles will go behind locked gates. Old skid trails could be used for access with minimal clearing within the old road/trail prism.
- Reseeding of disturbed soil will be required. Obtain seed from the District Office to spread over any disturbed soil.

Based on review of the Siskiyou Forest Plan, your proposed exploratory site testing activities are not likely to cause significant resource disturbance of surface resources. You do not need to submit a Plan of Operations for the activities you have proposed, as stated herein for June 2009 through November 2009.

As a reminder, you are required to follow all State and Federal mining and water quality rules and regulations.

Thank you for notifying our office and if you have any questions concerning the above measures, please call Karla Gallegos or Nancy Schwieger at (541)247-3640.

Sincerely,

/s/ Alan Vandiver
ALAN VANDIVER
District Ranger



United States
Department of
Agriculture

Forest
Service

Rogue River-Siskiyou
National Forest

Gold Beach Ranger District
29279 Ellensburg Ave
Gold Beach, OR 97444

File Code: 2810

Date: October 16, 2007

Mike Strickler
Agent for Ken Wright, claimant
LithoLogic Resources, LLC
P. O. Box 369
Selma, OR 97538

**CERTIFIED MAIL – RETURN
RECEIPT REQUESTED**

NUMBER: 7007 0710 0003 0545 2520

Dear Mr. Strickler:

We have reviewed your proposal after our October 9, 2007 field review. Based on the information you provided in your Notice of Intent for Mining Activities (NOI) I understand that:

1. Operations are proposed to begin in early November.
2. Access to the site will be on existing roads and there will be no new road or trail construction.
3. The proposed exploratory activity will take place on Lobe A (claims 69-114) of the RF Mining claims, as identified in the NOI.
4. All exploration is subsurface drilling using one or two-man augers drilling to a maximum of 15-20 feet.
5. Crew size is no more than 5 people, including the layout geologist.
6. Holes are to be drilled in a grid pattern across the landscape approximately 300 feet from each other and no more than 500 holes will be drilled.
7. No holes will be drilled within 200 feet of bogs, streams or seeps.
8. There will be no cutting of vegetation, except as stated below.
9. There will be no construction of any structures. There will be no camping on National Forest Lands.

To minimize the spread of *Phytophthora lateralis* root disease to uninfected stands of Port-Orford-cedar, all vehicles or ground equipment shall be cleaned prior to such equipment being moved onto the National Forest and the project area. Cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated and agreed to by a Forest Service representative to avoid runoff into other water sources and to avoid movement of the root disease prior to leaving a main access road onto closed spur roads. Additional wet weather measures include:

- Additional cleaning of personal gear such as boots and hand tools if soil movement on such gear is occurring;
- Vehicle/equipment travel will occur under dry like conditions behind gated roads (cessation of vehicle travel will occur when indicators such as



Caring for the Land and Serving People

Printed on Recycled Paper



puddles in the roadway or water running in roadside ditches occur in more than isolated locations);

- Four-wheeler equipment may be washed and left behind gates. Rewashing would be necessary if removed and used on un-gated areas;
- All four-wheelers or track equipment are required to stay on existing roads or skid roads;
- All vehicle, four-wheeler, or track equipment use will cease during significant rain events when movement of soil is likely on both gated or un-gated roads/skid roads;
- Travel routes into the proposed treatment areas will be agreed to;
- Re-washing may be necessary if Forest Service contracting representative determines vehicles/equipment are being used in areas where *P. lateralis* root disease exists and can be transferred back into the project area due to wet weather conditions. If rewashing is necessary within the Project Area due to a change in condition, cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated by a Forest Service representative to avoid runoff into other water sources.
- Only ATV or small tracked vehicles will go behind locked gates. Old skid trails could be used for access with minimal clearing within the old road/trail prism.
- Reseeding of disturbed soil will be required. Obtain seed from the District Office to spread over any disturbed soil.

Based on review of the Siskiyou Forest Plan, your proposed exploratory drilling activities are not likely to cause significant resource disturbance of surface resources. You do not need to submit a Plan of Operations for the activities you have proposed, as stated herein for November 2007 through January 2008, weather dependent.

As a reminder, you are required to follow all State and Federal mining and water quality rules and regulations. Please notify our office 48 hours prior to starting the layout of the drilling locations. Thank you for notifying our office and if you have any questions concerning the above measures, please call Nancy Schwieger at 247-3640.

Sincerely,



 MIKE LAWRENCE
Acting District Ranger

United States
Department of
Agriculture

Forest
Service

Rogue River-Siskiyou
National Forest

Gold Beach Ranger District
29279 Ellensburg Ave
Gold Beach, OR 97444

File Code: 2820

Date: January 30, 2008

Mike Strickler
Agent for Red Flat Nickel Corp., claimant
LithoLogic Resource, LLC
P. O. Box 369
Selma, OR 97538

**CERTIFIED MAIL - RETURN
RECEIPT REQUESTED
NUMBER: 7007 0710 0003 0544 9995**

Dear Mr. Strickler,

We have reviewed your proposal submitted in your 12/20/2007 email. Based on the information you provided in your Notice of Intent for Mining Activities (NOI) I understand that:

1. Operations are proposed to begin in early February.
2. Access to the site will be on existing roads and that there will be no new road or trail construction.
3. The proposed exploratory activity will take place on Lobe B (claims 1-18, 23-34, 38, 40, 42-60, and 62-78) of the RF Mining claims, as identified in the NOI.
4. All exploration is subsurface drilling using one or two-man augers drilling to a maximum of 15-25 feet.
5. Crew size is no more than 5 people, including the layout geologist.
6. Holes are to be drilled in a grid pattern across the landscape at approximately 300 feet from each other and no more than 500 holes will be drilled.
7. No holes will be drilled within 200 feet of bogs, seasonal streams or seeps. You will stay completely out of any riparian area. Perennial stream buffer (no holes drilled within) should be 300'. Avoid Hunter Creek inner gorge.
- > 8. You have stated that the brush clearing should be as minimal as possible. Please keep the brushing minimal and non-linear, go around clumps of brush when possible. No cutting of brush is otherwise allowed. ---
- > 9. Use only roads and spur trails that will allow passage by the ATV, no cutting of trees or brush to open roads or trails.
10. There will be no construction of any structures.
11. There will be no camping on National Forest Lands, unless authorized by forest officer.

To minimize the spread of *Phytophthora lateralis* root disease to uninfected stands of Port-Orford-cedar, all vehicles or ground equipment shall be cleaned prior to such equipment being moved onto the National Forest and the project area. Cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment.



with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated and agreed to by a Forest Service representative to avoid runoff into other water sources and to avoid movement of the root disease prior to leaving a main access road onto closed spur roads. Additional wet weather measures include:

- Additional cleaning of personal gear such as boots and hand tools if soil movement on such gear is occurring;
- Vehicle/equipment travel will occur under dry like conditions behind gated roads (cessation of vehicle travel will occur when indicators such as puddles in the roadway or water running in roadside ditches occur in more than isolated locations.);
- Four-wheeler equipment may be washed and left behind gates. Rewashing would be necessary if removed and used on un-gated areas;
- All four-wheelers or track equipment are required to stay on existing roads or skid roads;
- All vehicle, four-wheeler, or track equipment use will cease during significant rain events when movement of soil is likely on both gated or un-gated roads/skid roads;
- Travel routes into the proposed treatment areas will be agreed to;
- Re-washing may be necessary if Forest Service contracting representative determines vehicles/equipment are being used in areas where *P.lateralis* root disease exists and can be transferred back into the project area due to wet weather conditions. If rewashing is necessary within the Project Area due to a change in condition, cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated by a Forest Service representative to avoid runoff into other water sources.
- Only ATV or small tracked vehicles will go behind locked gates. Old skid trails could be used for access with minimal clearing within the old road/trail prism.
- Reseeding of disturbed soil will be required. Obtain seed from the District Office to spread over any disturbed soil.

Based on review of the Siskiyou Forest Plan, your proposed exploratory drilling activities are not likely to cause significant resource disturbance of surface resources including riparian areas. You do not need to submit a Plan of Operations for the activities you have proposed, as stated herein for February 2008 through September 2008, weather dependent.

As a reminder, you are required to follow all State and Federal mining and water quality rules and regulations. You are hereby notified that you must apply to the U.S. Army Corps of Engineers and obtain or be covered by a section 404 permit, which encompasses Section 401 certification by the State of Oregon, before conducting any suction dredging or the similar mining operations in a stream or its riparian area (please see the attached letter from the Corp). Since the Corp's requirements may change periodically, you should contact the Corps of Engineers at the following address: U.S.

Army Corps of Engineers, Regulatory Branch, 333 S.W. First Avenue, Portland, OR.
97208-2946. Phone: (503) 326-6995.

If you are working where Coho Salmon or any other endangered species are present or found, which our documentation shows they are not present within the project area, it is your responsibility to comply with the Endangered Species Act, which prohibits the take of any endangered species.

Please notify our office 48 hours prior to starting the layout of the drilling locations. Also, we would like a copy of your drilling results, as requested in the field meeting. Thank you for notifying our office and if you have any questions concerning the above measures, please call Nancy Schwieger at 247-3640.

Sincerely,



ALAN VANDIVER
District Ranger

cc: John R Nolan



United States
Department of
Agriculture

Forest
Service

Rogue River-Siskiyou
National Forest

Wild Rivers Ranger District
26568 Redwood Hwy
Cave Junction, OR 97523

File Code: 2810

Date: March 11, 2008

Mike Strickler
Agent for Ken Wright, Claimant
Litho Logic Resources, LLC
PO Box 369
Selma, OR 97538

**CERTIFIED MAIL - RETURN
RECEIPT REQUESTED
NUMBER: 7003 3110 0005 9643 6576**

Dear Mike,

I received your Notice of Intent for Mining Activities (NOI) dated 02/27/08 through an email on February 27, 2008 from our Minerals Administrator, Howard Jubas. I have reviewed your proposal for continued exploratory drilling for nickel, cobalt, and chromium. Based on the information you provided in your NOI and from the phone conversation of March 3, 2008 with Howard Jubas I understand that the proposed exploratory testing is a continuation of last years testing, which is 35% completed and will include the following:

1. Operations are proposed to begin when weather allows with completion of testing by December 31, 2008. Operations will continue seasonally (spring through fall) until the subsurface shallow drilling of no more than 1000 holes is completed.
2. Accessing the site will be on existing roads and that there will be no new road or trail construction. Minor road maintenance to the 4402450 road will be performed by hand, including patching of pot holes using native material from local side cast or from a local borrow pit.
3. The proposed exploratory activity will take place on the Cleopatra claims #1-133 only, which are located in T40S, R10W; T41S, R10W and R11W.
4. All exploration is subsurface drilling using a total of 3 augers drilling to a maximum depth of 20 feet with the two man auger and averaged depths ranging from 6-8 feet for the two (2) single man augers. Crew size for this operation is no more than 5 people.
5. Holes are to be drilled in a grid pattern across the landscape at approximately 300' from each other and no more 1000 holes will be drilled.
6. No holes will be drilled within 200' of any intermittent stream and there are no perennial streams in the testable limits of your proposed operations area.
7. You will plug each hole upon completion of sampling and spread any excess soil to grade by hand.
8. You will not be using heavy earth moving equipment. There will be no cutting of vegetation. A small generator may be used on site to charge GPS equipment.
9. There will be no construction of any structures. Intermittent camping in tents is expected to occur for crew members only at Sourdough Camp. The camp will be kept clean and orderly and all materials and debris will be removed on a weekly basis when the camp is in use.

Jubas
3/20/08
CLAIMS
OK - NO
PERMANENT REC



10. Fuel for the augers and generator will be stored in the back of the crew vehicle and no more than one quart per auger will be packed into the test sites.
11. You will follow all Industrial Fire Precaution Level (IFPL) requirements for internal combustions engine requirements.
12. Seismic testing will be accomplished with geophone sensors connected to a seismic meter. The meter will record and measure time from impact (delivered by striking a sledge hammer to the ground surface) to the sensors.

Based on past years observations of your and similar operations, and a review of the revised Suction Dredge Checklist and the checklist in Appendix 1 of the Revised Environmental Assessment, Siskiyou National Forest, Proposal to Amend the Siskiyou National Forest Land and Resource Management Plan for Mining Operations In Riparian Reserves (1996), your proposed exploratory drilling activities are not likely to cause significant resource disturbance of surface resources nor significantly retard or prevent attainment of the Aquatic Conservation Strategy Objectives. You do not need to submit a Plan of Operations for the activities you have proposed, as stated herein, on Cleopatra claims for the 2008 operating season.

You will be held responsible for checking changes to the IFPL which you will follow for the use of internal combustion engines.

As a reminder, you are required to follow all State and Federal mining and water quality rules and regulations. You are hereby notified that you must apply to the U.S. Army Corps of Engineers and obtain or be covered by a Section 404 permit, which encompasses Section 401 certification by the State of Oregon, before conducting any suction dredging or similar mining operations in a stream or its riparian area. For more information, you may contact the Corps of Engineers at the following address: U.S. Army Corps of Engineers, Regulatory Branch, 333 S.W. First Avenue, Portland, OR 97208-2946. The telephone number is (503) 326-6995.

If you are working where Coho Salmon or any other endangered species are present, it is your responsibility to comply with the Endangered Species Act, which prohibits the take of any endangered species.

Thank you for notifying our office and if you have any questions concerning your operations please call Howard Jubas at 471-6760.

Sincerely,

George Panik
for JOEL T. KING
District Ranger



United States
Department of
Agriculture

Forest
Service

Rogue River-Siskiyou
National Forest

Gold Beach Ranger District
29279 Ellensburg Ave
Gold Beach, OR 97444

File Code: 2820

Date: June 2, 2008

Michael D. Strickler
Agent for Red Flat Nickel Corp.
LithoLogic Resources, LLC
P. O. Box 368
Selma, OR 97538

Dear Mr. Strickler,

We have reviewed your proposal submitted in your 3/21/2008 email. Based on the information you provided in your Notice of Intent for Mining Activities (NOI), and the addendum, I understand that:

1. Operations are proposed to begin in June through November 1, 2008.
2. Access to the site will be on existing roads and that there will be no new road or trail construction.
3. The proposed exploratory activity will take place on Lobe A (RD #1 through RF#114) Mining claims, as identified in the NOI.
4. All exploration is subsurface drilling using a track mounted sonic core drill to 10 sites in Lobe A as shown on map submitted 4/30/08. One single test hole will be drilled at each location. Locations will fall upon existing system or roads and trails, no new road or trails will be created.
5. Upon completion of each test hole the hole will be plugged and tagged, excess soil will be spread to a natural grade and the area will be cleaned up.
6. You have stated that the brush clearing should be as minimal as possible.
7. Resource protection measures will be applied as described in the May 29, 2008 addendum to your Notice of Intent.

Based on review of the Siskiyou Forest Plan, your proposed sonic exploratory drilling activities are not likely to cause significant resource disturbance of surface resources including riparian areas and we don't anticipate there will be any effects to Threatened and Endangered species. You do not need to submit a Plan of Operations for the activities you have proposed, as stated herein for June 2008 through November 2008, weather dependent.

As a reminder, you are required to follow all State and Federal mining and water quality rules and regulations.

Please notify our office 48 hours prior to project initiation.



Thank you for notifying our office and if you have any questions concerning the above measures, please call Nancy Schwieger at 247-3640.

Sincerely,

A handwritten signature in black ink that reads "Alan Vandiver". The signature is written in a cursive, flowing style.

ALAN VANDIVER
District Ranger

Addendum to Notice of Intent

Red Flat Nickel Corp.
Lobe A (RF #1-RF114)
Curry County, Oregon
May 30, 2008

1. No holes will be drilled within 200 feet of bogs, seasonal streams or seeps. You will stay completely out of any riparian area. Perennial stream buffer (no holes drilled within) should be 300'. Hunter Creek inner gorge will be avoided.
2. There will be no construction of any structures.
3. There will be no camping on National Forest Lands, unless authorized by a Forest officer.
4. All vehicles or ground equipment will be cleaned prior to being moved onto the National Forest and the project area. Cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated and agreed to by a Forest Service representative to avoid runoff into other water sources and to avoid movement of the root disease prior to leaving a main access road onto closed spur roads. Additional wet weather measures include:
 - Additional cleaning of personal gear such as boots and hand tools if soil movement on such gear is occurring;
 - Vehicle/equipment travel will occur under dry conditions behind gated roads (cessation of vehicle travel will occur when indicators such as puddles in the roadway or water running in roadside ditches occur in more than isolated locations.);
 - Four-wheeler equipment will be washed and may be left behind gates. They will be washed again if removed and used on un-gated areas;
 - All four-wheelers or track equipment will stay on existing roads or skid roads;
 - All vehicle, four-wheeler, or track equipment use will cease during significant rain events when movement of soil is likely on both gated or un-gated roads/skid roads;
 - Travel routes into the proposed treatment areas will be agreed to with the Forest Service;
 - If Forest Service contracting representative determines vehicles/equipment are being used in areas where *P.lateralis* root disease exists and can be transferred back into the project area due to wet weather conditions, vehicles will be washed again. If rewashing is necessary within the Project Area due to a change in

condition, cleaning will consist of pressure washing to remove all soil and debris from vehicles and equipment with ULTRA Clorox treated water (1 gallon/1000 gallons). Wash sites will be designated by a Forest Service representative to avoid runoff into other water sources.

- Only ATV or small tracked vehicles will go behind locked gates. Old skid trails could be used for access with minimal clearing within the old road/trail prism.
- Reseeding of disturbed soil will be done. We will obtain seed from the District Office to spread over any disturbed soil.

**NOTICE OF INTENT FOR MINING EXPLORATION
ON NATIONAL FOREST SYSTEM LANDS**

USE OF THIS FORM IS OPTIONAL! 1st TIME USERS SHOULD DIRECT QUESTIONS REGARDING THIS FORM OR REGULATIONS (36 CFR 228A) TO THE FOREST SERVICE DISTRICT OFFICE NEAREST YOUR AREA OF INTEREST.

Submitted by: <u>Michael D. Strickler</u>	<u>Agent for Ken Wright, claimant</u>	<u>09/18/07</u>
Signature	Title	Date (mm/dd/yy)
_____	_____	_____
Plan Received by: _____	_____	_____
Signature	Title	Date (mm/dd/yy)

I. GENERAL INFORMATION

- A. Name of Mine/Project: Red Flats
- B. Type of Operation: Exploration of lode mining claims (RF #1 through RF #114)
(lode, placer, mill, exploration, development, production, other)
- C. Is this a (☒ new/☐ continuing) operation? (check one). If continuing a previous operation, this plan (☐ replaces/☐ modifies/☐ supplements) a previous plan of operations. (check one)
- D. Proposed start-up date (mm/dd/yy) of operation: 10/15/07
- E. Expected total duration of this operation: Ongoing until completed
- F. If seasonal, expected date (mm/dd/yy) of annual reclamation/stabilization close out: _____
- G. Expected date (mm/dd/yy) for completion of all required reclamation: _____

II. PRINCIPALS

- A. Name, address and phone number of operator: Ken Wright; 1400 Candlelight Drive, Space #137, Eugene, OR 97402; 360-556-3755
- B. Name, address, and phone number of authorized field representative (if other than the operator). Attach authorization to act on behalf of operator. LithoLogic Resources, LLC; Michael D. Strickler, P.O. Box 369, Selma, OR 97538; 541-597-4086; please see attached authorization
- C. Name, address and phone number of owners of the claims (if different than the operator):

- D. Name, address and phone number of any other lessees, assigns, agents, etc., and briefly describe their involvement with the operation, if applicable:

(If more space is needed to fill out a block of information, use additional sheets and attach form)

III. PROPERTY OR AREA

Name of claim, if applicable, and the legal land description where the operation will be located.

ORMC#	Name	Sections	Township	Range
161335-161434	RF #1-18, 23-34, 38, 40, 42-60, 62-78, 80, 82, 85-114	7, 18, 19, 29, 30, 31, 32 12, 13, 24	37S 37S	13W 14W

IV. DESCRIPTION OF THE OPERATION

- A. **Access.** Show on a map (USGS quadrangle map or a National Forest map, for example) the claim boundaries, if applicable, and all access needs such as roads and trails, on and off the claim. Specify which Forest Service roads will be used, where maintenance or reconstruction is proposed, and where new construction is necessary. For new construction, include construction specifications such as widths, grades, etc., location and size of culverts, describe maintenance plans, and the type and size of vehicles and equipment that will use the access routes.

Access into the claim block is via Hunter Creek Road, which joins US Highway 101 approximately 2 miles south of Gold Beach, Oregon. Approximately 5 miles up from Hwy. 101, Road 3680 allows access into the northern portions of the claim block, with Road 1703 coming in from the south and transiting across the top of Red Flats.

A series of exploration and skid roads branch off of Road 1703 and allow access into outlying sections of the proposed testing areas. Some of these have locked gates, and the claimant requests that keys be issued to facilitate the mobilization of personnel and equipment.

- B. **Map, Sketch or Drawing.** Show location and layout of the area of operation. Identify any streams, creeks or springs if known. Show the size and kind of all surface disturbances such as trenches, pits, settling ponds, stream channels and run-off diversions, waste dumps, drill pads, timber disposal or clearance, etc. Include sizes, capacities, acreage, amounts, locations, materials involved, etc.

See the attached maps for the location of the southern portion of the claims, and the proposed testing area. An extensive network of overgrown roads and trenching sites exists from previous exploration (for the most part during the USBM and DOGAMI programs of the 1960s and 1970s). Limited brushing with machete or chainsaw may be used on selected trails to clear passageways for small pick-ups or ATVs.

(If more space is needed to fill out a block of information, use additional sheets and attach form)

D. **Equipment and Vehicles.** Describe that which is proposed for use in your operation (Examples: drill, dozer, wash plant, mill, etc.). Include: sizes, capacity, frequency of use, etc.

Two (2) General Equipment, Model M240 One Man Hole Diggers (1.5 HP): these drill a 2.25" diameter hole to a maximum depth of 12 to 15 feet. Each auger will run four (4) ten-hour shifts per week.

One (1) General Equipment Series 300 Two Man Hole Digger (5 HP): this drills a 2.25" diameter hole to a depth of fifteen to twenty feet. The use of this auger will be intermittent, and based upon results obtained by the smaller augers testing at 300 foot intervals.

One (1) chainsaw for brush clearing.

E. **Structures.** Include information about fixed or portable structures or facilities planned for the operation. Show locations on the map. Include such things as living quarters, storage sheds, mill buildings, thickener tanks, fuel storage, powder magazines, pipelines, water diversions, trailers, sanitation facilities including sewage disposal, etc. Include engineering design and geotechnical information for project facilities, justification and calculations for sizing of tanks, pipelines and water diversions, etc.

No fixed or permanent structures are planned.

V. ENVIRONMENTAL PROTECTION MEASURES (SEE 36 CFR 228.8)

A. **Air Quality.** Describe measures proposed to minimize impacts on air quality such as obtaining a burning permit for slash disposal or dust abatement on roads.

No air quality impact is anticipated.

(If more space is needed to fill out a block of information, use additional sheets and attach form)

B. **Water Quality.** State how applicable state and federal water quality standards will be met. Describe measures or management practices to be used to minimize water quality impacts and meet applicable standards.

1. State whether water is to be used in the operation, and describe the quantity, source, methods and design of diversions, storage, use, disposal, and treatment facilities. Include assumptions for sizing water conveyance or storage facilities.

2. Describe methods to control erosion and surface water runoff from all disturbed areas, including waste and tailings dumps.

3. Describe proposed surface water and groundwater quality monitoring, if required, to demonstrate compliance with federal or state water quality standards.

4. Describe the measures to be used to minimize potential water quality impacts during seasonal closures, or for a temporary cessation of operations.

5. If land application is proposed for waste water disposal, the location and operation of the land application system must be described. Also describe how vegetation, soil, and surface and groundwater quality will be protected if land application is used.

No fluids of any kind are used in the testing process. All testing will maintain a 200-foot buffer around any permanent or seasonal spring or watercourse. No testing will be completed within the withdrawal area around Flycatcher Springs. No impact on water quality is expected.

C. **Solid Wastes.** Describe the quantity and the physical and chemical characteristics of solid waste produced by the operation. Describe how the wastes will be disposed of including location and design of facilities, or treated so as to minimize adverse impacts.

All un-sampled material from the testing will be spread at the site and blended with the natural slope of the land. No impact is anticipated.

D. **Scenic Values.** Describe protection of scenic values such as screening, slash disposal, or timely reclamation.

No impact is anticipated.

(If more space is needed to fill out a block of information, use additional sheets and attach form)

E. **Fish and Wildlife.** Describe measures to maintain and protect fisheries and wildlife, and their habitat (includes threatened, endangered, and sensitive species) affected by the operations.

No impacts anticipated.

F. **Cultural Resources.** Describe measures for protecting known historic and archeological values, or new sites in the project area.

No impacts anticipated.

G. **Hazardous Substances.**

1. Identify the type and volume of all hazardous materials and toxic substances which will be used or generated in the operations including cyanide, solvents, petroleum products, mill, process and laboratory reagents.

Fuel for the augers and chainsaw.

2. For each material or substance, describe the methods, volume, and frequency of transport (include type of containers and vehicles), procedures for use of materials or substances, methods, volume, and containers for disposal of materials and substances, security (fencing), identification (signing/labeling), or other special operations requirements necessary to conduct the proposed operations.

All fuel will be stored in appropriate containers. Small amounts will be packed with the crews on a daily basis to run the testing equipment.

(If more space is needed to fill out a block of information, use additional sheets and attach form)

3. Describe the measures to be taken for release of a reportable quantity of a hazardous material or the release of a toxic substance. This includes plans for spill prevention, containment, notification, and cleanup.

No release of any toxic substance is anticipated.

H. **Reclamation.** Describe the annual and final reclamation standards based on the anticipated schedule for construction, operations, and project closure. Include such items as the removal of structures and facilities including bridges and culverts, a revegetation plan, permanent containment of mine tailings, waste, or sludges which pose a threat of a release into the environment, closing ponds and eliminating standing water, a final surface shaping plan, and post operations monitoring and maintenance plans.

Upon completion of each test hole and the collection of the necessary samples, the hole will be plugged and tagged, excess soil spread, and the area cleaned and returned to natural grade.

VI. FOREST SERVICE EVALUATION OF NOTICE OF INTENT

A. Required changes/modifications/special mitigation for notice of intent:

(If more space is needed to fill out a block of information, use additional sheets and attach form)

- B. **Bond.** Reclamation of all disturbances connected with this plan of operations is covered by Reclamation Performance Bond No. _____, dated (mm/dd/yy) _____, signed by _____ (Principal) and _____ (Surety), for the penal sum of _____. This Reclamation Performance Bond is a guarantee of faithful performance with the terms and conditions listed below, and with the reclamation requirements agreed upon in the plan of operations. This Reclamation Performance Bond also extends to and includes any unauthorized activities conducted in connection with this operation.

The bond amount for this Reclamation Performance Bond was based on a bond calculation worksheet. The bond amount may be adjusted during the term of this proposed plan of operations in response to changes in the operations or to changes in the economy. Both the Reclamation Performance Bond and the bond calculation worksheet are attached to and made part of this plan of operations.

Acceptable bond securities (subject to change) include:

1. Negotiable Treasury bills and notes which are unconditionally guaranteed as to both principle and interest in an amount equal at their par value to the penal sum of the bond; or
2. Certified or cashier's check, bank draft, Post Office money order, cash, assigned certificate of deposit, assigned savings account, blanket bond, or an irrevocable letter of credit equal to the penal sum of the bond.

VII. TERMS AND CONDITIONS

- A. If a bond is required, it must be furnished before approval of the plan of operations.
- B. Information provided with this plan marked confidential will be treated in accordance with the agency's laws, rules, and regulations.
- C. Approval of this plan does not constitute certification of ownership to any person named herein and/or recognition of the validity of any mining claim named herein.
- D. Approval of this plan does not relieve me of my responsibility to comply with other applicable state or federal laws, rules, or regulations.
- E. If previously undiscovered cultural resources (historic or prehistoric objects, artifacts, or sites) are exposed as a result of operations, those operations will not proceed until notification is received from the Authorized Officer that provisions for mitigating unforeseen impacts as required by 36 CFR 228.4(e) and 36 CFR 800 have been complied with.
- F. This plan of operations has been approved for a period of _____ or until (mm/dd/yy) _____. A new or revised plan must be submitted in accordance with 36 CFR part 228, subpart A, if operations are to be continued after that time period.

(If more space is needed to fill out a block of information, use additional sheets and attach form)

VIII. NOTICE OF INTENT ACCEPTANCE

☐I/☐We have reviewed and agreed to comply with all conditions in this notice of intent including the required changes, modifications, special mitigation, and reclamation requirements.

☐I/☐We understand that the bond will not be released until the Authorized Officer in charge gives written approval.

☐Operator (or ☐Authorized Representative)

(Date)
(mm/dd/yy)

IX. NOTICE OF INTENT APPROVAL

(Name)

(Title)

(Authorized Officer)

(Date)
(mm/dd/yy)

“According to the Paperwork Reduction Act of 1995, an agency may not conduct or sponsor, and a person is not required to respond to a collection of information unless it displays a valid OMB number. The valid OMB number for this information collection is 0596-0022. The time required to complete this information collection is estimated to average 8 hours per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information.”

(If more space is needed to fill out a block of information, use additional sheets and attach form)

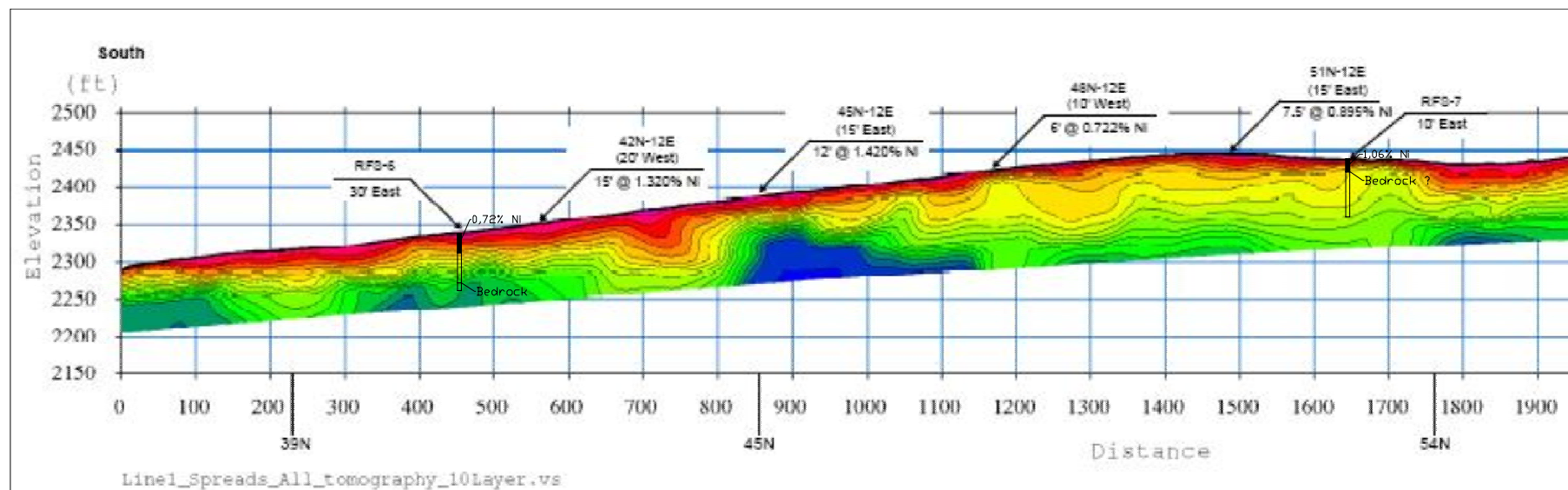
APPENDIX G

BREAKDOWN OF RESOURCE CALCULATION

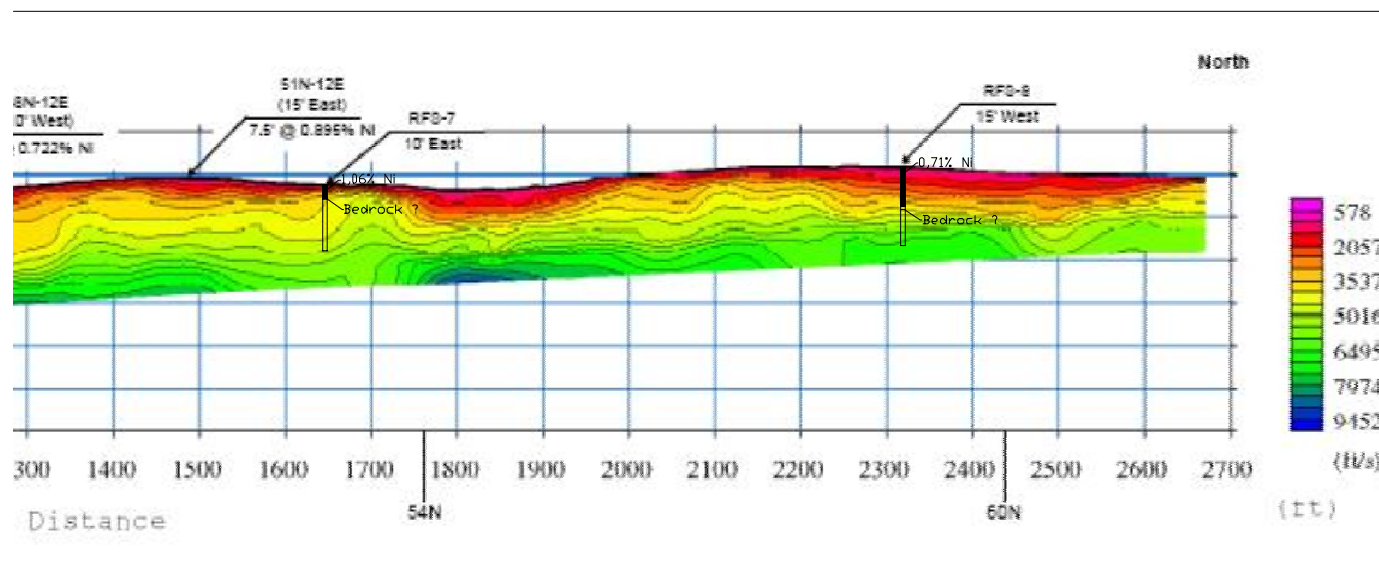
Cut-off Ni (%)		Type	Measured Tons (*1000)	Ni (%)	Indicated Tons (*1000)	Ni (%)	Inferred Tons (*1000)	Ni (%)	Total Inferred Tons (*1000)	Ni (%)
0.7	Inside the measured zone From 0 ft to depth model	Soil	1710	0.91						
		Rock	2277	0.99						
	Outside the measured zone Depth 0ft to 8ft	Soil			3218	0.81				
		Rock			3218	0.81				
	Outside the measured zone Depth 8ft to 16ft	Soil					4169	0.80		
		Rock					4169	0.8		
		Soil	1710	0.91	3218	0.81	4169	0.80	9097	0.82
0.8		Rock	2277	0.99	3218	0.81	4169	0.80	9664	0.85
		Total	3987	0.96	6436	0.81	8338	0.80	18761	0.84
	Inside the measured zone From 0 ft to depth model	Soil	1700	0.91						
		Rock	2007	1.1						
	Outside the measured zone Depth 0ft to 8ft	Soil			1684	0.88				
		Rock			1684	0.88				
	Outside the measured zone Depth 8ft to 16ft	Soil					1728	0.88		
		Rock					1728	0.88		
		Soil	1700	0.91	1684	0.88	1728	0.88	5112	0.89
		Rock	2007	1.10	1684	0.88	1728	0.88	5419	0.96
		Total	3707	1.01	3368	0.88	3456	0.88	10531	0.93

APPENDIX H

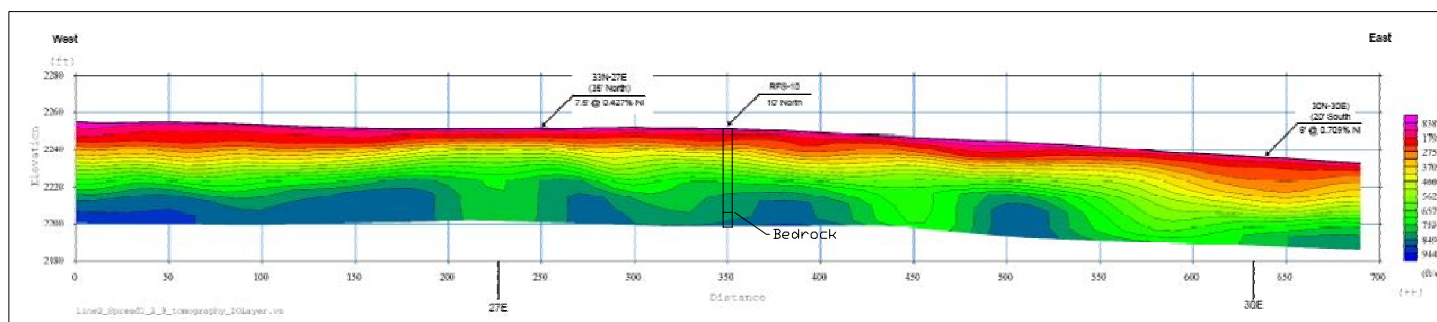
GEOPHYSIC



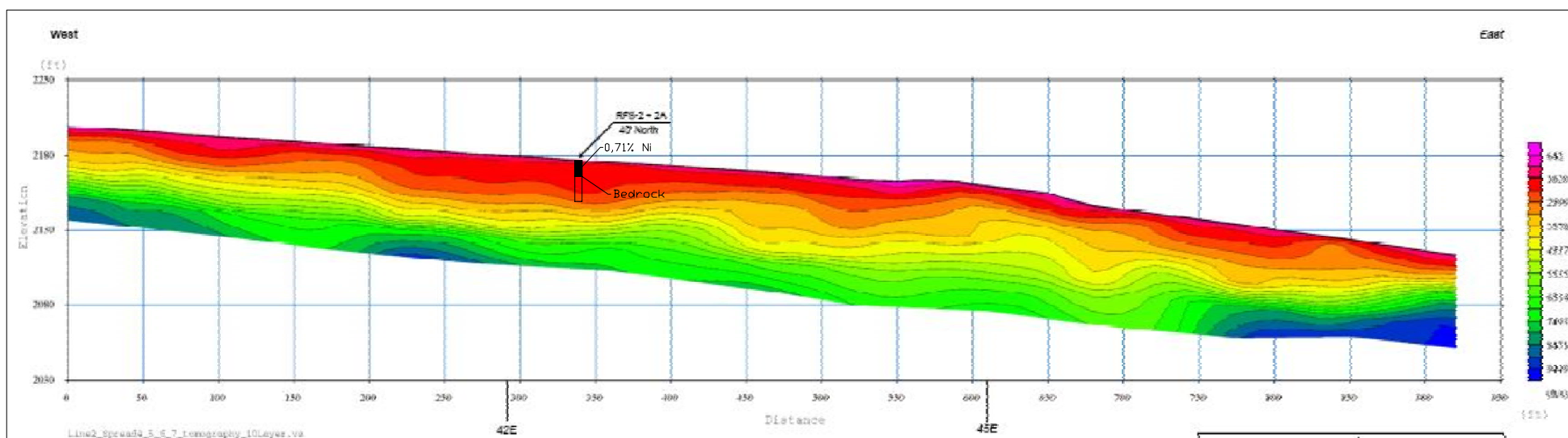
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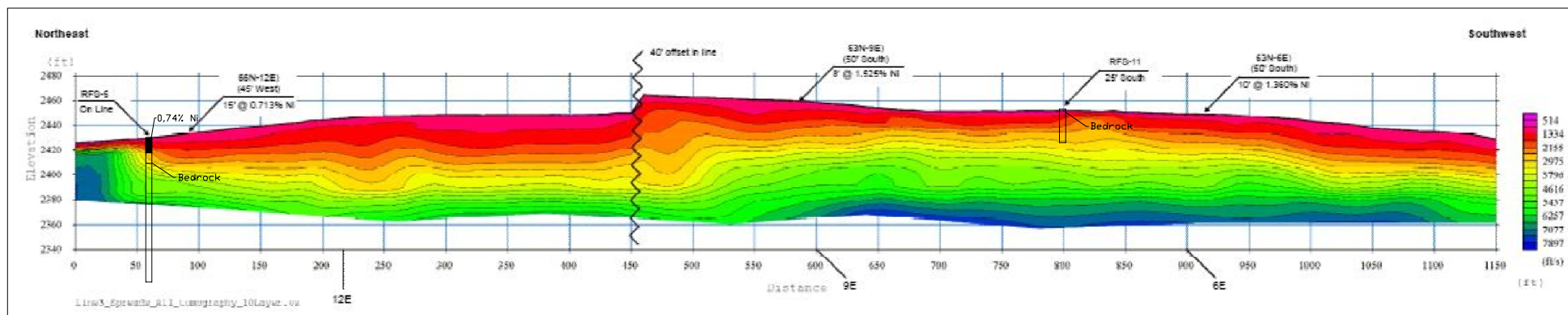
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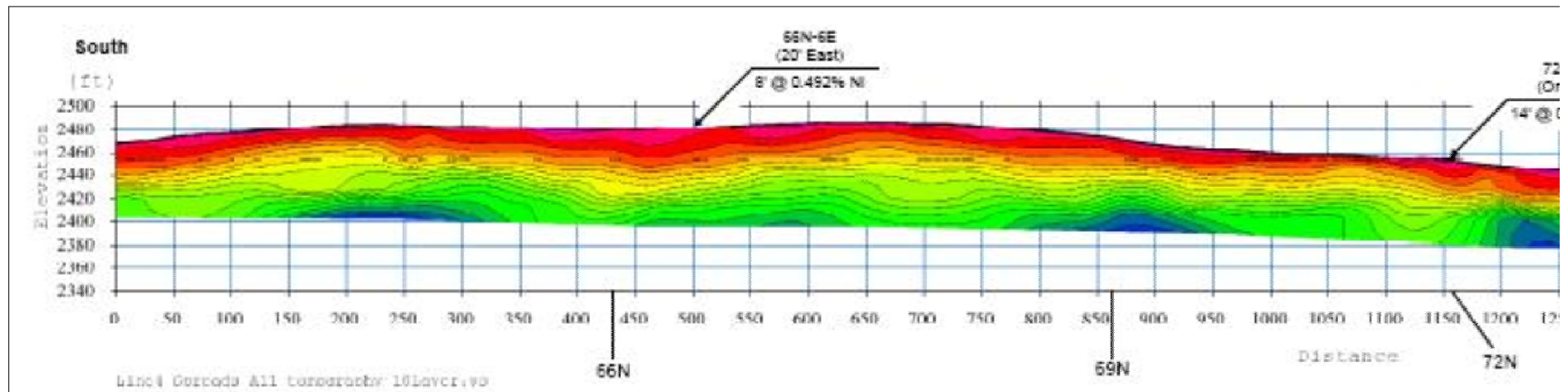
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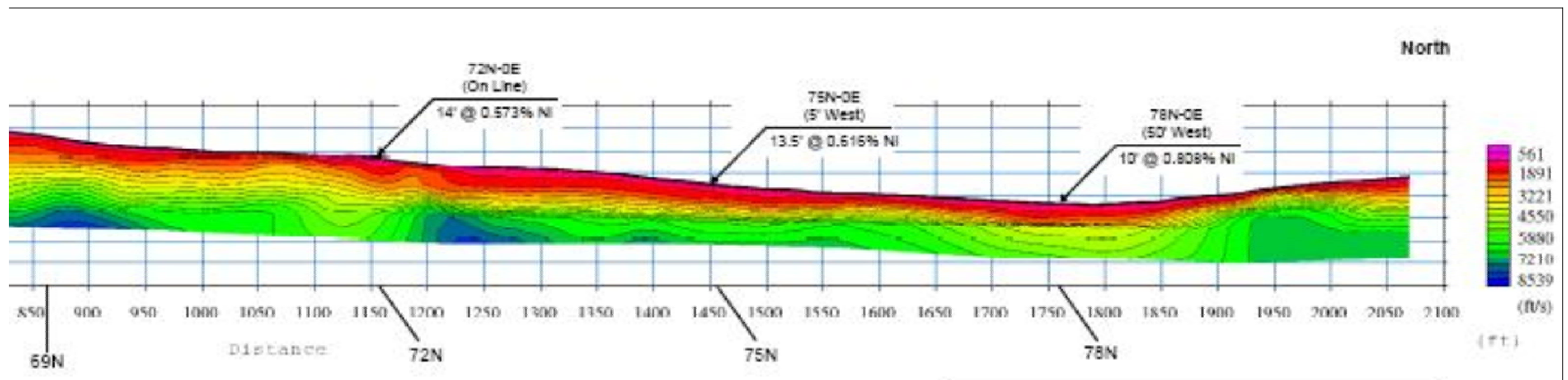
LINE 2 - SPREADS 4 -7



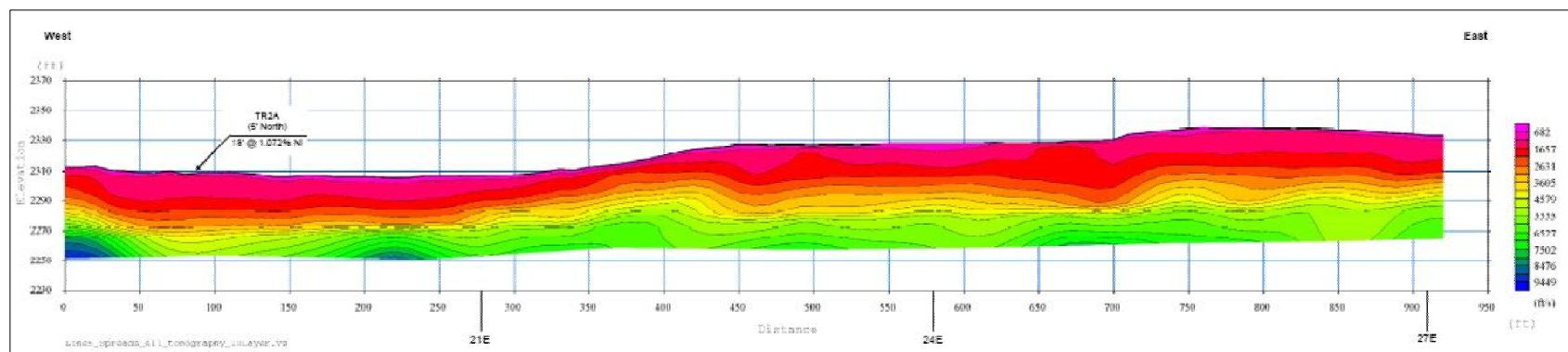
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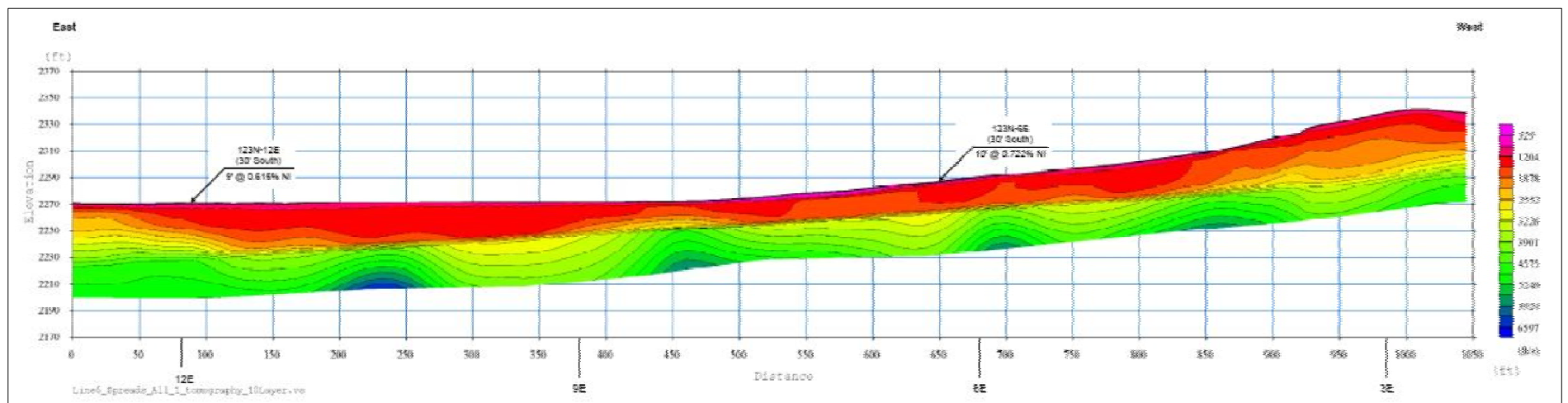
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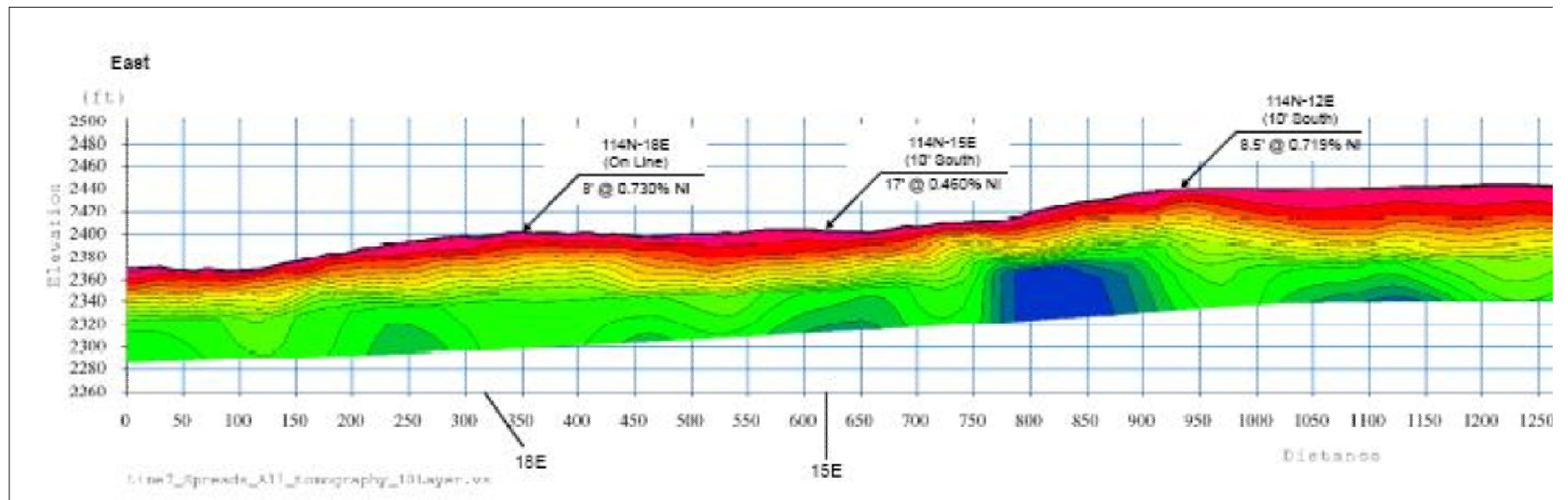
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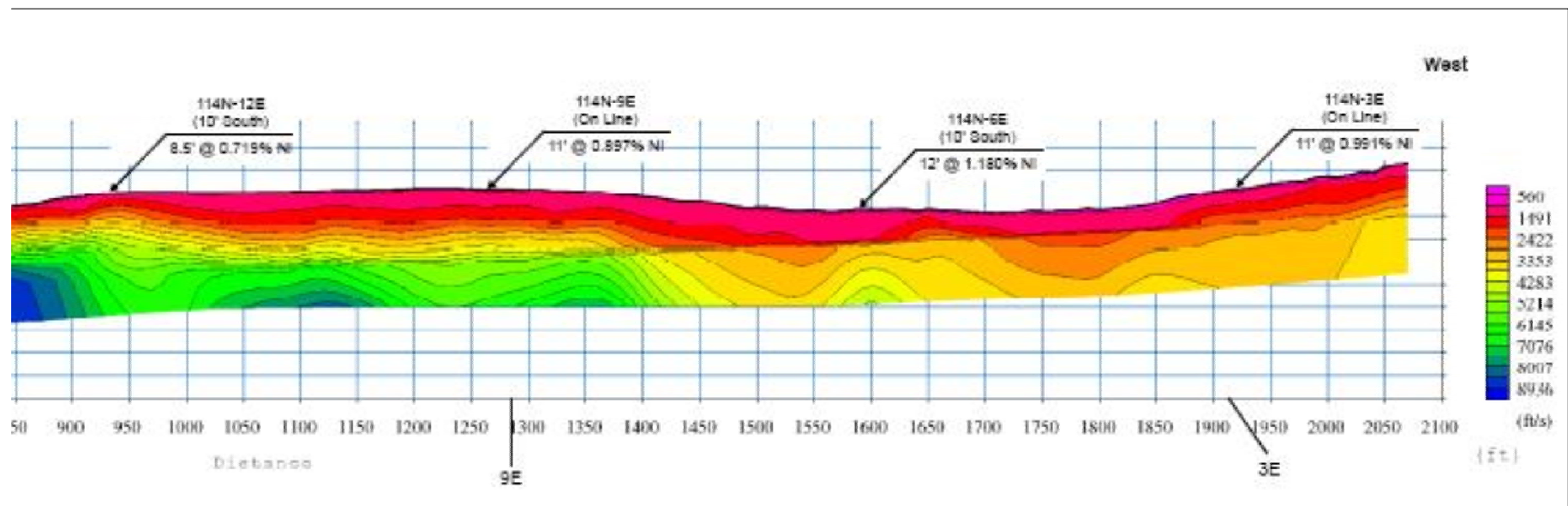
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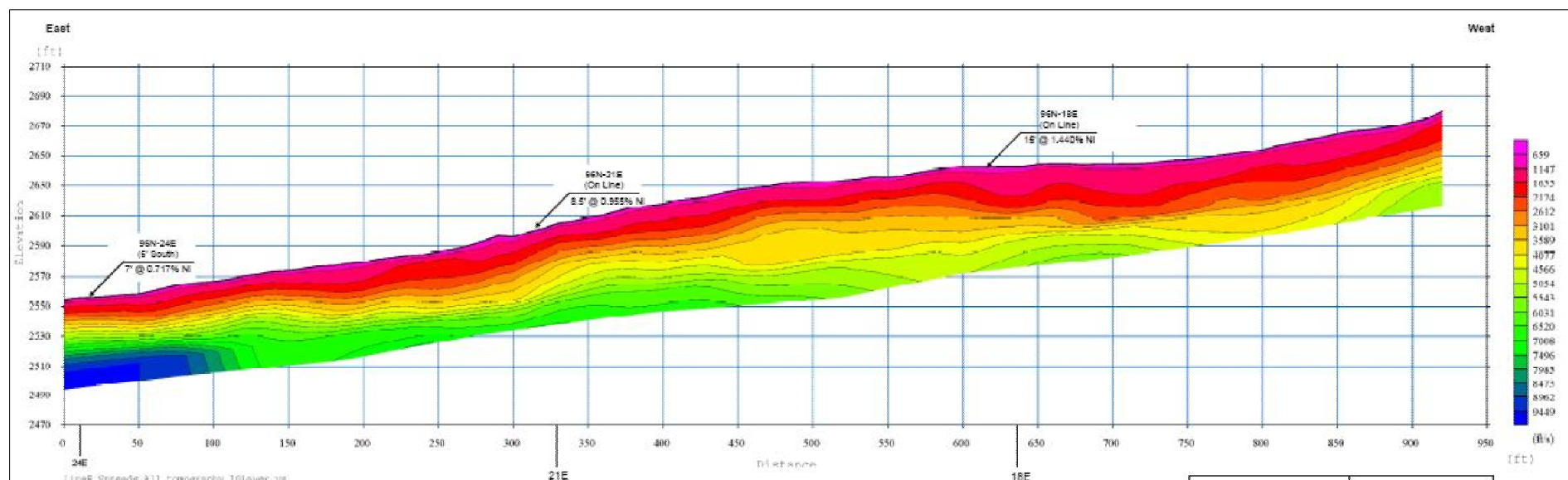
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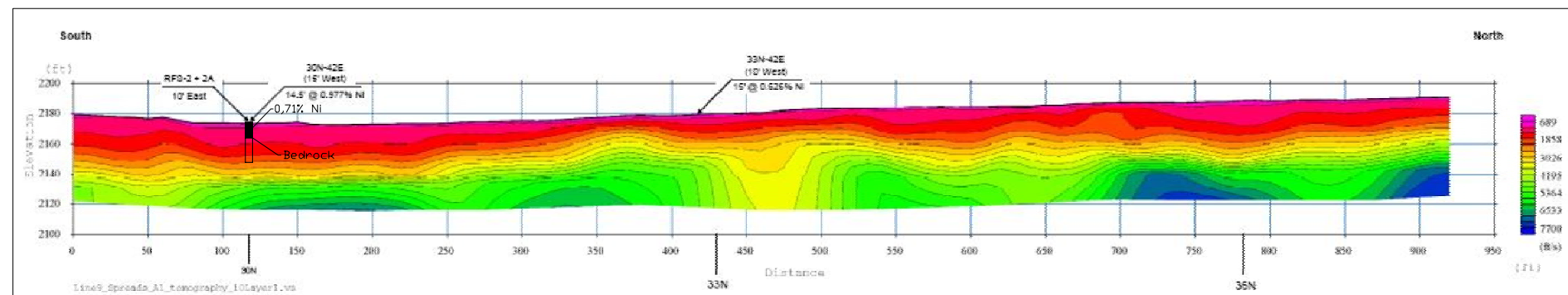
LINE 7



LINE 7



LINE 8



LINE 9